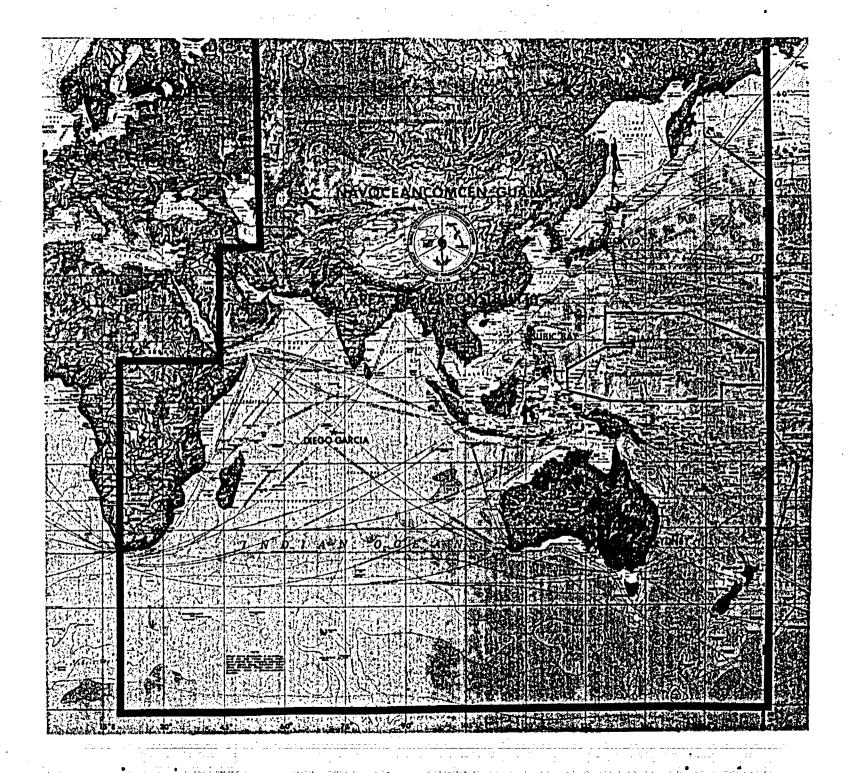


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U.S. NAVAL OCEANOGRAPHY COMMAND CENTER JOINT TYPHOON WARNING CENTER COMNAVMARIANAS BOX 17 FPO SAN FRANCISCO 96630

*JESUS B. TUPAZ Captain, United States Navy

KENDALL G. HINMAN JR.

Captain, United States Navy

COMMANDING

DEAN A. MORSS

Lieutenant Colonel, United States Air Force

COMMANDER, DETACHMENT 1, 1ST WEATHER WING

DIRECTOR, JOINT TYPHOON WARNING CENTER





STAFF

LCDR Benjamin L. Holt, USN MAJ Frank H. Wells, USAF *MAJ Richard A. Todd, USAF *CAPT James N. Heil, USAF LT Robert L. Allen, USN CAPT Roger T. Edson, USAF CAPT Robert S. Lilianstrom, USAF LT Robert C. Weir, USN *ENS James W. Allen, USNR *ENS Mary K. Kopper, USN ENS Richard E. Cianflone, USNR ENS Terrence J. Bonnstetter, USNR SSGT Terry R. Sandmeier, USAF *AG2 Stephani A. Bubanich, USN *AG2 Mahlon W. Perrin, USN AG2 James A. Frush, USN AG2 Carl L. Hurless, USN AG2 Robert B. Campbell, USN *SGT Michael P. Blomquist, USAF *SGT Andrew E. Parker, USAF *AG3 Suzanne L. Silverson, USN *AG3 Beverly A. McCreary, USN AG3 Vickianne Clark, USN AG3 Anne W. Lackey, USN SGT John W. Werner, USAF *SRA James W. Lewis, USAF SRA John C. Giles, USAF SRA Jeffrey A. Goldman, USAF AlC Jeffrey L. Cimini, USAF

CONTRIBUTOR: Detachment 1, 1WW - USAF Satellite Operations

*CAPT Michael S. Risch CAPT James N. Heil *CAPT James A. Smith 1LT David T. Miller MSGT Tommy M. Pelley TSGT Michael R. Pukajlo SSGT Terrence M. Young

*Transferred during 1982

FOREWORD

The Annual Tropical Cyclone Report is prepared by the staff of the Joint Typhoon Warning Center (JTWC), a combined USAF/USN organization operating under the command of the Commanding Officer, U.S. Naval Oceanography Command Center/Joint Typhoon Warning Center, Guam. JTWC was established in April 1959 when CINCPAC directed CINCPACFLT to provide a single tropical cyclone warning center for the western North Pacific region. The operations of JTWC are guided by CINCPACINST 3140.1 (series).

The mission of the Joint Typhoon Warning Center is multi-faceted and includes:

- 1. Continuous meteorological monitoring of all tropical activity in the Northern and Southern Hemispheres, from 180 degrees longitude westward to the east coast of Africa, to anticipate tropical cyclone development.
- 2. Issuing warnings for all significant tropical cyclones in the above area of responsibility.
- Determination or reconnaissance requirements for tropical cyclone surveillance and assignment of appropriate priorities.
- 4. In depth post-storm analysis of all tropical cyclones occurring within the western North Pacific and North Indian Oceans for publication in this report.
- 5. Cooperation with the Naval Environmental Prediction Research Facility (NEPRF), Monterey, California, on the operation evaluation of tropical cyclone models and forecast aids, and the development of new techniques to support operational forecast scenarios.

Should JTWC become incapacitated, the Alternate JTWC (AJTWC), located at the U.S. Naval Western Oceanography Center, Pearl Harbor, Hawaii, assumes warning responsibilities. Assistance in determining satellite reconnaissance requirements, and in

obtaining the resultant data, is provided by Letachment 4, lWW, Hickman AFB, Hawaii.

Satellite imagery used throughout this report represents data obtained by the tropical cyclone satellite surveillance network. The personnel of Det 1, lWW, colocated with JTWC at Nimitz Hill, Guam, coordinate the satellite acquisitions and tropical cyclone surveillance by the following units:

Det 5, 1WW, Clark AB, RP
Det 8, 1WW, Kadena AB, Japan
Det 15, 30WS, Osan AB, Korea
Det 4, 1WW, Hickam AFB, Hawaii
Air Force Global Weather Center,
Offutt AFB, Nebraska

In addition, the Naval Oceanography Command Detachment, Diego Garcia, and DMSP equipped U.S. Navy aircraft carriers have been instrumental in providing vital satellite position fixes of tropical disturbances in the Indian Ocean.

In line with the proposals to implement metric units of measurements within the United States over the next few years, various civilian and military organizations have begun extensive educational programs through use of metric equivalents in their publications. This report will include metric unit equivalent measures whenever possible.

A special thanks is extended to the men and women of: 27th Communication Squadron, Operating Location C, for their continuing support by providing high quality, real-time satellite imagery; the Pacific Fleet Audio-Visual Center, Guam, for their assistance in the reproduction of satellite and graphics data for this report; to the Navy Publications and Printing Service Branch Office, Guam, for their efforts to meet publication deadlines; and to Mrs. Cynthia Blevins for her patience and perseverance in typing the many drafts and the final manuscript of the report.

NOTE: Appendix 5 contains information on how to obtain past issues of the Annual Typhoon Report (redesignated Annual Tropical Cyclone Report in 1980).

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CHAPTER I - OPERATIONAL PROCEDURES

1. GENERAL

The Joint Typhoon Warning Center (JTWC) provides a variety of routine services to the organizations within its area of responsibility, including:

- a. Significant Tropical Weather Advisories: issued daily, this product describes all tropical disturbances and assesses their potential for further development;
- Tropical Cyclone Formation Alerts: issued when synoptic, satellite and/or aircraft reconnaissance data indicate development of a significant tropical cyclone in a specified area is likely;
- c. Tropical Cyclone Warnings: issued periodically throughout each day for signi-ficant tropical cyclones, giving forecasts of position and intensity of the system; and
- d. Prognostic Reasoning Message: issued twice daily for tropical storms and typhoons in the western North Pacific; these messages discuss the rationale behind the most recent warnings.

The recipients of the services of JTWC essentially determine the content of JTWC's products according to their ever-changing requirements. Thus, the spectrum of the routine services is subject to change from year to year; such changes are usually the result of deliberations held at the Annual Tropical Cyclone Conference.

2. DATA SOURCES

a. COMPUTER PRODUCTS:

A standard array of synoptic-scale computer analyses and prognostic charts are available from the Fleet Numerical Oceanography Center (FNOC) at Monterey, California. These products are provided via the Naval Environmental Data Network (NEDN).

b. CONVENTIONAL DATA:

This data set is comprised of landbased and shipboard surface and upper-air observations taken at or near synoptic times, cloud-motion winds derived twice daily from satellite data, and enroute meteorological observations from commercial and military aircraft (AIREPS) within six hours of synoptic times. Conventional data charts are prepared daily at 0000Z and 1200Z using hand- and computer-plotted data for the surface/gradient, 500 mb (mid-tropospheric), and 200 mb (upper-tropospheric) levels. In addition to these charts, a 700 mb (lower-tropospheric) chart is computerplotted from rawinsonde/pibal observations received at FNOC for the 12-hour synoptic times.

c. AIRCRAFT RECONNAISSANCE:

Aircraft weather reconnaissance data are invaluable for the position of the center of developing systems and essential for the accurate determination of numerous parameters, including;

- eye/center temperature and dewpointmaximum surface and flight level wind
- minimum sea level pressure horizontal wind distribution

In addition, wind and pressure-height data at the 500 and/or 400 mb level, provided by the aircraft while enroute to, or from fix missions, provide a valuable supplement to the all too sparse data fields of JTWC's area of responsibility. A comprehensive discussion of aircraft weather reconnaissance is presented in Chapter II.

d. SATELLITE RECONNAISSANCE:

Meteorological satellite data obtained from Defense Meteorological Satellite Program (DMSP), and National Oceanic and Atmospheric Administration (NOAA), spacecraft played a major role in the early detection and tracking of tropical cyclones in 1982. A discussion of the role of these programs is presented in Chapter II.

e. RADAR RECONNAISSANCE:

During 1982, as in previous years, land radar coverage was utilized extensively when available. Once a tropical cyclone moved within the range of land radar sites, their reports were essential for determination of small scale movement. Use of radar reports during 1982 is discussed in Chapter II.

3. COMMUNICATIONS

- a. JTWC currently has access to three primary communications circuits.
- (1) The Automated Digital Network (AUTODIN) is used for dissemination of warnings and other related bulletins to Department of Defense installations. These messages are relayed for further transmission over U.S. Navy Fleet Broadcasts, and U.S. Coast Guard CW (continuous wave Morse code) and voice broadcasts. Inbound message traffic for JTWC is received via AUTODIN addressed to NAVOCEANCONCEN GUAM or JTWC GUAM.
- The Air Force Automated Weather Network (AWN) provides weather data to JTWC through a dedicated circuit from the Automated Digital Weather Switch (ADWS) at Hickam AFB, Hawaii. The ADWS selects and routes the large volume of meteorological reports necessary to satisfy JTWC requirements for the right data at the right time. Weather bulletins prepared by JTWC are inserted into the AWN circuit via the NEDS and the Nimitz Hill Naval Telecommunication Center (NTCC) of the Naval Communications Area Master Station Western Pacific.
- The Naval Environmental Data Network (NEDN) is the communications link with the computers at FNOC. JTWC is able to receive environmental data from FNOC and access the computers directly to run various programs.

. b. The Naval Environmental Display Station (NEDS) has become the backbone of the JTWC communications system; it is the terminal that provides a direct interface with the NEDN and AWN; and it is capable of preparing messages for indirect AUTODIN transmission. The NEDS also provides a means for the Typhoon Duty Officer (TDO) to request forecast aids which are processed on the FNOC computers and transmitted to the TDO over the NEDN circuit.

4. ANALYSES

A composite surface/gradient level (3000 ft (915 m)) manual analysis of the JTWC area of responsibility is accomplished on the 0000Z and 1200Z conventional data. Analysis of the wind field using streamlines is stressed for tropical and subtropical regions. Analysis of the pressure field is accomplished routinely by the Naval Oceanography Command Center (NOCC) Operations watch-team and may be used in conjunction with JTWC's analysis of tropical wind fields.

Manual streamline analysis of the 500 mb level is accomplished on the 0000Z and 1200Z data. This analysis is used to delineate the mid-tropospheric steering currents, which can be extremely important to the tropical cyclone forecast.

A composite upper-tropospheric manual streamline analysis is accomplished daily utilizing rawinsonde data from 300 mb through 100 mb, winds derived from cloud motion analysis, and AIREPS (plus or minus 6 hours) at or above 29,000 feet (8,839 m). Wind and height data are used to arrive at a representative analysis of tropical cyclone outflow patterns, mid-latitude steering currents, and features that may influence tropical cyclone intensity. All charts are hand-plotted over areas of tropical cyclone activity to provide all available data as soon as possible to the TDO. These charts are augmented by the computer-plotted charts for the final analysis.

A 700 mb computer-plotted chart is available for streamline or height-change analysis from the 0000Z and 1200Z data base. Additional sectional charts at intermediate synoptic times and auxiliary charts such as station-time plot diagrams and pressure-change charts are also analyzed during periods of significant tropical cyclone activity.

5. FORECAST AIDS

The following objective techniques were employed in tropical cyclone forecasting during 1982 (a description of these techniques is presented in Chapter IV):

a. MOVEMENT

- (1) 12-HR EXTRAPOLATION
- (2) CLIMATOLOGY
- (3) HPAC (Extrapolation/Climatology)
- (4) BPAC (Extrapolation/Climatology)
- (5) CYCLOPS (Steering)
- (6) TYAN78 (Analog)

- (7) ONE-WAY TROPICAL CYCLONE MODEL (Dynamic)
- (8) NESTED TROPICAL CYCLONE MODEL (Dynamic)
- (9) TAPT (Empirical)

b. INTENSITY

- (1) THETA E (Empirical)
- (2) WIND RADIUS (Analytical)
- (3) DVORAK (Empirical)

6. FORECAST PROCEDURES

a. INITIAL POSITIONING:

In the preparation of each warning an accurate location (fix) of the tropical cyclone's surface center within two to three hours of warning time is of prime importance. JTWC uses the Selective Reconnaissance Program (SRP) to levy an optimal mix of available resources to obtain the necessary fix information. Whenever a tropical cyclone is poorly defined or the actual surface center cannot be determined, and when conflicting fix information is received, the "best estimate" of the surface location is subjectively determined from the analysis of all available data. If the fix data are not available due to reconnaissance platform malfunctions or communication problems, synoptic data or extrapolation from previous fixes are used. The warning position is then obtained by determining the "best track" of the tropical cyclone up to the last fix, or best estimate of the position of its surface center, and forecasting its movement to the warning time.

b. TRACK FORECASTING:

A preliminary forecast track is developed based on an evaluation of the rationale behind the previous warning and the guidance given by the most recent objective techniques and numerical prognoses. This preliminary track is subjectively modified based on the following considerations:

- (1) The prospects for recurvature or erratic movement are evaluated. This evaluation is based primarily on the present and forecast, positions and amplitudes of the middle-tropospheric, mid-latitude troughs as depicted on the latest upper air analyses and numerical prognoses.
- (2) Determination of the best steering level is partly influenced by the maturity and vertical extent of the tropical cyclone. For mature tropical cyclones located south of the subtropical ridge, forecast changes in speed of movement are closely correlated with anticipated changes in the intensity or relative position of the ridge. When steering currents are relatively weak, the tendency for tropical cyclones to move northward due to internal forces is an important consideration.
- (3) Over the 12- to 72-hour forecast period, speed of movement during the early forecast period is usually biased toward persistence, while the subsequent forecast periods are biased toward objective

techniques. When a tropical cyclone moves poleward, and toward the mid-latitude steering currents, speed of movement becomes increasingly more biased toward a selective group of objective techniques capable of estimating significant increases in speed of movement.

(4) The proximity of the tropical cyclone to other tropical cyclones is closely evaluated to determine if there is a possibility of a Fujiwhara interaction (the apparent rotation of two or more cyclones about a common axis or axes).

A final check is made against climatology to determine whether the forecast track is reasonable. If the forecast deviates greatly from one of the climatological tracks, the forecast rationale may be reappraised.

c. INTENSITY FORECASTING:

In this parameter, heavy reliance is placed on intensity trends from aircraft reconnaissance reports, wind and pressure data from ships and land stations in the vicinity of the tropical cyclone, the Dvorak satellite interpretation model and other objective techniques. An evaluation of the entire synoptic situation is made, including the location of major troughs and ridges, the position and intensity of any nearby tropical upper-tropospheric troughs (TUTT), the vertical and horizontal extent of the tropical cyclone's circulation and the extent of the associated upper-level outflow pattern. An essential element affecting each intensity forecast is the accompanying forecast track and the influence of environmental parameters along that track, such as: sea thermal fronts, terrain influences, vertical wind shear, and an extratropical environment.

Once the forecast intensities have been derived, the horizontal distribution of destructive winds (greater than 30-, 50- and 100-knots) is determined. The most recent wind radii and associated asymmetries are deduced from all available surface wind observations and reconnaissance aircraft reports. Based on the current wind distribution, preliminary estimates of future wind radii are provided by an empirically derived objective technique. These estimates may be subjectively modified based on the anticipated interaction of the tropical cyclone's circulation with forecast locations of large-scale wind regimes and significant landmasses. Other factors including the tropical cyclone's speed of movement and possible extratropical transition are considered.

7. WARNINGS

Tropical cyclone warnings are issued when a definite closed circulation is evident and maximum sustained surface winds are forecast to increase to 34 knots (18 meters per second) within 48 hours, or if the tropical cyclone is in such a position that life or property may be endangered within 72 hours. Warnings may also be issued in other situations if it is determined that there is a need to alert military or civil interests to conditions which may become hazardous in a short period of time.

Each tropical cyclone warning is numbered sequentially and includes the following information: the position of the surface center; estimate of the position accuracy and the supporting reconnaissance (fix) platforms; the direction and speed of movement in the past six hours; the intensity and radial extent of surface winds over 30-, 50-, and 100-knots, when applicable. At forecast intervals of 12-, 24-, 48- and 72-hours, information on the tropical cyclone's anticipated position, intensity and wind radii is also provided.

Warnings within the western North Pacific Ocean are issued within two hours of 0000Z, 0600Z, 1200Z and 1800Z with the constraint that consecutive warnings may not be more than seven hours apart. Warnings in the North Indian Ocean are issued within two hours of 0200Z, 0800Z, 1400Z and 2000Z, again with the constraint that consecutive warnings may not be more than seven hours apart. Warning forecast positions are verified against the corresponding "best track" positions. A summary of the verification results from 1982 is presented in Chapter IV.

As of 1 January 1980, JTWC issues tropical cyclone warnings in an Automated Data Processing (ADP) format. This formatted warning possesses readability for all users and allows activities with ADP equipment to enter tropical cyclone warning data directly into ADP equipment data bases.

8. PROGNOSTIC REASONING MESSAGE

For tropical storms and typhoons in the western North Pacific Ocean, prognostic reasoning messages are transmitted following the 0000Z and 1200Z warnings, or whenever the previous reasoning is no longer valid. This plain language message is intended to provide meteorologists with the reasoning behind the latest JTWC forecast.

Included in the prognostic reasoning message are confidence statements for the 24- and 48-hour forecast positions. These confidence values are percentage probabilities that forecast position errors will be less than 100 and 150 nm, and 200 and 300 nm for 24 and 48 hours, respectively. These probabilities are based on objective data from error analysis studies of past tropical cyclones and are a function of current position, initial forecast movement, intensity, and the number of tropical cyclones in warning status in the western North Pacific Ocean.

In addition to this message, prognostic reasoning information applicable to all customers is provided in the remarks section of warnings when significant forecast changes are made or when deemed appropriate by the

9. SIGNIFICANT TROPICAL WEATHER ADVISORY

This product contains a general, non-technical description of all tropical disturbances in the JTWC area of responsibility and an assessment of their potential for further (tropical cyclone) development. In addition, all tropical cyclones in warning status are briefly discussed. This message is issued by 0600Z daily and is reissued whenever the situation warrants.

10. TROPICAL CYCLONE FORMATION ALERT

Formation alerts are issued whenever interpretation of satellite imagery and other meteorological data indicates that the formation of a significant tropical cyclone is likely. These formation alerts will specify a valid period not to exceed 24 hours and must either be cancelled, reissued, or superseded by a tropical cyclone warning prior to the expiration of the valid time.

CHAPTER II - RECONNAISSANCE AND FIXES

1. GENERAL

The Joint Typhoon Warning Center depends on reconnaissance to provide necessary, accurate, and timely meteorological information in support of each warning. JTWC relies primarily on three reconnaissance platforms: aircraft, satellite, and radar. In data rich areas synoptic data are also used to supplement the above. Optimum utilization of all available reconnaissance resources is obtained through the Selective Reconnaissance Program (SRP); various factors are considered in selecting a specific reconnaissance platform including capabilities and limitations, and the tropical cyclone's threat to life/property afloat and ashore. A summary of reconnaissance fixes received during 1982 is included in Section 6 of this Chapter.

2. RECONNAISSANCE AVAILABILITY

a. Aircraft

Aircraft weather reconnaissance in the JTWC area of responsibility is performed by the 54th Weather Reconnaissance Squadron (54th WRS) located at Andersen Air Force Base, Guam. The 54th WRS is presently equipped with six WC-130 aircraft and, from July through October, is augmented by the 53rd WRS from Keesler Air Force Base, Mississippi, bringing the total number of available aircraft to nine. The JTWC reconnaissance requirements, provided daily throughout the year to the Tropical Cyclone Aircraft Reconnaissance Coordinator (TCARC), include system(s) to be fixed, fix times, and forecast positions for each fix. The following priorities are utilized in acquiring meteorological data from reconnaissance aircraft in the western North Pacific area in accordance with CINCPACINST 3140.1 (series):

- (1) Investigative flights and vortex or center fixes.
- (2) Synoptic data acquisition in support of tropical cyclone warnings.
- (3) Supplementary fixes on tropical cyclones.

As in previous years, aircraft reconnaissance provided direct measurements of height, temperature, flight-level winds, sea level pressure, estimated surface wind (when observable), and numerous additional parameters. The meteorological data are gathered by the Aerial Reconnaissance Weather Officers (ARWO) and dropsonde operators of Detachment 4, Hq AWS, who fly with the 54th WRS. These data provide the Typhoon Duty Officer (TDO) with indications of changing tropical cyclone characteristics, radii of associated winds, and current tropical cyclone position and intensity. Another important aspect is the availability of the data for research on tropical cyclone analysis and forecasting.

b. Satellite

Satellite fixes from USAF/USN ground sites and USN ships provide day and night

coverage in the JTWC area of responsibility. Interpretation of this satellite imagery provides tropical cyclone positions and estimates of current and forecast intensities through the Dvorak technique (for daytime rasses).

c. Radar

Land radar provides positioning data on well developed tropical cyclones when in the proximity (usually within 175 nm (324 km)) of the radar sites in the Philippines, Taiwan, Hong Kong, Japan, South Korea, Kwajalein, and Guam.

d. Synoptic

In 1982 JTWC also determined tropical cyclone positions based on the analysis of the surface/gradient level synoptic data. These positions were helpful in situations where the vertical structure of the tropical cyclone was weak or accurate surface positions from aircraft were not available due to flight restrictions.

3. AIRCRAFT RECONNAISSANCE SUMMARY

During the 1982 tropical season, the JTWC levied 276 vortex fixes and 50 investigative missions of which 17 were flown into disturbances which did not develop. In addition to the levied fixes, 180 supplemental fixes were also obtained. The average vector error for all aircraft fixes received at the JTWC during 1982 was 11 nm (20 km).

Aircraft reconnaissance effectiveness is summarized in Table 2-1 using the criteria as set forth in CINCPACINST 3140.1 (series).

TABLE 2-1. AIRCRAFT	RECONNAIS	SANCE EFFE	CTIVENESS
EFFECTIVENESS	NUMBER LEVIED		PERCENT
COMPLETED ON TIME EARLY LATE MISSED	239 6 14 17	_	86.5 2.2 5.1 6.2
TOTA	L 276	_	100.0
LEVIED	VS. MISSED	FIXES MISSED	PERCENT
AVERAGE 1965-1970 1971 1972 1973 1974 1975 1976 1977 1978 1979 1980 1981	507 802 624 227 358 217 317 203 290 289 213 201 276	10 61 126 13 30 7 11 3 2 14 4 4 3	2.0 7.6 20.7 8.4 3.5 1.5 0.7 4.8 1.9 1.5

4. SATELLITE RECONNAISSANCE SUMMARY

The Air Force provides satellite reconnaissance support to JTWC using imagery from a variety of spacecraft. The tropical cyclone satellite surveillance network consists of both tactical and centralized facilities. Tactical DMSP sites are located at Nimitz Hill, Guam; Clark AB, Republic of the Philippines; Kadena AB, Japan; Osan AB, Korea; and Hickam AFB, Hawaii. These sites provide a combined coverage that includes most of the JTWC area of responsibility in the western North Pacific from near the dateline westward to the Malay Peninsula. The Naval Oceanography Command Detachment, Diego Garcia, provides NOAA polar-orbiting coverage in the central South Indian Ocean; this reconnaissance supplements the Air Force Global Weather Central (AFGWC) support in this data sparse region.

AFGWC, located at Offutt AFB, Nebraska, is the centralized member of the tropical cyclone satellite surveillance network. In support to JTWC, AFGWC processes imagery from DMSP and NOAA spacecraft. Imagery processed at AFGWC is recorded on-board the spacecraft as it passes over the earth. Later, these data are downlinked to AFGWC via a network of command/readout sites and communications satellites. This enables AFGWC to obtain the coverage necessary to fix all tropical systems of interest to JTWC. AFGWC has the primary responsibility to provide tropical cyclone surveillance over the entire Indian Ocean and portions of the western North Pacific on both sides of the dateline. Additionally, AFGWC can be tasked to provide tropical cyclone positions in the western North Pacific and South Pacific as backup to coverage routinely available in those regions.

The hub of the network is Det 1, 1WW, colocated with JTWC on Nimitz Hill, Guam. Based on available satellite coverage, Det 1 coordinates satellite reconnaissance requirements with JTWC and tasks the individual network sites for the necessary tropical cyclone fixes. Therefore, when a position from a polar-orbiting satellite is required as the basis for a warning, called a "levied fix", a dual-site tasking concept is applied. Under this concept, two sites are tasked to fix the tropical cyclone from the same satellite pass. This provides the necessary redundancy to virtually guarantee JTWC a successful satellite fix on the tropical cyclone. Using this dual-site concept, the satellite reconnaissance network is capable of meeting all of JTWC's levied satellite fix requirements. Dual-site tasking can also be applied in portions of the North Indian Ocean by tasking AFGWC and the Navy site at Diego Garcia.

The network provides JTWC with several products and services. The main service is one of surveillance. Each site reviews its daily satellite coverage for indications of tropical cyclone development. If an area exhibits the potential for development, JTWC is notified. Once JTWC issues either a formation alert or warning, the network is tasked to provide three products: tropical cyclone positions, intensity estimates, and 24-hour intensity forecasts. Satellite tropical cyclone positions are assigned position code numbers (PCN) depending on the availability of geography for precise gridding and the degree of organization of the tropical cyclone's circulation center (Table 2-2). During 1982, the network provided JTWC with a total of 2026 satellite fixes on tropical systems in the western North Pacific. Another 146 were made for tropical systems in the North Indian Ocean. A comparison of those fixes made on numbered tropical cyclones in the western North Pacific with their corresponding JTWC best track positions is shown in Table 2-3. Estimates of the tropical cyclone's current intensity and a 24-hour intensity forecast are made once each day by applying the Dvorak technique (NOAA Technical Memorandum NESS 45 as revised) to daylight visual data.

The availability of polar-orbiting meteorological satellites declined again in 1982, after an improvement in 1981. At the beginning of 1982, there were three polarorbiting satellites available; F-3 (FTV 14537) with limited coverage and availability, and NOAA 6 and 7 which were functioning normally. In February, NOAA 6 developed scanning problems and provided very little imagery data except for brief periods through most of the 1982 season. In November, the problem was corrected and NOAA 6 began functioning normally once again. NOAA 7, with nearly 8,000 orbits at the end of 1982, provided excellent data throughout the year and served as the network's primary reconnaissance satellite. A DMSP spacecraft, F-6 (FTV 17540), was launched on 20 December and is expected to be operational in January, 1983. F-6 replaces F-3 and may become the network's primary reconnaissance satellite in 1983. The outlook for 1983 looks even better, with projected launches of NOAA-E in February and F-7 in the latter part of the year.

TABLE 2-2. POSITION CODE NUMBERS

PCN METHOD OF CENTER DETERMINATION/GRIDDING

- 1 EYE/GEOGRAPHY
- 2 EYE/EPHEMERIS
- 3 WELL DEFINED CC/GEOGRAPHY
- 4 WELL DEFINED CC/EPHEMERIS
- 5 POORLY DEFINED CC/GEOGRAPHY
- POORLY DEFINED CC/EPHEMERIS

CC = Circulation Center

TABLE 2-3. MEAN DEVIATION (NM) OF ALL SATELLITE DERIVED TROPICAL CYCLONE POSITIONS FROM THE JTWC BEST TRACK POSITIONS. NUMBER OF CASES (IN PARENTHESES).

	WESTERN NORTH PA	ACIFIC OCEAN	NORTH INDIA	OCEAN
	1974-1981 AVERAGE	1982	1980-1981 AVERAGE	1982
PCN	(ALL SITES)	(ALL SITES)	(ALL SITES)	(ALL SITES)
1 2	13.7 (428) 17.9 (85)	12.9 (109) 11.5 (291)	17.0 (9) 9.5 (2)	15.4 (18) 8.5 (2)
3 4	19.5 (652) 24.4 (120)	16.8 (113) 15.7 (293)	29.7 (6) (0)	15.8 (3) 19.1 (3)
5 6	36.6 (1514) 44.1 (317)	32.3 (325) 32.8 (732)	32.0 (22) 37.0 (33)	33.3 (43) 33.6 (31)
1&2	14.4 (513)	11.9 (400)	15.6 (11)	14.7 (20)
3&4	20.4 (772)	16.0 (406)	29.7 (6)	17.5 (6)
5&6	37.9 (1831)	32.6 (1057)	35.0 (55)	33.4 (74)

Besides fixes from the network, JTWC also received satellite-derived tropical cyclone positions from several secondary sources during 1982. These included: U.S. Navy ships equipped for direct readout; the National Environmental Satellite Service (NESS) using NOAA and GOES data; and the Naval Polar Oceanography Center, Suitland, Maryland using stored DMSP and NOAA data. Fixes from these secondary sources are not included in the network statistics.

5. RADAR RECONNAISSANCE SUMMARY

Eighteen of the 28 significant tropical cyclones occurring over the western North Pacific during 1982 passed within range of land based radars with sufficient cloud pattern organization to be fixed. The hourly and oftentimes, half-hourly land radar fixes that were obtained and transmitted to JTWC totaled 475.

The WMO radar code defines three categories of accuracy: good (within 10 km (5 nm)), fair (within 10 to 30 km (5 to 16 nm)), and poor (within 30 to 50 km (16 to 23 nm)). This year, 475 radar fixes were coded in this manner; 243 were good, 145 fair, and 87 poor. Compared to the JTWC best track, the mean vector deviation for land radar sites was 16 nm (30 km). Excellent support through timely and accurate radar fix positioning allowed JTWC to track and forecast tropical cyclone movement through even the most difficult and erratic tracks.

No radar fixes were made by reconnaissance aircraft during the 1982 tropical cyclone season in the western North Pacific area and, as in previous years, no radar reports were received on North Indian Ocean tropical cyclones.

6. TROPICAL CYCLONE FIX DATA

A total of 2970 fixes on 28 western North Pacific tropical cyclones and 127 fixes on five North Indian Ocean tropical cyclones were received at JTWC. Table 2-4, Fix Platform Summary, delineates the number of fixes per platform for each individual tropical cyclone. Season totals and percentages are also indicated.

Annex A includes individual fix data for each tropical cyclone. Fix data are divided into four categories: Satellite, Aircraft, Radar, and Synoptic. Those fixes labelled with an asterisk (*) were determined to be unrepresentative of the surface center and were not used in determining the best tracks. Within each category, the first three columns are as follows:

FIX NO. - Sequential fix number

TIME (Z) - GMT time in day, hours and minutes

FIX POSITION - Latitude and longitude to the nearest tenth of a degree

Depending upon the category, the remainder of the format varies as follows:

a. Satellite

- (1) ACCRY Position Code Number (PCN) is used to indicate the accuracy of the fix positon. A "l" indicates relatively high accuracy and a "6" relatively low accuracy.
- (2) DVORAK CODE Intensity evaluation and trend utilizing visual satellite data (Figure 2-1, Table 2-5). (For specifics, refer to NOAA TM; NESS-45)
- (3) COMMENTS For explanation of abbreviations, see Appendix I.
- (4) SITE ICAO call sign of the specific satellite tracking station.

b. Aircraft

- (1) FLT LVL The constant pressure surface level, in millibars or altitude, in feet, maintained during the penetration. The normal level flown in developed tropical cyclones, due to turbulence factors, is 700 mb. Low-level missions are normally flown at 1500 ft (457 m).
- $\,$ (2) 700 MB HGT Minimum height of the 700 mb pressure surface within the vortex recorded in meters.

TABLE 2-4. FIX PLATFORM SUMMARY FOR 1982

FIX PLATFORM SUMMARY

WESTERN NORTH PACIFIC	AIRCRAFT	SATELLITE	RADAR	SYNOPTIC	TOTAL
TS MAMIE	7	68	3		78
TY NELSON	25	105	11		141
TY ODESSA	15	55			70
TY PAT	16	52	6	1	75
TY RUBY	15	63			78 78
TS TESS		40		8	48
TS SKIP	4	25		ì	30
TS VAL	2	14		4	
					20
TS WINONA	16 11	86	92	3	197
TY ANDY		72	14		97
STY BESS	30	101	4	4	139
TY CECIL	16	82	38	7	143
TY DOT	23	66	3	2	94
TY ELLIS	24	87	64	3	178
TY FAYE	27	133	41	3	204
TY GORDON	36	90			126
TS HOPE	1	26	2	4	33
TY IRVING	13	109	59	7	188
TY JUDY	26	68	10	5	109
TY KEN	33	84	32	3	152
TS LOLA		28			28
TD 22	2	10			12
STY MAC	32	73	35		140
TY NANCY	19	80	14	2	115
	1	15			16
TD 25	27				
TY OWEN	21	128			155
TY PAMELA	3	160	22	3	229
TY ROGER	3	44	25	3 3	75
TOTAL	468	1964	475	63	2970
% OF TOTAL					
NR OF FIXES	15.8	66.1	16.0	2.1	100.0
INDIAN OCEAN		SATELLITE		SYNOPTIC	TOTAL
TC 20-82		46			46
TC 22-82		31			31
TC 23-82		29			29
TC 24-82		6		1	7
TC 25-82		10		4	14
10 23-02		10		**	T.4
TOTAL		122		5	127
		166		.	121
% OF TOTAL					
NR OF FIXES		96.1		3.9	100.0

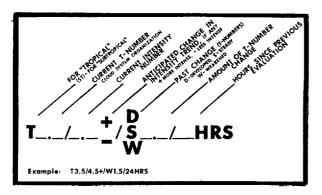


Figure 2-1. The current T-number is 3.5 but the current intensity estimate is 4.5 (equivalent to 17 kt). The cloud system has weakened by 1.5 T-numbers since the previous evaluation conducted $\frac{24}{hours}$ earlier. The plus (+) symbol indicates an expected reversal of the weakening trend or very little further weakening of the tropical cyclone during the next 24-hour period.

AS A F (CURRE NUMBER		DVORAK CI & FI ST INTENSITY)
TROPICAL CYCLONE	WIND SPEED	MSLP (NW PACIFIC)
INTENSITY NUMBER	DI BUD	(1111 211 27
1.0	25	
1.5	25	
2.0	30	1003
2.5	35	999
3.0	45	994
3.5	55	988
4.0	65	981
4.5	77	973
5.0	90	964
5.5	102	954
6.0	115	942
6.5	127	929
7.0	140	915
7.5	155	900
8.0	170	884

- (3) OBS MSLP If the surface center can be visually detected (e.g., in the eye), the minimum sea level pressure is obtained by a dropsonde released above the surface vortex center. If the fix is made at the 1500-foot level, the sea level pressure is extrapolated from that level.
- (4) MAX-SFC-WND The maximum surface wind (knots) is an estimate made by the ARWO based on sea state. This observation is limited to the region of the flight path and may not be representative of the entire tropical cyclone. Availability of data is also dependent upon the absence of undercast conditions and the presence of adequate illumination. The positions of the maximum flight level wind and the maximum observed surface wind do not necessarily coincide.

- (5) MAX-FLT-LVL-WND Wind speed (knots) at flight level is measured by the AN/APN 147 doppler radar system aboard the WC-130 aircraft. Values entered in this category represent the maximum wind measured prior to obtaining a scheduled fix. measurement may not represent the maximum flight level wind associated with the tropical cyclone because the aircraft only samples those portions of the tropical cyclone along the flight path. In many instances, the flight path is through the weak sector of the tropical cyclone. In areas of heavy rainfall, the doppler radar may track energy reflected from precipitation rather than from the sea surface, thus, preventing accurate wind speed measurement. In obvious cases, such erroneous wind data will not be reported. In addition, the doppler radar system on the WC-130 restricts wind measurements to drift angles less than or equal to 27 degrees if the wind is normal (perpendicular) to the aircraft heading.
- (6) ACCRY Fix position accuracy. Both navigational (OMEGA and LORAN) and meteorological (by the ARWO) estimates are given in nautical miles.
- (7) EYE SHAPE Geometrical representation of the eye based on the aircraft radar presentation. The eye shape is reported only if the center is 50 percent or more surrounded by wall cloud.
- (8) EYE DIAM/ORIENTATION Diameter of the eye in nautical miles. When an elliptical eye is present, the lengths of the major and minor axes and the orientation of the major axis are respectively listed. When concentric eye walls are present, each diameter is listed.

c. Radar

- (1) RADAR Specific type of platform (land, aircraft, or ship) utilized for fix.
- (2) ACCRY Accuracy of fix position (good, fair, or poor) as given in the WMO ground radar weather observation code (FM20-V).
- (3) EYE SHAPE Geometrical representation of the eye given in plain language (circular, elliptical, etc.).
- (4) EYE DIAM Diameter of eye given in kilometers.
- (5) RADOB CODE Taken directly from WMO ground weather radar observation code FM20-V. The first group specifies the vortex parameters, while the second group describes the movement of the vortex center.
- $\,$ (6) RADAR POSITION Latitude and longitude of tracking station given in tenths of a degree.
- $\mbox{(7)}$ SITE WMO station number of the specific tracking station.

CHAPTER III - SUMMARY OF TROPICAL CYCLONES

1. WESTERN NORTH PACIFIC TROPICAL CYCLONES

During 1982, the western North Pacific experienced the fourth consecutive year of below average tropical cyclone activity. Twenty-eight tropical cyclones occurred in 1982, three and one-half less than the annual average. Only two significant tropical cyclones failed to develop beyond the tropical depression (TD) stage and seven tropical storms (TS) failed to reach typhoon intensity. Of the 19 tropical cyclones that developed to typhoon (TY) intensity (the highest frequency since 1972), only two reached the 130 kt (67 m/sec) intensity necessary to be classified as super typhoons (STY). In the western North Pacific, tropical cyclones reaching tropical storm intensity or greater are assigned names in alphabetical

order from a list of alternating male/female names (refer to Appendix 3).
Table 3-l provides a summary of key statistics for western North Pacific tropical cyclones. Each tropical cyclone's maximum surface winds (in knots) and minimum observed sea level pressure (in millibars) were obtained from best estimates based on all available data. The distance traveled (in nautical miles) was calculated from the JTWC official best tracks (see Annex A).

Table 3-2 through 3-5 provide further information on the monthly distribution of tropical cyclones and statistics on Tropical Cyclone Formation Alerts and Warnings.

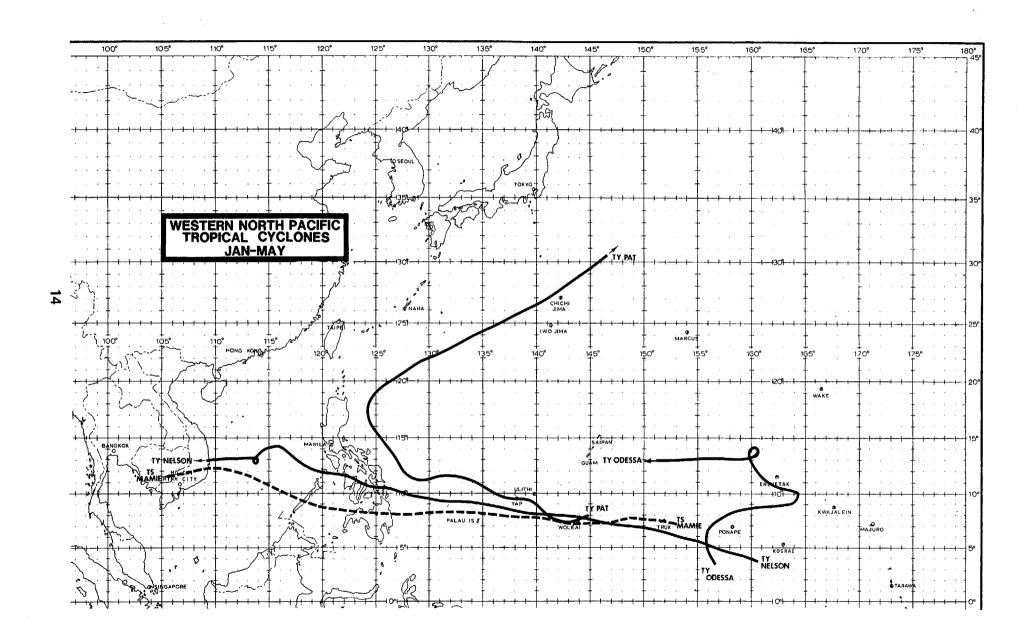
ABLE	3-1.		WESTERN NORT	H PACIFIC			
982	SIGNIFICANT :	TROPICAL CYCLONES					
TROPI	CAL CYCLONE	PERIOD OF WARNING	CALENDAR DAYS OF WARNING	NUMBER OF WARNINGS ISSUED	MAXIMUM SURFACE WIND (KT)	OBSERVED MSLP (MB)	BEST TRACK DISTANCE TRAVELED (
01	TS MAMIE	16 MAR - 24 MAR	9	35	60	990	2733
02	TY NELSON	19 MAR - 1 APR	14	53	105	934	3063
03	TY ODESSA	29 MAR - 4 APR	7	25	75	964	1528
04	TY PAT	17 MAY - 23 MAY	7	24	105	947	1994
05	TY RUBY	21 JUN - 27 JUN	7	25	75	970	2173
06	TS TESS	29 JUN - 2 JUL	4	14	35	999	585
07	TS SKIP	30 JUN → 1 JUL	2	8	50	991	1197
08	TS VAL	3 JUL - 4 JUL	2	7	55	987	867
09	TS WINONA	12 JUL - 17 JUL	6	22	55	985	1486
10	TY ANDY	22 JUL - 30 JUL	9	32	120	920	2072
11	STY BESS	22 JUL - 2 AUG	12	43	140	901	2811
12	TY CECIL	5 AUG - 14 AUG	10	39	125	914	1665
13	TY DOT	9 AUG - 15 AUG	7	27	80	960	2435
14	TY ELLIS	18 AUG - 27 AUG	10	36	125	913	2640
15	TY FAYE	21 AUG - 3 SEP	14	50	90	960	2454
16	TY GORDON	27 AUG - 5 SEP	10	38	100	944	2014
17	TS HOPE	4 SEP - 6 SEP	3	10	60	979	630
18	TY IRVING	5 SEP - 16 SEP	12	44	90	952	1778
19	TY JUDY	5 SEP - 12 SEP	8	29	90	953	2133
20	TY KEN	16 SEP - 25 SEP	10	37	110	936	1647
21	TS LOLA	16 SEP - 19 SEP	4	12	50	993	1424
22	TD 22	21 SEP - 22 SEP	2	5	30	1001	282
23	STY MAC	1 OCT - 9 OCT	9	32	140	895	2287
24	TY NANCY	13. OCT - 18 OCT	8	29	115	926	2400
25	TD 25	15 OCT - 16 OCT	2	5	20	1002	228
26	TY OWEN	15 OCT - 27 OCT	** 12	40	105	939	3604
27	TY PAMELA	24 NOV - 9 DEC	16	60	100	940	4291
28	TY ROGER	8 DEC - 10 DEC	3	12	65	985	906
**	IN ADDITION	1982 TOTALS: DAYS INCLUDED ONLY 17 AMENDED WARNIN WERE ISSUED FOR TY	GS WERE ISSU	JED DURING 1	1982		

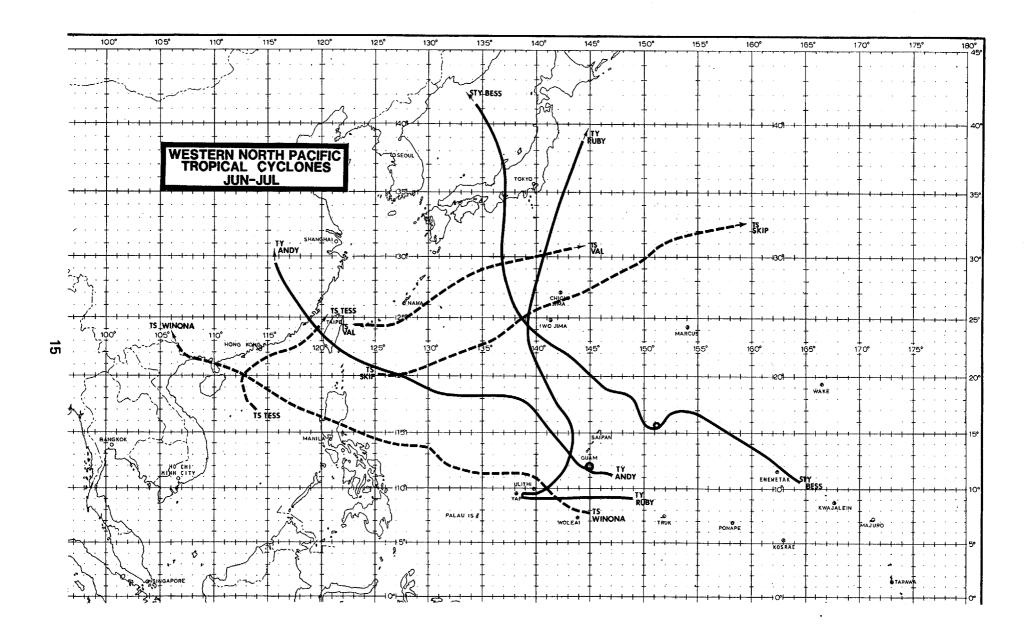
TABLE 3-2.															
WESTERN			19	82 SI	GNIFI	CANT	TROP	ICAL (CYCLO	NES				1	
NORTH PACIFIC	<u>JAN</u>	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL	(1959-: <u>AVERAGE</u>	L981) CASES
TROPICAL DEPRESSIONS	0	0	0	0	0	0	0	0	1	1	0	0	2	4.0	91
TROPICAL STORMS	0	0	1	0	0	2	2	0	2	0	0	0	7	9.8	225
TYPHOONS	0	0	2	0	1	1	2	5	3	3	1	1	19	17.8	409
ALL TROPICAL CYCLONES	0	0	3	0	1	3	4	5	6	4	1	1	28	31.5	725
1959-1981						·								PREVI	ous
AVERAGE	.6	• 3	.7	1.0	1.4	2.0	5.0	6.3	5.9	4.4	2.7	1.4	31.5	23-Y	EAR
CASES	13	8	15	22	32	45	115	144	136	101	62	32	725	HIST	ORY
FORMATION ALERT:	LERTS: 26 of 36 Formation Alert Events developed into significant trop cyclones. Tropical Cyclone Formation Alerts were issued for a two of the significant tropical cyclones that developed during								r all but						
WARNINGS:	ARNINGS: Number of warning days: 150														
	Number of warning days with two tropical cyclones in region: 56														
								three		6					

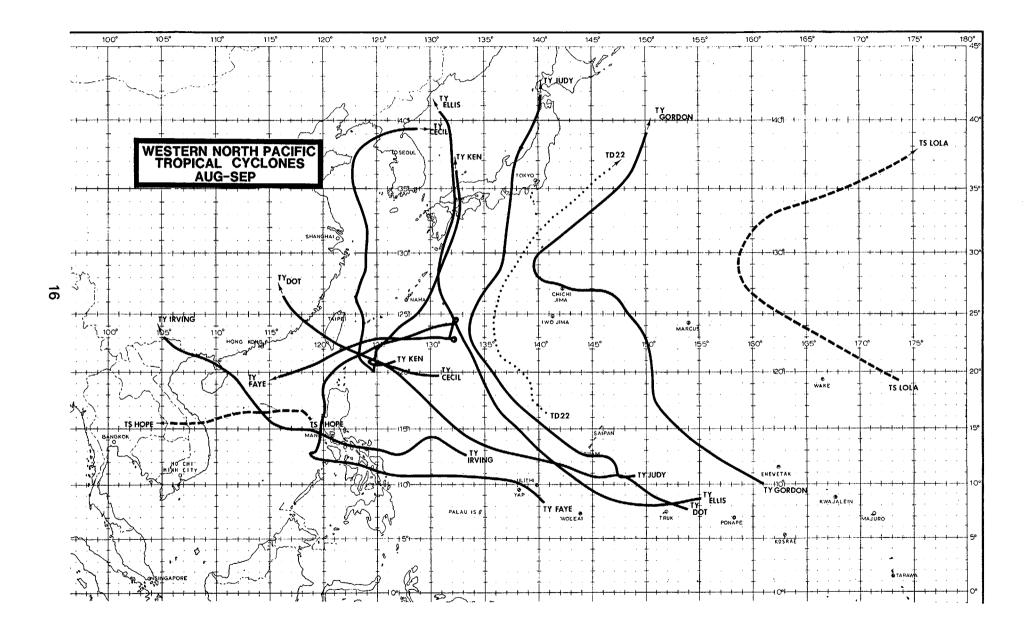
TABLE 3-3.													
		F	REQUE	NCY O	F TYP	HOONS	BY M	ONTH .	AND Y	EAR			
		_											
YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
						_			_				
(1945-1958) AVERAGE	. 4	.1	. 3	. 4	. 7	1.1	2.0	2.9	3.2	2.4	2.0	. 9	16.3
AVERAGE	. 4	• +	• •	• 4	• /	1.1	2.0	2.,	3.2	2.7	2.0	• •	10.5
1959	0	0	0	1	0	0	1	5	3	3	2	2	17
1960	0	0	0	1	0	2	2	8	0	4	1	1	19
1961	0	0	1	Ó	2	1	3	3	5	3	1	1	20
1962	0	0	0	1	2	0	5	7	2	4	3	0	24
1963	0	0	0	1	1	2	3	3	3	4	0	2	19
1964	0	0	0	0	2	2	6	3	5	3	4	1	26
1965	1	0	0	1	2	2	4	3	5	2	1	0	21
1966	0	0	0	1	2	1	3	6	4	2	0	1	20
1967	0	0	1	1	0	1	3	4	4	3	3	0	20
1968	0	0	0	1	1	1	1	4	3	5	4	0	20
1969	1	0	0	1	0	0	2	3	2	3	1	0	13
1970	0	1	0	0	0	1	0	4	2	3	1	0	12
1971	0	0	0	3	1	2	6	3	5	3	1	0	24
1972	1	0	0	0	1	1	4	4	3	4	2	2	22
1973	0	0	0	0	0	0	4	2	2	4	0	0	12
1974	0	0	0	0	1	2	1	2	3	4	2	0	14
1975	1	0	0	0	0	0	1	3	4	3	2	0	15
1976	1	0	0	1	2	2	2	1	4	1	1	0	15
1977	0	0	0	0	0	0	3	0	2	3	2	1	11
1978	ŏ	Ō	0	1	0	0	3	2	4	3	2	0	15
1979	1	0	1	1	0	0	2	2	3	2	1	1	14
1980	0	0	0	0	2	0	3	2	5	2	1	0	15
1981	0	0	1	0	0	2	2	2	4	1	2	2	16
1982	0	0	2	0	1	1	2	5	3	3	1	1	19
(1959-1982)													
AVERAGE	.3	.04	.3	.6	.9	1.0	2.8	3.4	3.3	3.0	1.6	. 7	17.8
CASES	6	1	6	15	20	23	66	81	80	72	38	15	423

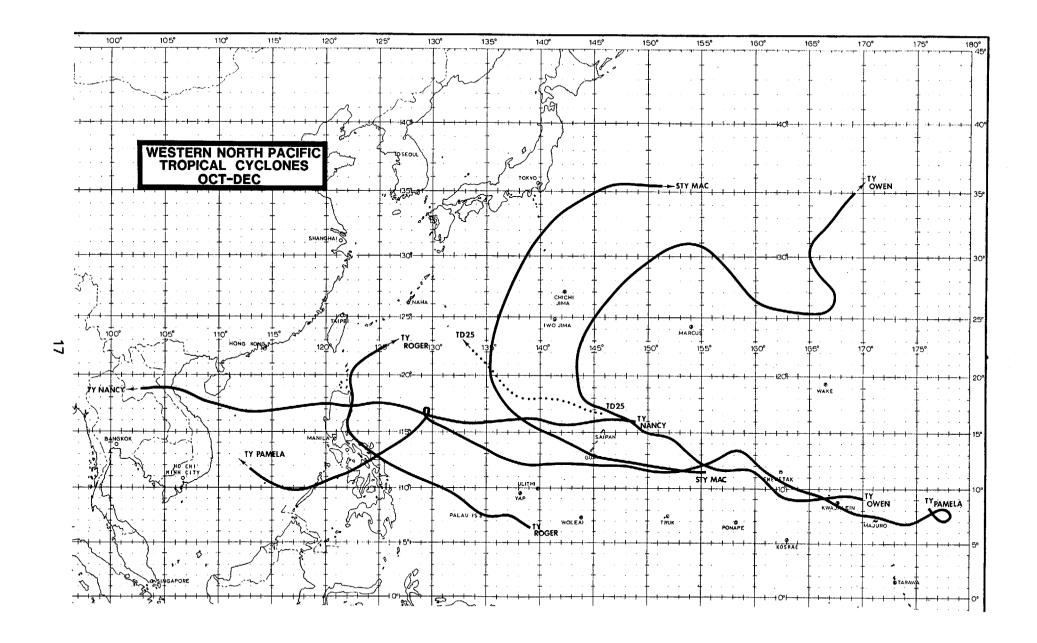
YEAR YEAR YEAR JAN FEB MAR APR MAY JUN JUL AUG SEP OCT NOV DEC TOTAL (1945-1958) AVERAGE .4 .1 .4 .5 .8 1.3 3.0 3.9 4.1 3.3 2.7 1.1 21.6 1959 0 1 1 1 1 0 0 0 3 6 6 6 4 2 2 2 26 1960 0 0 0 1 1 1 1 3 2 5 4 6 5 1 1 31 1962 0 1 1 0 1 2 0 6 7 3 5 3 2 30 1963 0 0 0 1 1 1 1 3 2 5 4 6 6 7 3 2 3 3 1964 0 0 0 0 1 1 1 3 3 4 3 5 5 0 3 25 1964 0 0 0 0 0 1 1 1 6 8 7 9 7 6 6 1 40 1965 2 2 1 1 2 3 5 6 7 2 2 2 1 30 1966 0 0 0 0 1 1 1 1 6 8 7 4 3 1 35 1968 0 0 0 1 1 1 1 6 8 7 4 3 1 35 1968 0 0 0 1 1 1 1 6 8 7 4 3 1 35 1968 0 0 0 1 1 1 1 6 8 7 4 3 1 35 1968 0 0 0 0 1 1 1 1 6 8 7 4 3 1 35 1969 1 0 1 1 0 0 0 3 4 3 2 1 19 1970 0 1 0 1 2 0 6 4 5 4 5 2 3 30 1971 1 0 2 1 1 1 1 6 8 7 4 3 1 35 1969 1 0 1 1 1 0 0 0 3 4 3 3 6 4 0 27 1969 1 0 1 1 1 0 0 0 3 4 3 3 2 1 19 1970 0 1 1 0 1 1 4 4 4 5 5 4 5 2 3 30 1973 0 0 0 0 0 1 1 1 1 1 5 6 5 4 6 4 5 2 3 30 1974 1 0 0 0 0 1 3 4 2 8 4 6 4 5 4 0 24 1971 1 0 0 0 0 1 3 4 5 5 5 3 0 20 1975 1 0 0 0 0 0 0 0 2 2 2 7 7 5 2 4 3 0 21 1977 0 0 0 1 0 0 0 0 2 2 4 5 5 3 0 20 1978 1 0 0 1 1 0 0 0 2 2 4 5 5 5 3 0 20 1978 1 0 0 1 1 0 0 0 1 2 4 5 5 5 3 0 20 1978 1 0 0 0 1 0 0 1 0 3 4 7 5 4 2 2 1 19 1979 1970 0 0 1 0 0 1 0 0 0 2 2 4 5 5 5 3 0 20 1977 0 0 0 1 0 0 0 0 0 2 2 4 5 5 5 3 0 20 1978 1 0 0 0 1 0 0 4 2 7 3 2 2 2 4 1981 0 0 0 1 1 1 1 0 4 2 7 3 2 2 2 1981 1999 1 0 0 1 1 0 0 4 2 7 3 2 2 2 2 4 4 5 5 5 3 1 1 2 2 5 1978 1 0 0 0 1 1 0 0 4 2 7 3 2 2 2 2 4 4 5 5 5 3 1 1 2 2 5 1978 1 0 0 0 1 1 0 0 4 2 7 3 2 2 2 2 4 4 5 5 5 3 1 1 2 2 5 1978 1 0 0 0 1 1 0 0 4 2 7 3 2 2 2 2 4 4 5 5 5 3 1 1 2 2 5 1978 1 0 0 0 1 1 0 0 4 2 7 3 2 2 2 2 4 4 5 5 5 3 1 1 2 2 5 1978 1 0 0 0 1 1 0 0 3 4 7 5 5 4 3 0 28 1999 1 0 0 1 1 1 1 1 0 4 2 2 7 3 2 2 2 2 4 1 1981 0 0 0 1 1 1 1 1 0 4 2 2 7 3 2 2 2 4 1 1981 0 0 0 1 1 1 1 1 0 4 2 2 7 3 2 2 2 4 1 1981 0 0 0 1 1 1 1 1 0 4 2 2 7 3 2 2 2 4 1 1981 0 0 0 1 1 1 1 1 0 4 2 2 7 3 2 2 2 4 1 1981 0 0 0 1 1 1 1 1 0 4 2 2 7 3 3 2 2 2 7 5 2 8 660	TABLE 3-4.		-											
YEAR (1945-1958) JAN FEE MAR APR MAY JUN JUL AUG SEP OCT NOV DEC TOTAL (1945-1958) .4 .1 .4 .5 .8 1.3 3.0 3.9 4.1 3.3 2.7 1.1 21.6 1959 0 1 1 1 0 0 3 6 6 4 2 2 26 1960 0 0 0 1 1 3 3 10 3 4 1 1 27 1961 1 1 1 1 3 2 5 4 6 5 1 1 31 1962 0 1 0 1 2 0 6 7 3 5 5 0 3 25 1 1 3 3 3 2 1 1 3 4 3 5 5 0	111000 J 4.	FPFOII	NCV O	ድ ጥኮር	DTCNT	CTT()	MC AN	ועים רונ	DEI O ONIG	e DV M	OMME	ט מונת	מוהים	
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1966	1964	0	0	0	0	2	2	7	9	7	6	6	1	40
1967	1965	2	2	1	1	2	3	5	6	7	2	2	1	34
1968	1966	0	0	0	1	2	1		8	7	3	2	1	30
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1972	1970	0	1	0	0	0	2	2	6	4	5	4	0	24
1973	1971	1	0	1	3	4	2	8	4	6	4	2	0	35
1974	1972	1	0	0	0	1	3	6	5	4	5	2	3	30
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1977	1975			0						5	5			
1978	1976	1	1	0	2	2	2	4	4	5	1	1	2	25
1979	1977	0	0	1	0	0	1	4			4	2	1	19
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CASES 12 7 14 21 29 39 108 130 120 95 57 28 660	AVERAGE	.5	. 3	.6	.9	1.2	1.6	4.5	5.4	5.0	4.0	2.4	1.2	27.5
	CASES	12	7	14	21	29	39	108	130	120	95	57	28	660

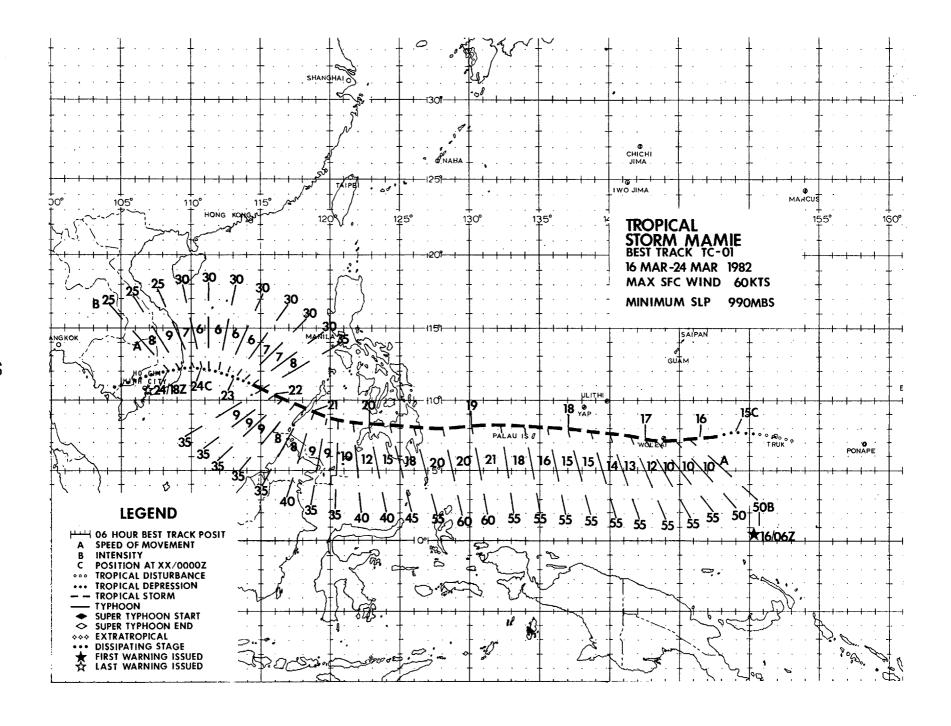
TABLE 3-5.				
		FORMATION ALERT	SUMMARY	
		WESTERN NORTH PA	ACIFIC	
YEAR	NUMBER OF ALERT SYSTEMS	ALERT SYSTEMS WHICH BECAME NUMBERED TROPICAL CYCLONES	TOTAL NUMBERED TROPICAL CYCLONES	DEVELOPMENT RATE
1972	41	29	32	71%
1973	26	22	. 23	85%
1974	35	30	36	86%
1975	34	25	25	74%
1976	34	25	25	74%
1977	26	20	21	77%
1978	32	27	32	84%
1979	27	23	28	85%
1980	37	28	28	76%
1981	29	28	29	97%
1982	36	26	28	72%
(1972-1982) AVERAGE	32.5	25.7	27.9	79%











Tropical Storm Mamie, the first tropical cyclone of the season, developed from an area of active convection which was first sighted on 7 March, near 150E and just south of the equator (Figure 3-01-1). During the next five days, this convective area was observed migrating northward as the near-equatorial trough set up south of 05N. By 12 March, the convective organization was sufficient to warrant discussion in the Significant Tropical Weather Advisory (ABEH PGTW). On 14 March, the first satellite fix located the developing disturbance approximately 104 nm (193 km) east-southeast of Truk Atoll (WMO 91344). As the disturbance tracked westward and was followed on satellite imagery, the available synoptic data indicated a relatively weak wind field with surface pressures near normal (1010 mb). However, because satellite imagery showed continued convective organization, a reconnaissance aircraft was sent on an investigative mission which proved to be very enlightening. Upon receipt of observed winds of 50 kt (26 m/sec) and evidence of a closed circulation from the reconnaissance data, the first warning on Tropical Storm Mamie was issued immediately (1606002). Mamie's intensities up to that point can only be extrapolated backwards; however, further intensification was very slow with the maximum intensity of 60 kt (31 m/sec) reached shortly before making landfall on Mindanao on 19 March.

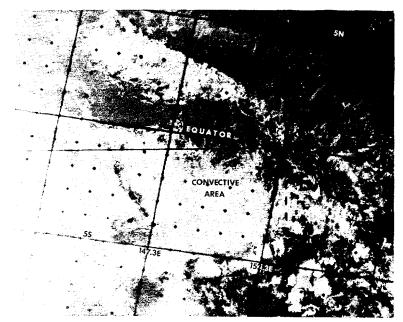


Figure 3-01-1. Satellite imagery shows an area of convection south of the equator which migrated northward and eventually became associated with the development of Tropical Storm Mamie, 0704307 March (NOAA 7 visual imagery).

From the first satellite fix to landfall on Mindanao, Mamie tracked westward along the southern periphery of a strong subtropical ridge (Figure 3-01-2). During this period, had it not been for satellite surveillance, Mamie may well have gone undetected until initial casualty reports were received from Mindanao (approximately 40 persons dead and extensive property and crop damage). Aside from winds received from the reconnaissance aircraft missions,

no other surface observations were received which indicated a well-organized circulation. Even upon landfall, Mamie was not detectable from the observations of local reporting stations. Fortunately, given Mamie's track and compact circulation (less than 90 nm (167 km)), both satellite and aircraft reconnaissance platforms were available and Mamie was tracked and monitored despite the paucity of reporting stations and ships in the Philippine Sea.

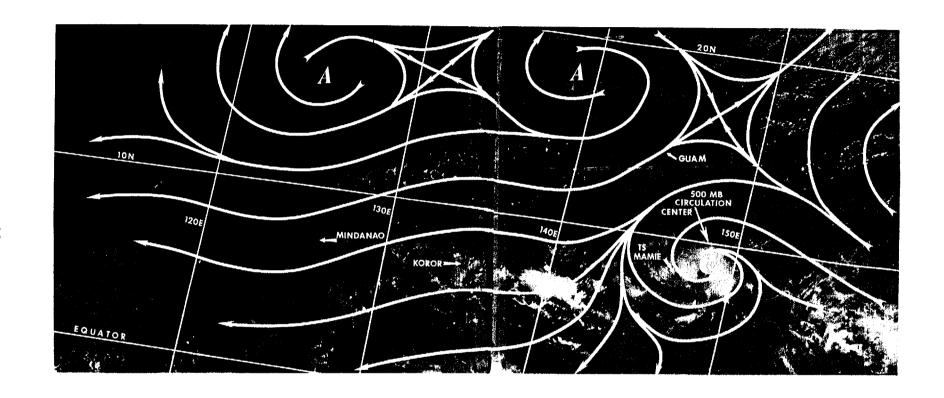
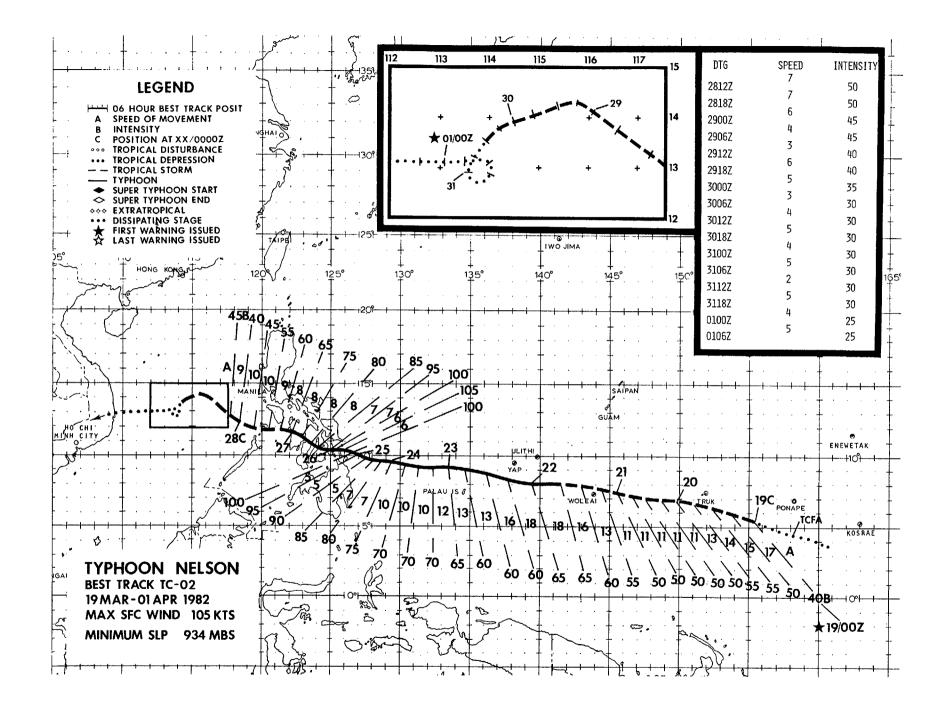


Figure 3-02-1. 500 mb streamline analysis for 1500007 March superimposed on a mosaic from visual satellite imagery. This figure depicts the steering influence of a strong subtropical ridge north of Tropical Storm Mamie. (1504367 and 1506187 March, NOAA 7 visual imagery).

On the second, and on subsequent reconnaissance aircraft missions, the Aerial Reconnaissance Weather Officers (ARWOs) observed an eyewall which was restricted to the lower levels. (Maximum observed height of the eyewall was near 10,000 ft (3048 m)). Due to Mamie's compactness and increasing vertical wind shear in the mid- and uppertropospheric levels, the eyewall did not fully develop and extend to heights that could be observed on satellite imagery. This failure to develop in the vertical contributed to Mamie not reaching typhoon strength.

After tracking across the northern portion of Mindanao, Mamie entered the Sulu Sea with winds of 40 kt (21 m/sec) and was unable to reintensify despite surface conditions which were generally favorable for reintensification. On 21 March, as Mamie reached the South China Sea, a weakness in the subtropical ridge allowed a more north-westward track which was maintained until approximately 230000Z, when the ridge strengthened and Mamie resumed a westward movement. At 241200Z, Mamie made final landfall near Nha Trang, Vietnam and then dissipated in the mountainous region to the west.



Typhoon Nelson was the second of three early season tropical cyclones in the western North Pacific which formed at very low latitudes southeast of Guam. Nelson, similar to Mamie (01), was a well-behaved tropical cyclone which developed and tracked westward, south of a strong midtropospheric ridge (centered near 15N 150E and extending west-northwest toward Taiwan).

In the initial stages of development, Nelson intensified rapidly from a weak tropical disturbance to a full-fledged tropical storm. In fact, the Tropical Cyclone Formation Alert, which was issued just 10 hours before the first warning, was preceded and followed by satellite fixes (180900Z and 181800Z) which described very little convective organization. However, at 190615Z, a reconnaissance aircraft reported flight level (1500 ft (457 m)) winds of 66 kt (34 m/sec), surface winds of 50 kt (26 m/sec), and an extrapolated sea level pressure of 993 mb.

Nelson's rapid development was in response to a véry strong divergence field in the upper-troposphere located over the cyclone, where a 40 to 60 kt (21 to 31 m/sec) easterly jet branched to the northwest and southwest. However, while these strong easterlies remained near Nelson, further development was limited to minimal typhoon strength. During this entire period, Nelson moved rapidly westward at speeds reaching 18 kt (33 km/hr) on 22 April, after which a gradual slowing in forward speeds and further intensification followed. After maintaining intensities between 60 and 70 kt (31 to 36 m/sec) for 60 hours, a change in the upper air patterns allowed Nelson to deepen rapidly, reaching 100 kt (51 m/sec) within 24 hours.

At 231200Z, while Nelson was moving away from the westernmost extent of the upper-tropospheric ridge (Figure 3-02-1), nearby westerlies aloft provided a strong outflow channel to the north and northeast.

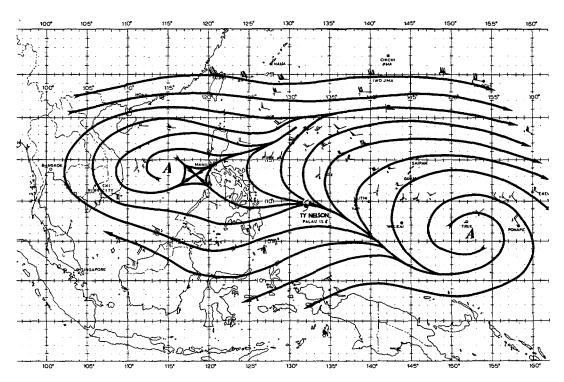


Figure 3-02-1. 200 mb analysis at 2312002 March. Note Typhoon Nelson's position just west of the westernmost portion of the ridge and the presence of a westerly current seven degrees north which will provide a good outflow channel.

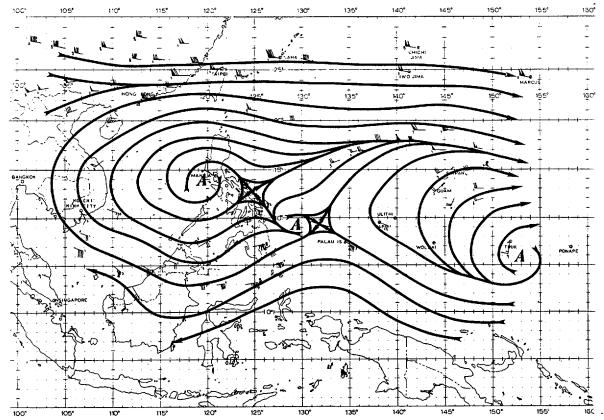


Figure 3-02-2. 200 mb analysis at 2400007 March. Within 12 hours an appreciable change in the upper-tropospheric levels has allowed the formation of an anticyclone aloft and the beginning of the good outflow channel into the westerlies.

As this occurred, an upper-level anticyclone was established (Figure 3-02-2) and intensified over Nelson; concurrently, Nelson responded and reached a maximum intensity of 105 kt (54 m/sec) at 251200Z (Figure 3-02-3).

On 27 March, a much weakened Tropical Storm Nelson entered the South China Sea after navigating through the south-central Philippines. On 28 March, Nelson briefly reintensified before weakening under the influence of vertical wind shear. Until

291200Z, the presence of a 500 mb short wave trough north of Nelson provided a favorable opportunity for recurvature toward the northeast. However, Nelson was quickly sheared and the low-level center meandered westward and eventually dissipated four days later. The fifty-third and final warning was issued at 010000Z April for Tropical Depression 02 (Nelson), approximately 240 nm (444 km) east of Nha Trang, Vietnam, near to the location where Tropical Storm Mamie (01) had made landfall one week earlier.

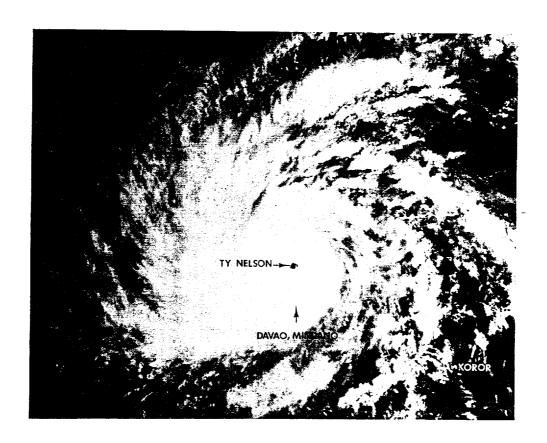
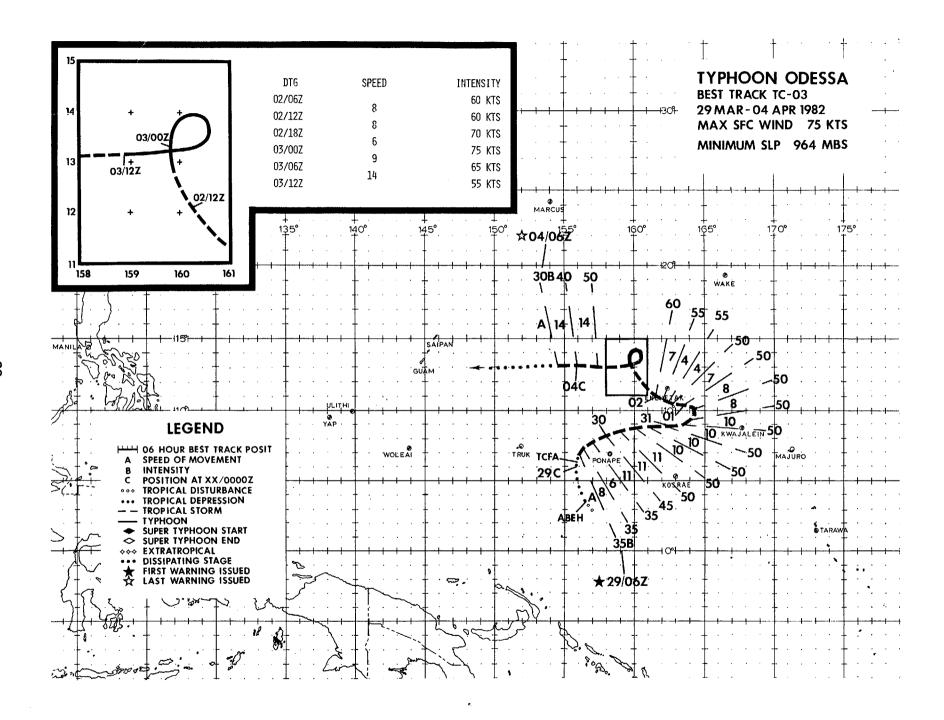


Figure 3-02-3. Typhoon Nelson near peak intensity, east of the Philippines. Note the anticyclonic flow aloft and the well-formed outflow channel to the north, 250601Z March. (NOAA 7 visual satellite imagery)



March is normally a relatively quiet month in the tropical western North Pacific, producing on the average less than one tropical cyclone per year. March 1982 was quite the contrary, with the genesis of three tropical cyclones taking place within a period of 13 days; 1967 was the most recent year with more than one tropical cyclone during March. Typhoon Nelson (02) and the subject of this report, Typhoon Odessa represent only the fifth and sixth typhoons to occur in March since the JTWC was established in 1959.

Just as March was a unique month in the level of tropical cyclone activity, Odessa was unique among the three tropical cyclones. As illustrated in Figure 3-03-1, tropical cyclones which develop near 160E tend to follow one of two climatological tracks: 60 percent move in a generally westward direction and 40 percent move in a generally northward direction. Although both Tropical Storm Mamie (01) and Typhoon Nelson (02) moved westward from this genesis area, Odessa's track defied climatology as it moved both eastward and westward across the area shown for northward-moving tropical cyclones.

Typhoon Odessa was initially detected as an area of loosely organized convection near 2N 159E on 26 March. In the following three days, a cloud system center emerged from these low-latitudes and moved northwestward. A Tropical Cyclone Formation Alert was issued at 2904002 upon receipt of reconnaissance aircraft data which indicated that a closed circulation had developed. As subsequent aircraft data and satellite imagery became available, it was evident that the circulation had rapidly organized and thus, at 2907412, the initial warning was issued for Odessa with maximum surface winds of 35 kt (18 m/sec)

Much of the remaining discussion will concentrate on the meteorological factors which influenced Odessa's atypical track. To facilitate this discussion, Odessa's best track has been divided into four segments (Figure 3-03-2) representing the different track directions of the tropical cyclone. Each of these segments can be explained quite well in post-analysis when largescale changes in the mid-latitudes at distances 600 to 1200 nm (1111 km to 2222 km) from Odessa are considered.

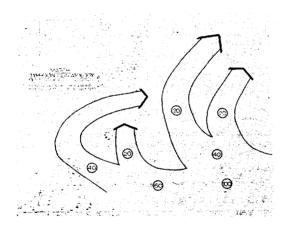


Figure 3-03-1. March Typhoon Climatology Tracks [IWW Special Study 105-8 March 1970]

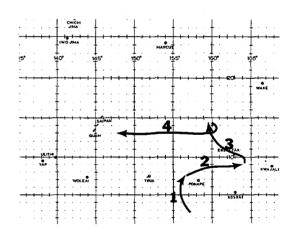


Figure 3-03-2. Typhoon Odessa's best track illustrating the four segments of Odessa's track as discussed in the text.

Odessa's initial movement to the northwest was in response to a weakening of the subtropical ridge northeast of Guam and the rapid cyclogenesis which was occurring southeast of Japan. The first three forecasts described a short-term northwestward movement followed by a more pronounced westward track. However, the continued deteri-oration of the subtropical ridge, north of Odessa, essentially removed any easterly steering current capable of driving Odessa westward. During the same period, a major high pressure system moved southeastward from Japan and strengthened the low-level northeasterly wind regime west of Odessa. Conventional surface data, at 300000Z, show this ridging extended deep into the tropics and created an effective block to any continued northwestward advance by Odessa (Figure 3-03-3). At mid-tropospheric levels, rawinsonde data from Truk (WMO 91334), Ponape (WMO 91348) and Kwajalein (WMO 91366) indicated that the base of a mid-latitude trough extended well into the tropics and south of Odessa. Although the axis of this trough was located well northeast of Odessa, between 160E and 165E (500 mb), its influence on Odessa's movement became obvious in the days that followed.

On 30 and 31 March, as Odessa tracked eastward at 10 to 11 kt (19 to 20 km/hr), the mid-latitude trough advanced more rapidly eastward and was located near 170E at 310000Z. Odessa, now 400 nm (741 km) west of the trough axis, began to slow and eventually turn toward the north. As Odessa approached 10N, it turned west-northwestward in response to a weak subtropical ridge filling in behind the mid-latitude trough

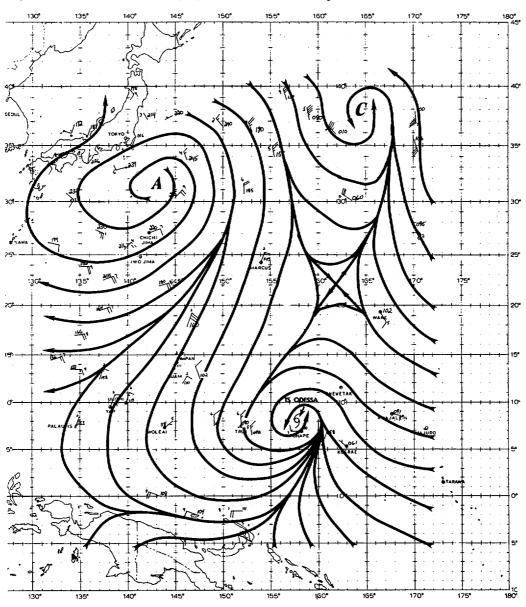


Figure 3-03-3. The 3000007 March 1982 surface/gradient level wind data and streamline analysis. Wind speeds are in knots.

(which had stalled near 175E). To this point, Odessa had maintained an intensity near 50 kt (26 m/sec) as westerlies restricted the development of the cyclone's circulation. With the subtropical ridge in place, Odessa was able to develop a closed circulation in the mid-tropospheric levels and a noticeable intensification trend began which culminated with a peak intensity of 75 kt (39 m/sec) at 030000Z (Figure 3-03-4 shows Odessa just prior to reaching typhoon strength).

Just as Odessa reached maximum intensity, the last major directional change

commenced. On 3 April, Odessa was approaching a break in the subtropical ridge, along 158E. Forecasts described a track northward around the ridge axis and then northeastward toward Wake Island. However, strong midand upper-level southerly winds moved over Odessa and a rapid shearing of the major convective features to the northeast followed. At 030800Z, a reconnaissance aircraft located Odessa's low-level circulation center 90 nm (167 km) southwest of the closest convective activity. During the 24 hours that followed, Odessa weakened rapidly and was no longer detectable from satellite imagery after 0406002.

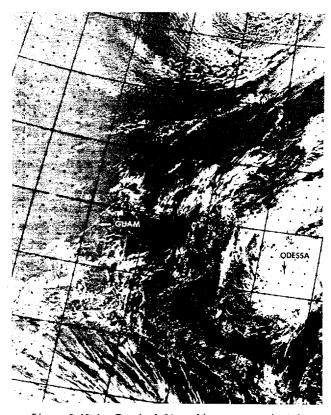
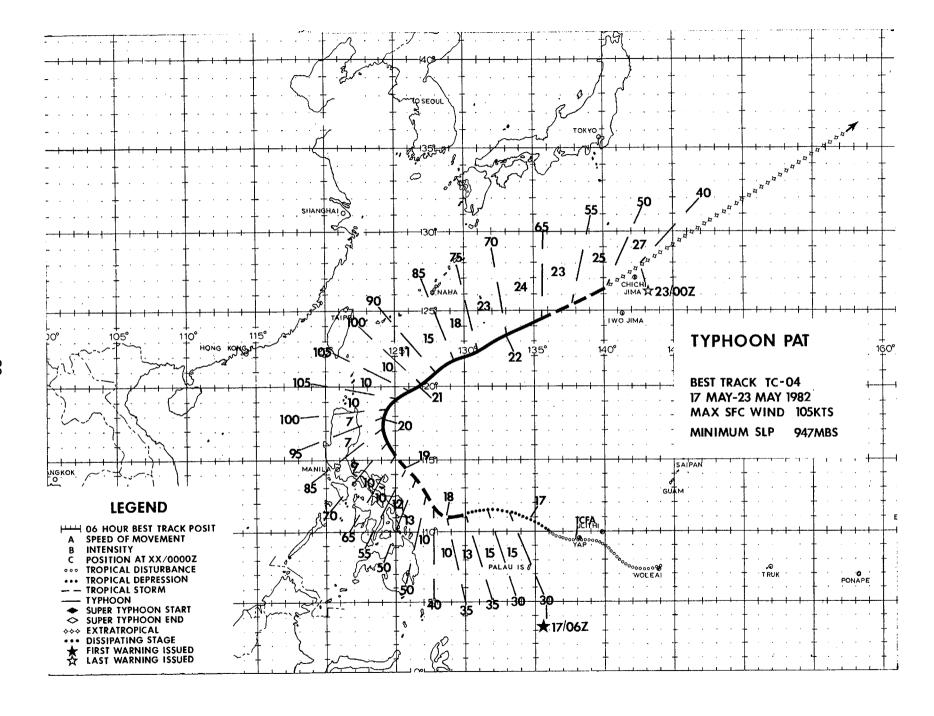


Figure 3-03-4. Tropical Storm Odessa, approximately 18 hours prior to reaching maximum intensity. At this time, Odessa was approximately 90 nm (167 km) west of Enewetak Atoll with maximum winds of 60 kt (31 m/sec). Note the cirrus streamers to the south, these originated from TC 17-82 (Bernie) in the Southern Hemisphere. Later, near 0300007, Bernie's expansive development would increase the southerly winds moving toward Odessa and aid in the shearing process which led to Odessa's dissipation. 0204257. April (NOAA 7 visual imagery).



The transition from the winter to the summer monsoon regime over the tropical western North Pacific can vary greatly from year to year. During this transition time (March through May), tropical cyclone activity can be very strong (six in 1980) or moderate (three in 1981). In May, 1982, there were several disturbances that developed in the near-equatorial trough and then dissipated without producing a significant tropical cyclone. During the third week of May, Typhoon Pat developed and became the only disturbance to reach warning status in the region between early April (Typhoon Odessa (03)) and late June (Typhoon Ruby (05)).

The disturbance that eventually produced Typhoon Pat was first detected as a mid-level circulation southwest of Guam. The 140000Z May 500 mb streamline analysis depicted a cyclonic circulation center near 8N 143E. Coincident with the analysis, satellite imagery indicated an area of centralized convection associated with the circulation. A Tropical Cyclone Formation Alert (TCFA) was issued at 140305Z when evidence of a strong upper-level circulation center was noticed on satellite

imagery. Aircraft reconnaissance at 140600Z reported no evidence of a surface circulation but did observe an area of strong low-level convergence near the convective disturbance.

It wasn't until the disturbance began moving out of the near-equatorial trough that a low-level circulation could be located by reconnaissance aircraft. On 17 May, another aircraft investigation located a closed circulation at 1500 ft (472 m) but surface winds were too light to determine a surface circulation center. The first warning on Pat, as Tropical Depression 04, was issued at 170600Z when sustained increased convective organization was observed on satellite imagery.

The forecast movement for the first six warnings projected Pat to move westward with passage over the Philippines, south of Luzon. This scenario was based on the existence of a mid-level (500 mb) ridge centered over the western portion of the South China Sea which was forecast to build eastward thus blocking northward movement of Typhoon Pat. During the ensuing 24-hour period, little change was evident in the mid-level ridge north and northwest of Pat (Figure 3-04-1). The

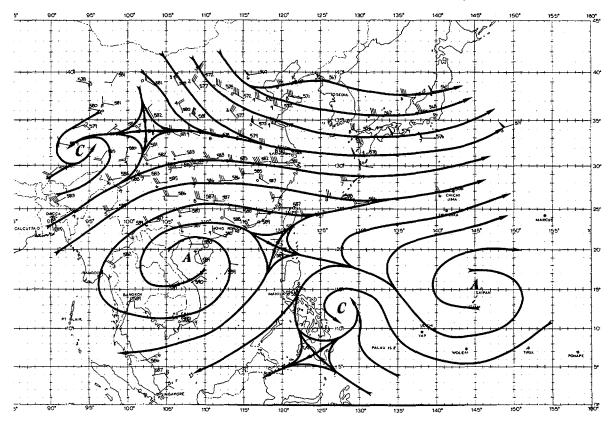


Figure 3-04-1. 500 mb streamline analysis at 1812007 May which shows Pat just south of an apparent weakness in the subtropical ridge. There had been no appreciable height - fall changes over a 24-hour period when Pat suddenly changed from a westward-moving to northward-moving tropical cyclone.

expected building of the ridge had not materialized; yet until 18 May, Pat persisted on its westward track. Then abruptly at 180600Z, Pat turned northward and paralleled the eastern portion of the Philippines for two days. Aircraft reconnaissance data at 180940Z provided the first indication of a possible track change, which was later confirmed by satellite fixes from Detachment 1, 1WW, Nimitz Hill, Guam and radar fixes from Cataduanes Island (WMO 98447). At 190000Z, upon evaluation of the fix data and a reevaluation of the westward track forecast scenario, JTWC changed the forecast track northward and toward eventual recurvature. From that point forward, Pat presented no further track forecasting problems.

Shortly after turning northward, Pat began to rapidly intensify, aided by a 200 mb wind maximum that had moved north of Pat and had enhanced outflow channels to the northeast. At 211200Z, Typhoon Pat reached its maximum intensity of 105 kt (54 m/sec) (Figure 3-04-2). This rapid intensification was not fully anticipated as Pat was forecast to only attain minimal typhoon strength. When aircraft reconnaissance data at 192233Z reported 95 kt (49 m/sec) surface winds, this new information was factored into the

next forecast which then called for Pat to attain maximum intensity within the ensuing 12 to 18 hours. Fortunately, Pat's increased intensity did not bring any destructive winds to the Philippines, previously hit by Tropical Storm Mamie (01) and Typhoon Nelson (02), despite approaches as close as 90 nm (167 km) to Cataduanes Island and eastern Luzon.

As Typhoon Pat approached 20N, a track toward the northeast became increasingly In recurvature, Pat began to favorable. accelerate in response to increasing midand upper-level westerly steering currents. A new method for forecasting the acceleration of northward-moving tropical cyclones, developed by JTWC personnel during the past year, was used to predict the point of initial acceleration as well as the rate of acceleration; Typhoon Acceleration Prediction Technique (TAPT) (Weir, 1982), utilizes 200 mb analysis data to determine possible future acceleration. First used on the 1912002 analysis data, TAPT accurately predicted acceleration to begin near 19N and gave excellent guidance on the speed of movement to 24N, where Pat slowed its forward speed and weakened from the effects of vertical wind shear on the system's organization.

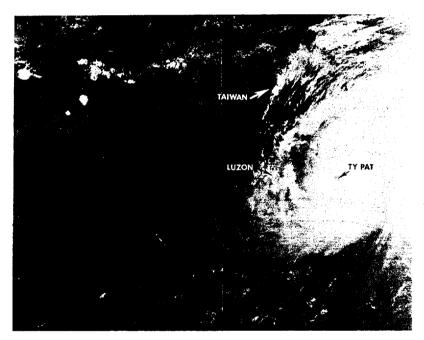
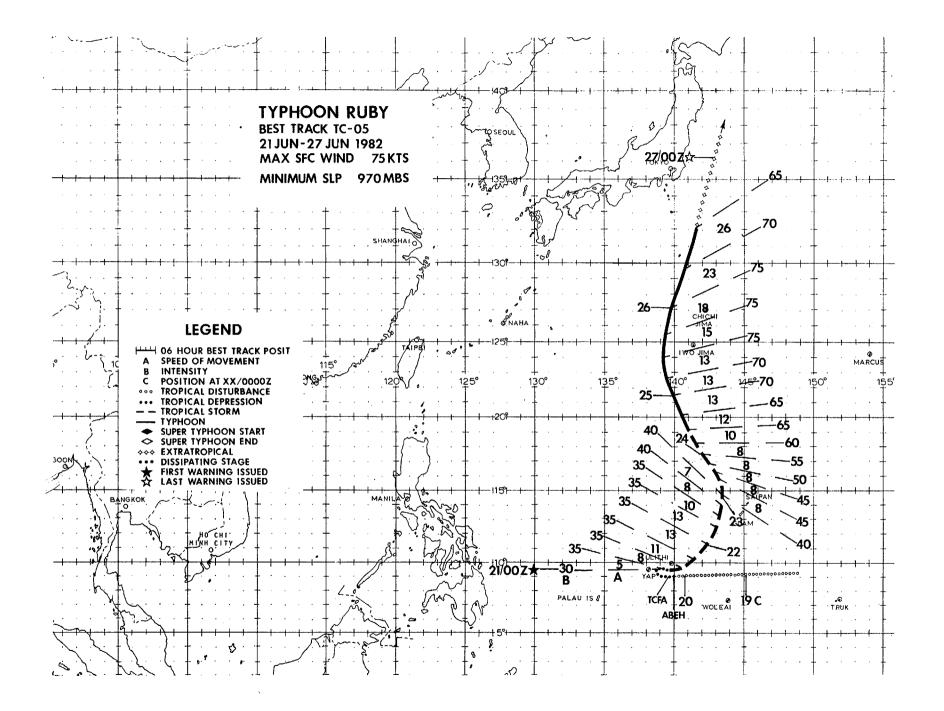


Figure 3-04-2. Typhoon Pat near maximum intensity of 105 kt (54 m/sec), 150 nm (278 km) east of Luzon, 200641Z May (NOAA 7 visual imagery).

On 22 May, as Typhoon Pat approached 24N, a weak frontal system (associated with an extratropical low east of Japan) was moving toward Pat and the first indications of Pat's eventual transition to an extratropical low were observed. Since 2116002, there had been a marked decrease in Pat's deep-layer convection; additionally, aircraft reconnaissance data at 220955Z indicated that the central sea level pressure had risen to 988 mb. Although observed winds were still near typhoon strength, the maximum winds were observed at distances much further from the center than in previous missions. These

expanding wind radii are frequently associated with tropical cyclones undergoing extratropical transition as the cyclone's energy source changes from latent heat release to a more baroclinic process. By 221200Z, synoptic data gave evidence of the incursion of cool, dry air into Pat's center and satellite imagery showed the system merging into a weak frontal boundary. Transition to an extratropical low was completed by 230000Z and this low gradually dissipated during the subsequent 24 hours as it was drawn into a stronger extratropical system, east of Japan.



Typhoon Ruby developed from a convective disturbance which was initially detected southeast of Guam on 18 June. During the first ten days of Ruby's development, its track and eventual extratropical transition were dramatically affected by several events which can be traced to fairly rapid changes in the upper-troposphere. These events will be discussed individually as they occurred during Ruby's lifespan; however, collectively, they illustrate the need for a better understanding of the upper-troposphere and its effects on subsequent tropical cyclone development and movement.

Satellite imagery, on 18 June, located a weak convective disturbance 320 nm (593 km) southeast of Guam. During the next 24 hours, this disturbance was observed tracking westward to near 145E where it weakened significantly while an upper-level anticyclone, previously supporting the convection, receded to a position east of 150E. On 20 June, a cloud cluster developed near 9N 141E and continued moving westward, south of Ulithi Atoll (WMO 91203). A Tropical Cyclone Formation Alert was issued upon receipt of Ulithi's 200600Z surface observation which reported a six-hour pressure fall

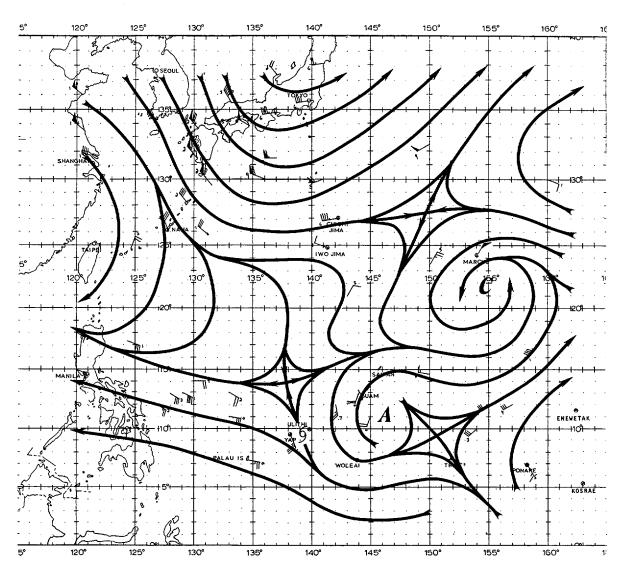


Figure 3-05-1. 210000Z June 1982, 200 mb streamline analysis. Ruby, positioned within a divergent southerly flow, was maintaining a central convective feature. To the north, a broad northerly flow was beginning to influence the near-storm environment. Wind speeds are in knots.

of 5 mb to 1004 mb, and a windshift from 030 degrees at 20 kt (10 m/sec) to 100 degrees at 25 kt (13 m/sec).

During the next 42 hours, satellite imagery and synoptic data indicated very little westward movement, with the system moving erratically between Yap and Ulithi. At 202339Z, the first aircraft reconnaissance mission into the system located a well-defined, very compact, 995 mb circulation center 45 nm (83 km) west-southwest of Ulithi. Based on these data, the first warning was issued for Tropical Storm Ruby at 210000Z with a forecast track toward the west-northwest. This forecast track was based on a very close agreement in most objective forecast aids. In fact, only the 700 mb and 850 mb steering aids, which indicated south-eastward low-level steering, did not support this initial forecast movement.

The apparent conflict between low-level and mid-level steering was seen as a reason for Ruby's erratic movement; but at that point, the long-term potential for a west-northwest-ward track looked good. At 2108302, an aircraft fix located Ruby 35 nm (65 km) scuth of Ulithi; this fix was in good agreement with Ulithi's 2106002 observation. Unfortunately, the 2106002 observation would be the last received from Ulithi for 24 hours. During the next 18 hours, fix positions from infrared satellite imagery showed Ruby moving northward, then northwestward, passing over Ulithi. Without sufficient synoptic data to the contrary, the next few warnings followed these satellite positions and maintained the forecast track toward the west-northwest.

However, on this first day in warning status, the upper-level wind regime near Ruby was changing. As depicted in Figure 3-05-1,

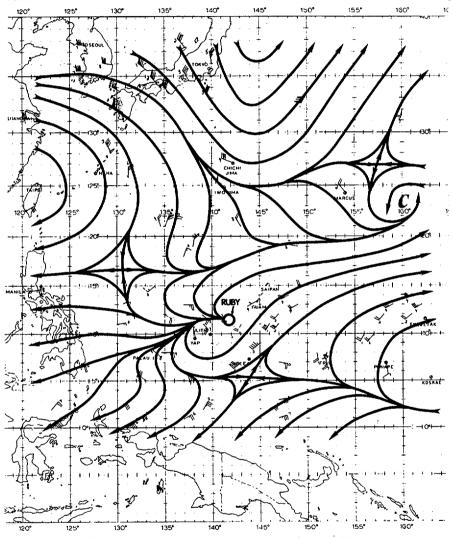


Figure 3-05-2. 2200002 June 1982, 200 mb streamline analysis. Considerable change has occurred in a 24-hour period. The northerly winds have penetrated to 10N, where the base of an upper-level trough formed. Coincident with this trough, a maximum cloud zone developed over the area south of Ruby's position and near-gale force winds were observed over a broad area at the surface and gradient levels near the upper-level trough/maximum cloud zone. Wind speeds are in knots.

the 200 mb winds at 210000Z were strongly divergent over Ruby but a broad mid-latitude trough, south of Japan, was introducing a significant northerly flow into the region. By 2200002, the 200 mb winds (see Figure 3-05-2) had changed and an upper-level trough had set up south of 10N, and south of Ruby. While this process was underway, the objective forecast aids - especially the tropical cyclone models - were predicting a return to a westward track while analyses data were indicating a strengthening of the monsoon flow, located southeast and southwest of Ruby. When the first visual satellite imagery became available on 22 July, a low-level circulation center was seen embedded in a maximum cloud zone which had developed over the monsoon flow. This circulation, presumed to be Ruby, was located near 11N 142E, or more than 200 nm (370 km) from the 210000Z warning position. The 220000Z warning was immediately amended and Guam, was issued. Interestingly, this amended warning had an exact 24-hour fore-cast position and only a 57 nm (106 km) error at 48-hours; but more importantly, a similar set of forecast errors could have been produced as early as 2106002 if the development of an upper-level trough and associated surge in the southwest monsoon

could have been predicted from the 2100002 upper-wind flow analysis. This northeastward movement has become a familiar pattern in years past when developing tropical cyclones become involved with an intensifying southwest monsoon. For recent examples, refer to past ATCRs describing Tropical Depression 16/Typhoon Orchid (1980), Tropical Storm Thelma/Typhoon Vernon (1980), Tropical Depression 11/Tropical Storm Phyllis (1981), and Typhoon Gay (1981).

As Ruby moved northeastward toward Guam, its intensity remained near 35 kt (18 m/sec). During this period, much of Ruby's circulation pattern was involved with the monsoonal flow and the strongest winds were observed within the maximum cloud zone associated with this flow. Not until 23 June, when Ruby turned northward and became a separate entity from this maximum cloud zone, did its surface pressures fall and intensity increase.

Although the best track might suggest a rather steady increase in both Ruby's intensity and speed of movement from 23 through 25 June, these days were marked by often conflicting fix data. For example, the 2404452 visual satellite imagery (refer to Figure 3-05-3) indicated an exposed low-level circulation center near 19N 142E, while a

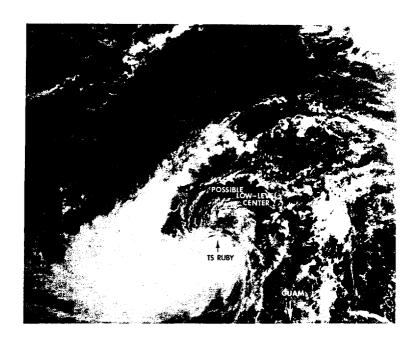


Figure 3-05-3. Visual satellite imagery suggested a low-level circulation center located in the northern periphery of the cloud system. This apparent low-level center was located well-north of a aircraft position received more than 3 hours later. 2404452 June 1982 (NOAA 7 visual satellite imagery).

reconnaissance aircraft surface/700 mb fix. at 240809Z, found a center nearly 60 nm (111 km) to the south. On 25 June, the 250630z and 250911z 700 mb aircraft fixes were positioned in a way to suggest either erratic movement or multiple circulation centers. These phenomena have been observed in other tropical cyclones which have emerged These phenomena have been observed from an active monsoon flow. Typhoon Orchid (1980) had a sufficient amount of satellite, aircraft and radar fixes to suggest a high speed looping pattern over a 30-hour period. Ruby's intensity during this period was equally hard to determine. Intensity estimates derived from visual satellite imagery (Dvorak, 1973) and minimum sea level pressures (Atkinson and Holliday, 1977) were normally separated by 15 to 25 kt (8 to 13 m/sec), with the pressure consistently lower than expected during this period. In postanalysis, both the track and the intensity trend have been smoothed by a careful reevaluation of the data during this period.

As Ruby moved north-northwestward, the potential for recurvature, significant acceleration and extratropical transition Based on a became increasingly important. series of evaluations from the 240000Z, 241200Z and 250000Z 200 mb charts, 24N was consistently identified as the best latitude for initial acceleration into the midlatitude westerlies (Typhoon Acceleration Prediction Technique (Weir, 1982)). A persistent and strong west-southwesterly 200 mb flow over Japan gave an indication for the potential of recurvature toward the northeast and, based on the mean latitudes of recent mid-latitude low pressure systems and ocean sea surface temperature fronts, 35N was deemed to be a favorable latitude for extratropical transition. Figure 3-05-4 depicts the 251200Z 200 mb flow with Typhoon Ruby near 24N. Within 18 hours, Ruby had assumed a north-northeastward track and accelerated to 23 kt (43 km/hr). The 2600007 200 mb analysis (Figure 3-05-5)

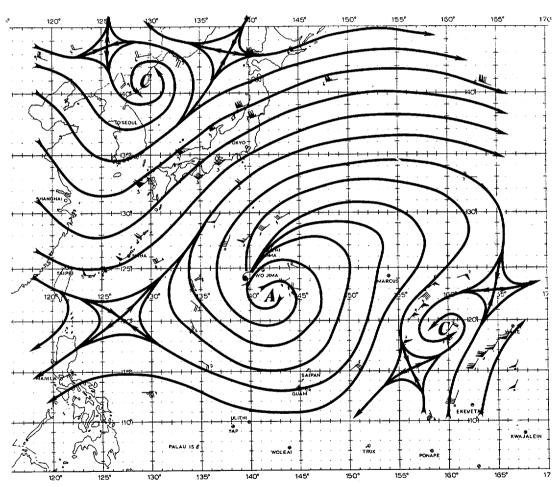


Figure 3-05-4. 2512007 June 1982, 200 mb streamline analysis. Typhoon Ruby was becoming involved with the upper-level mid-latitude westerlies. Wind speeds are in knots.

showed a dramatic change in the upper-wind pattern over Japan; 200 mb winds had become south-southeasterly and thus, signalled the potential for a more northward track. However, visual satellite fixes indicated a continuing tendency toward the northeast and the northeast forecast track was maintained. The 260602Z reconnaissance aircraft fix located Ruby's low-level circulation center 70 nm (130 km) west of the 260600Z warning position and these data, along with the 200 mb winds, dictated an amended warning toward the north-northeast and passing just east of northern Honshu.

A similar shift in the 200 mb flow also occurred with Typhoon Thad (August, 1981)

and as Ruby approached the mid-latitude westerlies, the potential for such a shift was being closely monitored. Unlike Thad, Ruby quickly transitioned to an extratropical low and this movement and upper-wind shift may have been associated with that process more than any large-scale changes in the upper-troposphere.

The final tropical cyclone warning for Ruby was issued at 2700002, after the 262149Z aircraft fix data indicated a cold core low was present at 700 mb. As an extratropical low, Ruby continued to move toward the north and rapidly occluded, becoming nearly stationary east of Hokkaido for several days thereafter.

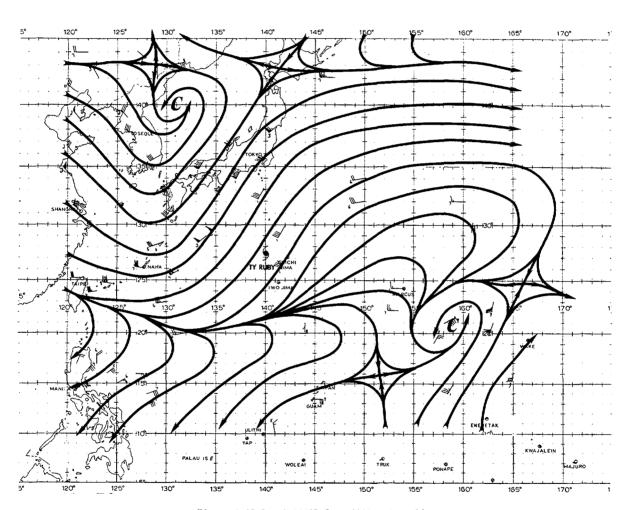
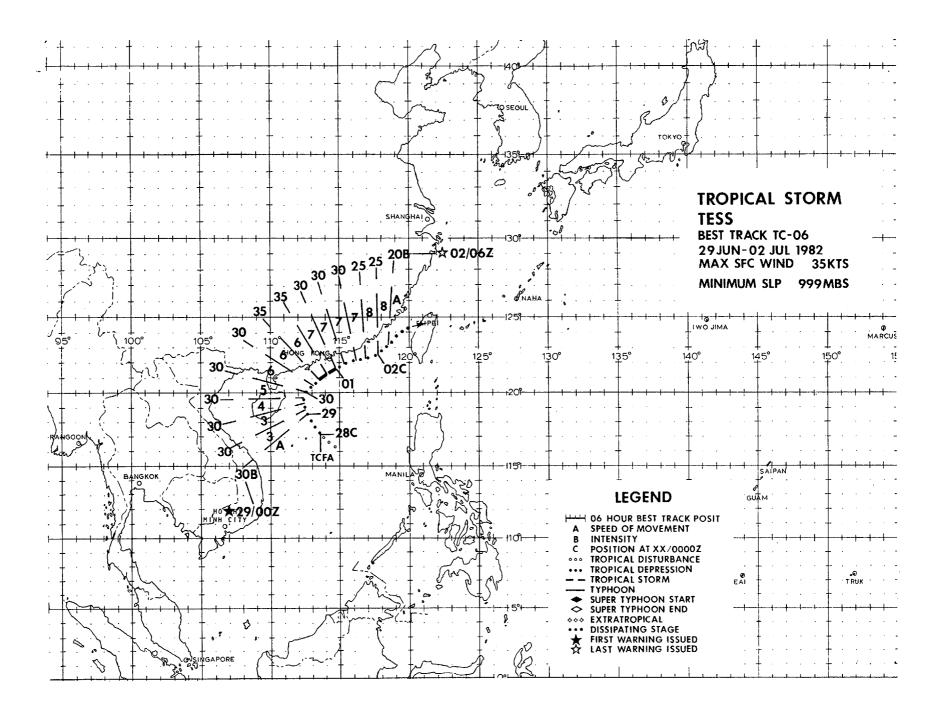


Figure 3-05-5. 2600007 June 1982, streamline analysis. Typhoon Ruby was well-embedded in the mid-latitude flow. Note the significant change in the 200 mb wind pattern over Japan in just 12 hours. This change, along with Ruby's rapid extratropical transition produced an extended north-northeastward movement and not the northeastward track predicted earlier from the 200 mb flow depicted in Figure 3-05-4. Wind speeds are in knots.



The Tropical Storm Tess had its origins and much of its life cycle linked to a strong southwest monsoonal flow which was established over the South China Sea in late June. While low surface pressures and gale force winds generally prevailed over a majority of the region, a disturbance could not be detected until 27 June, when synoptic reports indicated the development of a weak low-level circulation. At the point of initial detection, the nearest area of significant convection was located more than 200 nm (370 km) to the northwest of the circulation. A Tropical Cyclone Formation Alert was issued at 272330Z when it had become apparent that a zone of lower surface pressures (< 1002 mb) was aligning itself in close proximity to the disturbance.

During the subsequent 24-hour period, there was an increase in convective activity within the formation alert area and satellite imagery suggested an increase in convective organization. Although still lacking evidence of vertical alignment, the trends toward lower surface pressures and increased convection

prompted the issuance of the initial warning for Tropical Depression 06 at 290000Z.

From 28 to 30 June, Tropical Depression 06 tracked northward without any further evidence of convective organization. On 30 June, the depression turned east-northeastward and paralleled the coast of China. During this period, the southwest monsoon had abated somewhat and several weak circulations (eddies) became evident on satellite imagery (Figure 3-06-1). However, as the system passed south of Hong Kong, synoptic reports indicated that near-gale and gale force winds were present close to Tropical Depression 06. Thus, on the 010000Z July warning, Tropical Depression 06 was upgraded to Tropical Storm Tess. Post-analysis of this period indicates that Tess probably only attained tropical storm strength for a relatively short period (3012002 to 3018002).

On 1 and 2 July, surface synoptic data indicated a marked decrease in wind velocities in the area and thereafter, the remants of Tess gradually dissipated as it approached the Formosa Strait.

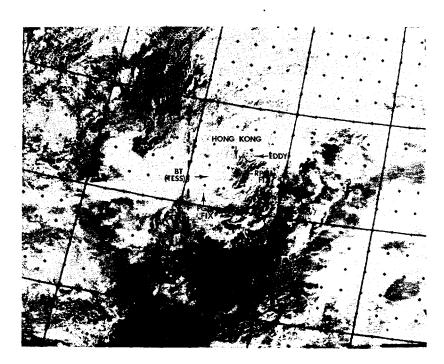
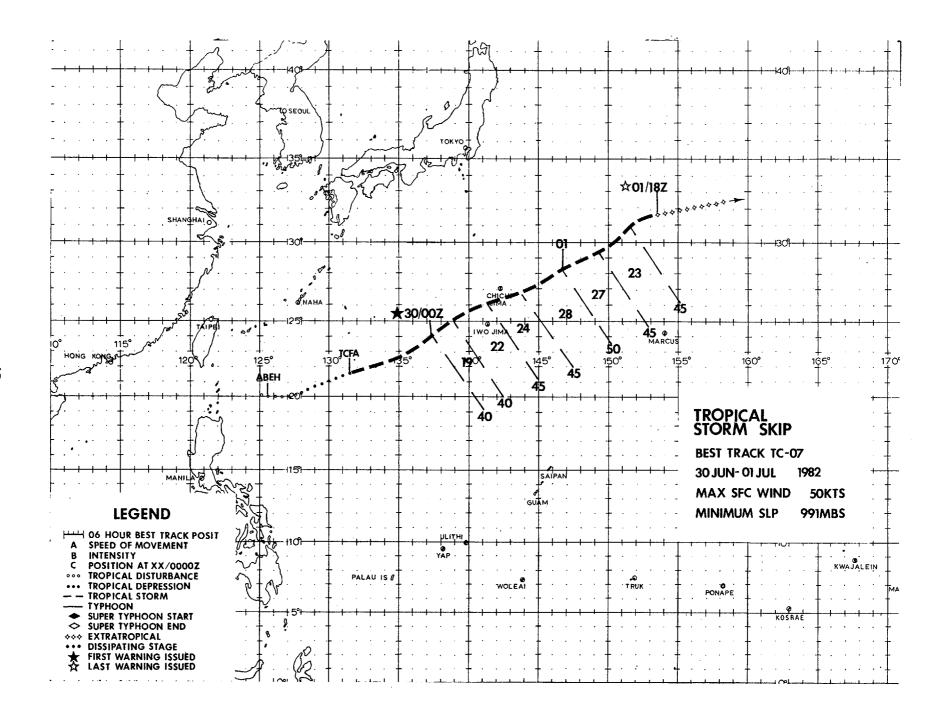
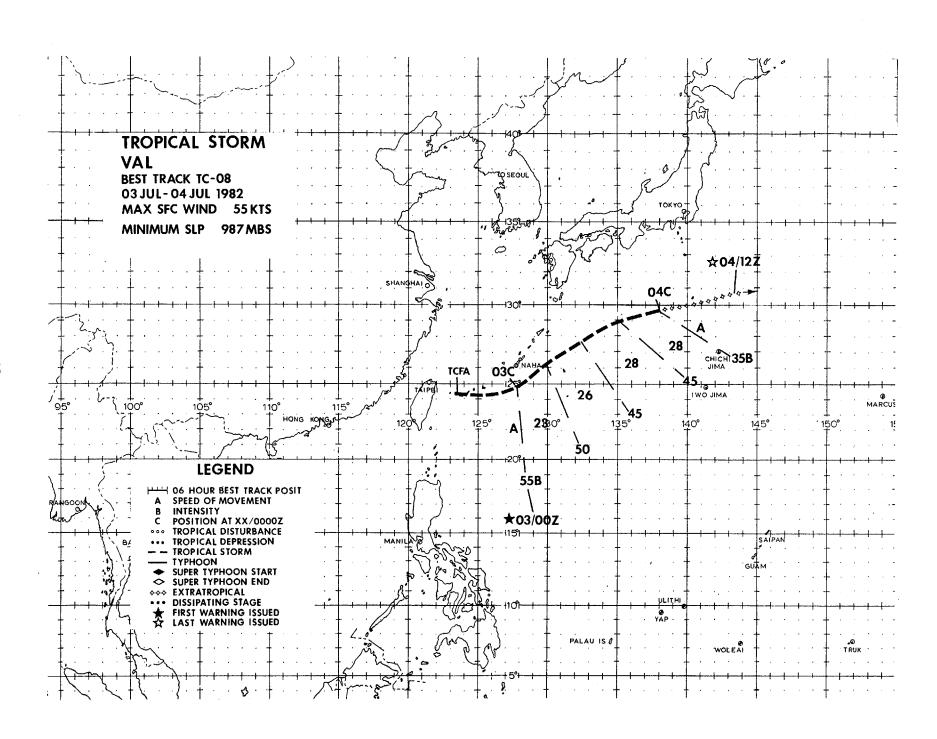


Figure 3-06-1. Satellite imagery shows several low-level eddies far removed from the central convective mass. Fix positions supplied from Detachment 5, 1WW, Clark AB, RP (RPMK) and from Detachment 1, 1WW, Nimitz Hill, Guam (PGTW) differ considerably in determining which eddy is the developing Tropical Storm Tess. The final best track position at fix time is shown as BT. 3006562 June (NOAA 7 visual imagery)





Each tropical cyclone season sees a few circulations develop near the mid-latitudes which appear to have both tropical and extratropical characteristics. These "hybrid" or "subtropical" cyclones have long been known to the tropical forecaster. particular, an article by Herbert and Poteat (1975) describes several distinguishing characteristics that allow differentiation between tropical and subtropical systems based upon satellite imagery (Table 3-07-1). The week between 23 June and 5 July saw two such circulations, Tropical Storms Skip and Val, develop southeast of Taiwan. During their existence each of these relatively small and compact systems were observed to have several characteristics associated with non-tropical cyclones, e.g. very little deep-layer convection near the surface center, displacement of convective features poleward and eastward of the system center, and each remained entirely enveloped within a larger cloud system associated with the mid-latitude westerlies. Conversely, both aircraft and satellite reconnaissance data indicated some typical tropical characteristics, i.e. a sharp pressure gradient near the center, surface winds in excess of 45 kt (23 m/sec), warm central temperatures, and a small but uniquely tropical upper-level anticyclonic outflow pattern.

The origin of the first circulation, Tropical Storm Skip, was more tropical in nature. The disturbance was first detected near 20N 124E on 26 June when surface

synoptic data indicated the presence of a circulation that was subsequently apparent as an exposed low-level circulation on satellite imagery. Synoptically, a sharp trough existed between this area and Typhoon Ruby (05), which was in its initial phases of extratropical transition near 30N 130E. Although satellite imagery indicated that frontogenesis had begun, it is unclear from the available data just how far south along the trough the front could be identified. To the west, an active monsoon trough, which was soon to spawn Tropical Storm Tess (06) in the South China Sea, had also begun to push into the area. During the next three days, winds in excess of 15 to 20 kt (8 to 10 m/sec) could be detected in the monsoon flow south of the circulation; however, very little organized convection could be detected near the vortex. In the upper-troposphere, westerlies penetrated as far south as 25N (at 500 mb) and 20N (at 200 mb) as the result of deep troughing behind the now extratropical Ruby. By 29 June the 200 mb flow began to ridge strongly along the trough boundary and 60 to 70 kt (31 to 36 m/sec) westerly winds to the north were soon accompanied by 65 kt (33 m/sec) northeasterly winds south of the trough. This resulted in an extensive cloud band more than 500 nm (926 km) wide along this entire region. A Tropical Cyclone Formation Alert (TCFA) was issued at 2905002 when a small upper-level anticyclone appeared to be developing in the vicinity of the low-level circulation (Figure 3-07-1).

TABLE	3-07-1.	SUBTROPICAL	AND	TROPICAL.	CYCLONES
THDUE	3-01-1-	PODITOLICATI	MIND	INOLICHE	CICHOHDD

A. DETERMINING TYPE

SUBTROPICAL TROPICAL Equatorward & eastward Poleward & eastward 1. Main convection from center from center Width 15° latitude Width usually less than 2. Cloud system size 10° latitude or more Convective cloud Cloud system becomes 3. Interaction with isolated system remains environment. connected to other synoptic systems (Some cold lows excepted)

B. DETERMINING ORIGIN

- 1. Frontal band typical cloud structure
- 2. East of upper trough amorphous convective cloud mass
- 3. Cold low circular cloud pattern with limited convection near center

(From Herbert and Poteat, 1975)

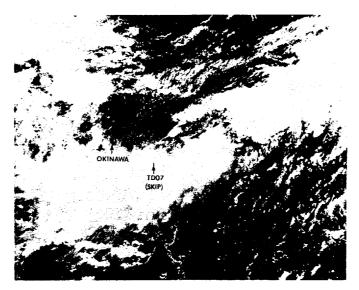


Figure 3-07-1. A developing low-level circulation can be detected within the confines of a broad large-scale cloud pattern. Weak upper-level outflow can be detected at 2905267 June (NOAA 7 visual imagery).

An aircraft investigative mission on 30 June located a 991 mb center with surface winds of 45 kt (23 m/sec), prompting the first warning to be issued at 300000Z. During the next 36 hours, Skip moved quickly northeastward along the frontal trough, averaging over 24 kt (44 km/hr), however its convection remained weak and generally restricted to within 120 nm (222 km) of its northern and eastern sides (Figure 3-07-2). Throughout Skip's lifetime, the Aerial

Reconnaissance Weather Officers (ARWOs) consistently reported very little convection near the center, rather large light and variable wind centers, and an abundance of stratocumulus entrainment. By 011600Z July, all convection had dissipated from the vicinity of Skip's center and the upperlevel anticyclone was no longer visible, indicating that the storm had completed its extratropical transition.

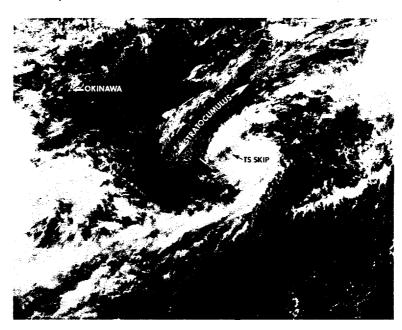


Figure 3-07-2. Tropical Storm Ship's exposed low-level circulation can be seen at 300514Z June to the south and west of its major convective area. Note the extent of stratocumulus to the north of this system. (NOAA 7 visual imagery).

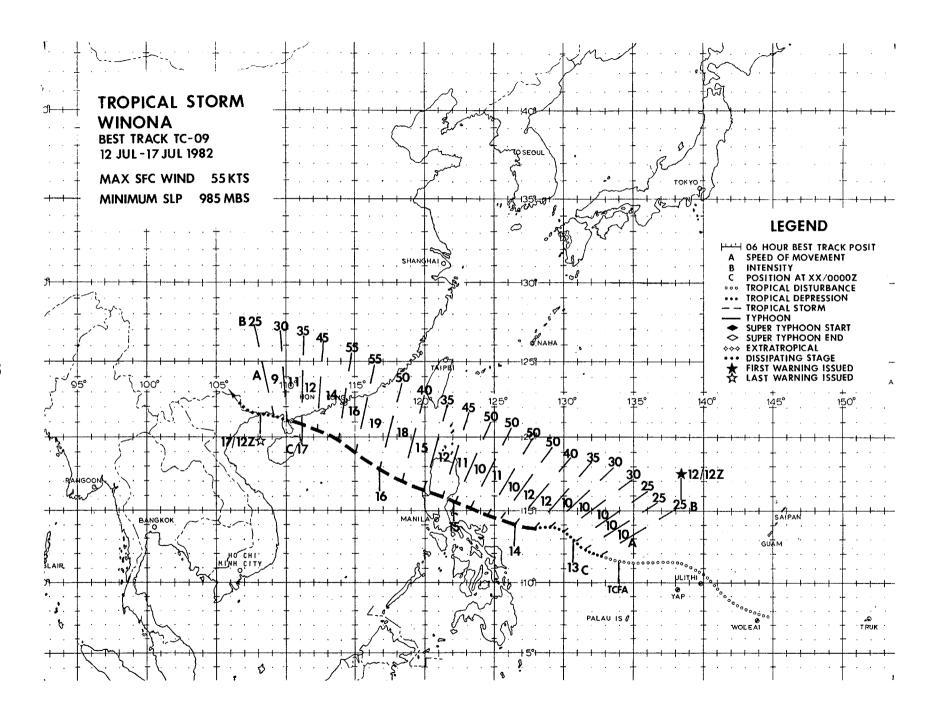
As Skip was moving rapidly toward the northeast, a new circulation could be identified from 1 July synoptic data, just east of Taiwan. At this time, the frontal east of Talwan. At this time, the trough ran westward from Skip into the vicinity of northern Talwan. Upper-level westerlies prevailed throughout the region although sharp ridging south of the 200 mb jet still maintained the large band of clouds. Isolated convection was present throughout this cloud mass, although none could be identified with the low-level circulation as it remained quasistationary. However, aircraft reconnaissance at 020115Z did identify a 995 mb center with winds up to 35 kt (18 m/sec) in the flow south of the circulation, thus a TCFA was issued. Convection finally began to develop near the circulation's center by 021200Z and, when the next aircraft mission found that the circulation had moved eastward and deepened to 987 mb, the first warning was issued at 030000Z. As was the case for Tropical Storm Skip, Val moved quickly northeastward along the trough, averaging over 26 kt (46 km/hr). Also like Skip, convection remained weakly organized and restricted to within 100 to 200 nm (185 to 370 km) of the system's center (mostly on the northern and eastern sides). As can be seen in Figure 3-07-3, Val still displayed its own individual outflow pattern despite being embedded within the larger cloud mass. By 040000Z, Val had lost all of its convection and could no longer be identified on satellite imagery as it completely merged into the frontal zone.

Both Tropical Storms Skip and Val contained many of the characteristics of subtropical cyclones identified in Table 3-07-1. Although monsoonal flow probably helped initiate Skip's low-level vortex, its further development and propagation can more likely be attributed to its position in relation to the eastern side of the upper trough. This is especially true of Val which formed farther north. Convection for both storms remained weak and unorganized and, partially due to strong westerly vertical shear, the low-level centers were often exposed with convection remaining poleward and eastward. Figures 3-07-2 and 3-07-3 show that each system did eventually become partially isolated from the dominance of the midlatitude westerlies and displayed their own anticyclonic outflow pattern.

Re-analysis of synoptic and satellite data revealed that Skip and Val were not the only circulations to develop during this unique period. At 300000Z, Skip (located near 24N 137E) could be seen flanked by circulations (or frontal waves) at 34N 153E, 31N 143E and 20N 125E. Similar conditions occurred for Tropical Storm Val as well. On the synoptic-scale each was only a small part of an extensive mass of clouds along the eastern boundary of a very active mid-latitude upper-level trough.



Figure 3-07-3. Tropical Storm Val's unorganized convection and outflow pattern can be seen with respect to larger frontal cloud mass pattern at 0317237 July. [NOAA 7 infrared imagery].



Tropical Storm Winona exemplifies tropical cyclone development without corresponding upper-level support. The presence of strong upper-level winds is often an inhibiting factor for significant tropical cyclone development. Based on JTWC's 200 mb synoptic data and streamline analyses, a strong subtropical ridge centered over central China was reinforcing strong upper-level winds over the Philippine Sea and South China Sea (See Figure 3-09-1). This situation persisted throughout Winona's warning period. The presence of 35 to 45 kt (17 to 23 m/sec) northeasterly winds in the upper-troposphere over Winona prevented the development of a strong anticyclonic outflow pattern and was a major factor in restricting further development to typhoon strength.

Winona's entire intensification process was slow. Between 10 and 12 July, three Tropical Cyclone Formation Alerts (TCFA) were issued as satellite imagery, synoptic and reconnaissance aircraft data revealed a persistent, but weak, disturbance moving westward through a primary tropical cyclone genesis region between Guam and the Republic of the Philippines. Reconnaissance aircraft investigative missions on the 10th and 11th found a weakly organized system with minimum sea level pressures of 1008 mb. At 1212002, synoptic data gave the first indication that the disturbance was intensifying as gradient-level winds reported by Yap (WMO 91413) increased to 25 kt (13 m/sec). Simultaneously, the 200 mb streamline analysis indicated the development of a weak anti-

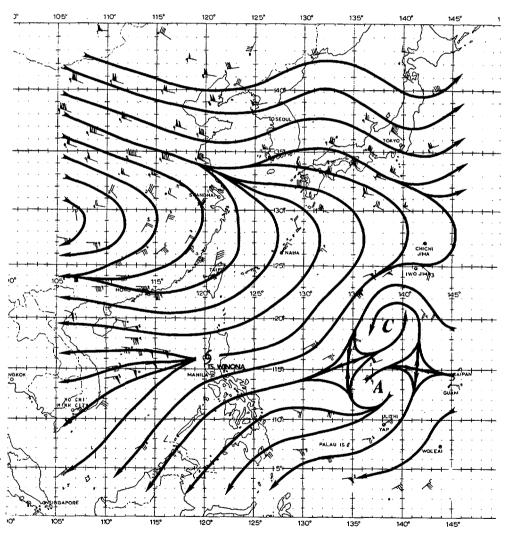


Figure 3-09-1. 200 mb streamline analysis at 1512007 July. Strong upper-level northeasterly winds prevent the development of outflow channels to the north.

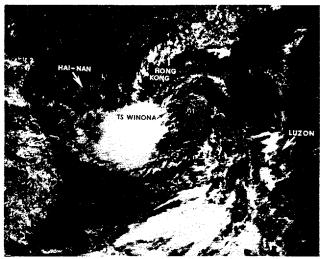


Figure 3-09-2. Tropical Storm Winona at 55 kt (28 m/sec) intensity, 400 nm (741 km) northwest of central Luzon. Even at maximum intensity, Winona's upper- and lower-level centers are not aligned due to the presence of strong upper-tropospheric winds. 1607077 (NOAA 7 visual imagery).

cyclone over the disturbance. This information, combined with increasing convection and organization (apparent on satellite imagery), prompted the issuance of the initial warning for Tropical Depression 09 at 121400Z. Subsequent aircraft reconnaissance at 130036Z confirmed JTWC's suspicions of intensification when it was reported that the minimum sea level pressure had dropped to 1000 mb.

From the initial warning, JTWC forecasts predicted that Winona would move into a region of strong upper-level winds which would inhibit its development. Thus, a maximum intensity of 50 kt (26 m/sec) was forecast prior to Winona's expected landfall upon central Luzon. Winona's intensity and movement were well-forecast during this period as it

proceeded west-northwestward along the southern periphery of the subtropical ridge, centered along 25N.

By 140600Z, Winona reached the forecast 50 kt (26 m/sec) intensity which it maintained until landfall on Luzon at 150500Z. As Winona crossed central Luzon, it passed 35 nm (65 km) north of Clark AB, where maximum sustained winds recorded were 23 kt (12 m/sec) with peak gusts to 30 kt (15 m/sec). Reported damage to the surrounding region was estimated at \$275,000 with 272 families left homeless as a result of severe flooding.

Winona entered the South China Sea as a minimal tropical storm, but upon reaching open waters, its convection increased and Winona reintensified to a peak intensity of 55 kt

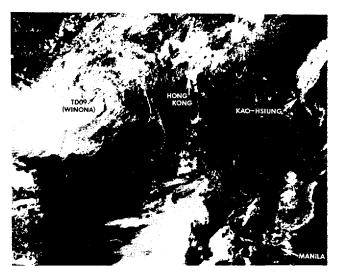


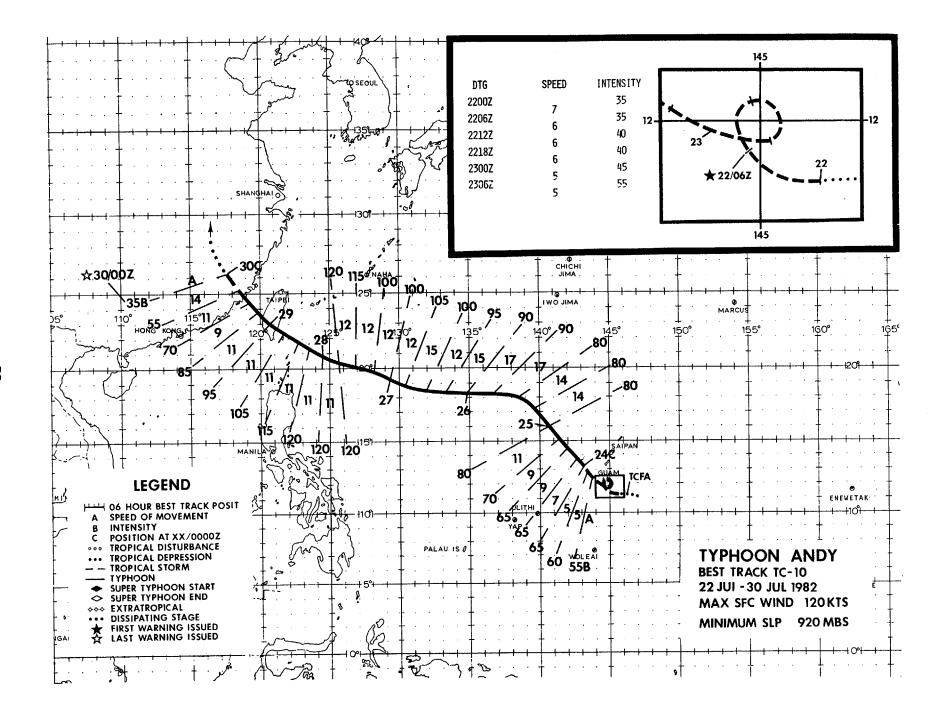
Figure 3-09-3. Winona after being downgraded to a tropical depression 210 nm (389 km) west-southwest of Hong Kong. Notice the persistent strong upper-level shear. 170655Z July (NOAA 7 visual imagery).

(28 m/sec) at 160600Z (Figure 3-09-2). This intensification occurred even though 40 kt (21 m/sec) 200 mb winds persisted over the area. However, based on limited 500 and 700 mb data, it appears that the strong winds did not extend into the mid-tropospheric levels. This situation allowed Winona's convection to develop well into the mid-tropospheric levels while the strong upper-level winds provided a sufficient outflow channel to the southwest.

Winona was forecast to move northward along the western periphery of the subtropical ridge upon entering the South China Sea. However, a 500 mb synoptic track completed by the 54th Weather Reconnaissance Squadron at 151200% showed that a second ridge had developed east of Taiwan, resulting in a steering flow over the South China Sea

toward the west-northwest. The 1518002 and subsequent forecasts reflected this new information and projected Winona on a west-northwestward track, with landfall expected southwest of Hong Kong.

After reaching maximum intensity on 16 July, Winona weakened as wind shear in the mid- and upper-layers increased. Winona became an exposed low-level system as its convective center was sheared to the southwest early on 17 July. By 170600Z, Winona was downgraded to a tropical depression as it passed 40 nm (74 km) north of Hai-Nan Island (See Figure 3-09-3). Further dissipation as a significant tropical cyclone occurred as it moved toward the China-Vietnam coastline on 18 July.



Andy formed on the northern edge of a zone of maximum cloudiness associated with the monsoon trough south of Guam. Prior to 22 July, the low-level westerlies were well established along 10N and extended eastward to the dateline. Satellite imagery on 20 July showed this maximum cloud zone had begun to segment. Within 24 hours the cloudiness consolidated into three distinct masses centered near 132E, 148E and 168E. Each cloud mass was poorly defined but had rudimentary banding features. The cloud system centers near 148E and 168E drifted westward, intensified, and became Typhoon Andy and Super Typhoon Bess (11) respectively. The cloud mass near 132E drifted westward and was disrupted by the combined effects of the rugged terrain over the Philippines and vertical wind shear from a tropical upper-tropospheric trough (TUTT).

A Tropical Cyclone Formation Alert (TCFA) was issued for the area south of Guam

at 2119002 due to significant pressure falls (to below 1004 mb), increased convection, and convective organization. Aircraft reconnaissance at 220229Z located a small, tight circulation center with a minimum sea level pressure of 995 mb. These data, along with observed winds of 35 to 40 kt (18 to 21 m/sec) prompted the issuance of the first warning. Although intensification was evident from 20 to 24 July on satellite imagery, the cloud pattern remained poorly defined and the circulation center was difficult to position—except for a brief period on 23 July, when the low-level center was visible on the satellite imagery. Aircraft reconnaissance was an invaluable asset during this period; no other reconnaissance platform was capable of following the low-level wind center, particularly since there was considerable interest on Guam as the fix data received implied an anticyclonic loop 35 nm (65 km) in diameter just 90 nm (167 km) south of the island.

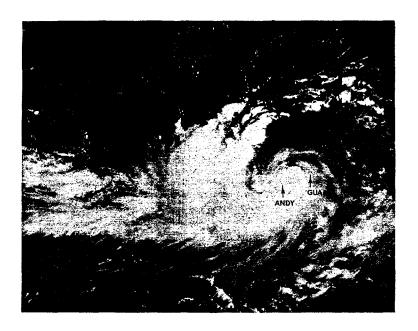


Figure 3-10-1. At 2405307 July Andy, shortly after reaching typhoon strength, is shown 125 nm (232 km) west of Guam (see arrow). During this time the strong south-westerly fetch south of Typhoon Andy brought phenomenal surf to Guam. (NOAA 7 visual imagery)

While Andy was undergoing the loop south of Guam, several meteorological factors were influencing the synoptic situation. Rawinsonde observations from Chichi Jima (WMO 47971) at 2212002 and 2300002 revealed 500 mb height falls of 10 to 20 meters. These falls indicated a weakening of the subtropical ridge north of Andy as well as a lessening of the steering current, factors probably accounting for Andy's lack of forward movement. In addition, reconnaissance aircraft consistently reported Andy's 700 mb center 10 to 20 nm (19 to 37 km) south of the surface center. This tilt, half of the diameter of the loop, suggests that Andy's

actual movement during this period might have been virtually nil, and may have been more related to the fix accuracies and the internal dynamics of the developing tropical cyclone. However, for best track purposes, this period is described well by the loop.

After completing the loop, Andy accelerated to the northwest and intensified. In Andy's wake, Guam experienced phenomenal surf on exposed southern and western beaches as a strong southwesterly fetch was brought to bear on the island on 24 July (See Figure 3-10-1). Andy's northwestward track turned abruptly toward the west as the cyclone

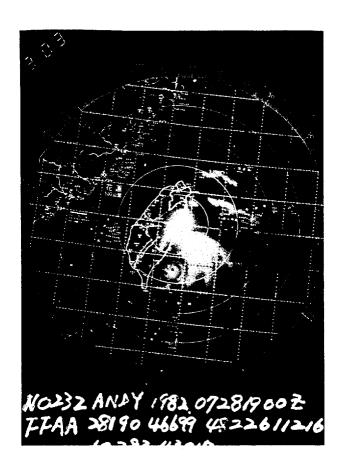
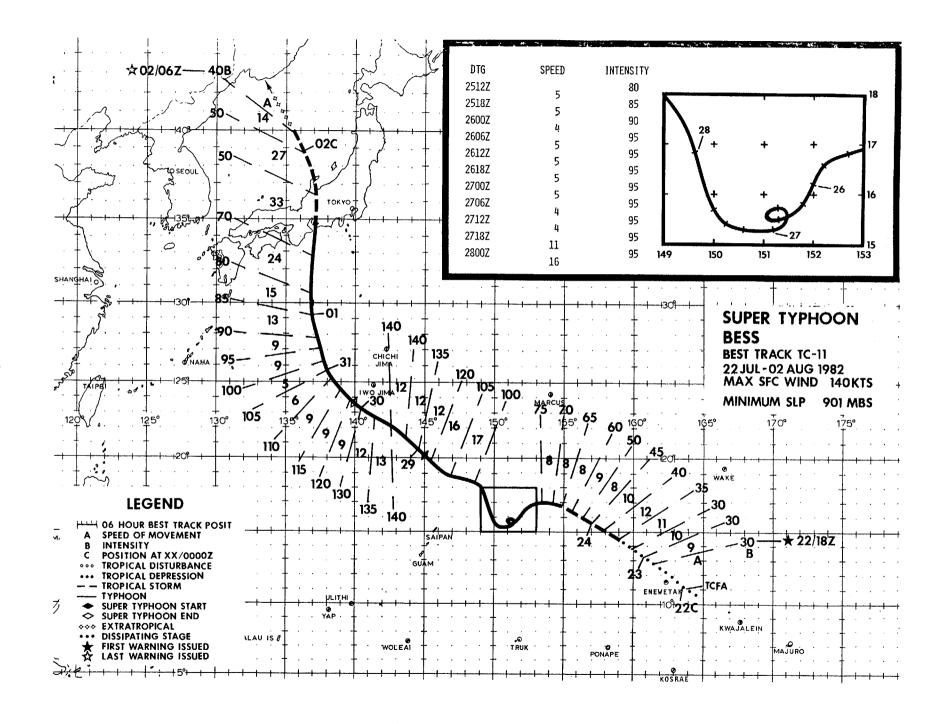


Figure 3-10-2. Typhoon Andy as seen by radar from Hua Lien (WMO 46699) at 281900Z July (Photograph courtesy of Central Weather Bureau, Taipei, Taiwan)

reached 18N on 25 July. This track change occurred while reported 500 mb heights rose at Chichi Jima, to the northeast of Andy. From this point onward, Andy remained equatorward of and parallelled the subtropical ridge axis.

While Andy was tracking westward, upperlevel outflow channels to the east (south of the TUTT axis) and to the southwest (return flow from the monsoon over southeast Asia) provided a favorable environment for intensification. At 2718002, Andy reached a maximum intensity of 120 kt (62 m/sec). Until making landfall upon the southern portion of Taiwan on 29 July (See Figure 3-10-2), Andy's intensity remained over 100 kt (51 m/sec). Taiwan experienced torrential rains from the typhoon's passage; especially hard hit was the eastern coastal area, where considerable damage from flooding was reported. Weakened from Taiwan's rugged terrain, Andy continued westward, across the Formosa Strait, and dissipated in the mountainous area of southeastern China on 30 July.



Bess formed at the eastern end of a maximum cloud zone associated with the monsoon trough anchored south of Guam. By 21 July, this area of cloudiness had separated into three masses near 132E, 148E, and 168E. The two easternmost cloud masses continued to develop and became Typhoon Andy (10) and Super Typhoon Bess. The third area dissipated over the Philippine Islands.

A Tropical Cyclone Formation Alert was issued for an area near 11N 165E at 211900Z. Observations from Kwajalein (WMO 91336) and Ailinglaplap (WMO 91367) showed that sea level pressures had continued to fall in the region, and satellite imagery indicated increased convection and organization in the cloud system.

The first warning, with maximum winds of 30 kt (15 m/sec), was issued at 2218002 when the curvature of loosely organized cloud bands into the central cloud mass increased. Initial forecasts for Bess indicated a track toward the northwest, in response to an east-southeasterly flow at low- and mid-levels. Reconnaissance aircraft missions during the period 2222002 to 2322002 indicated that the surface and 700 mb centers were not well-aligned vertically. Once this feature was eliminated, Bess began to intensify and by 2418002, it was upgraded to typhoon strength based upon satellite imagery which indicated a 30 nm (56 km) eye had developed.

Bess maintained its northwestward track for the first 48 hours in warning status. However, by 2418002 a noticeable decrease in the speed of movement was observed as Bess began to move toward the west-northwest. This change in motion was thought to be the result of westward building of the subtropical ridge to the north. Consequently, the forecast track was changed to a more westward heading. Contrary to JTWC expectations, Bess took a turn toward the southwest at 2512002. Subsequent analysis of satellite imagery indicates that a short wave trough had just passed to the north of the circulation. The enhanced northwesterly flow behind this

trough forced Bess toward the southwest. During this period, Bess slowed to 5 kt (9 km/hr) and completed a 20 nm (37 km) diameter cyclonic loop, while its intensity remained at 95 kt (49 m/sec). Further intensification did not occur and Bess remained on its southwestward track until another short wave trough moved eastward from Japan on 27 July. In response to this trough, Bess took a noticeable turn north-northwestward until 280600Z when Bess began moving toward the northwest along the southwestern extension of the subtropical ridge. While moving northwestward, a rapid intensification period began, culminating in the attainment of super typhoon strength and a peak intensity of 140 kt (72 m/sec) at 290600Z.

As Bess approached 25N, a decrease in forward movement was observed; numerical forecast fields and the JTWC 500 mb analysis of 30 June indicated a weakness forming in the subtropical ridge over the southern islands of Japan which would allow Bess to take a more northward track. As Bess entered the south-southeasterly flow associated with the western periphery of the subtropical ridge, interaction with the midlatitude westerlies was expected to occur within 36 hours and Bess was forecast to recurve along the southern coast of Japan. Bess, however, maintained a northward track. The Typhoon Acceleration Prediction Technique TAPT (Weir, 1982) was employed, and correctly forecast significant acceleration commencing near 28N. From this latitude, Bess did begin to accelerate toward the north and eventually merged with a low pressure center in the Sea of Japan on 02 August.

Bess passed over the Araumi Peninsula on central Honshu where extensive damage and human suffering were reported. The greatest damage was caused by torrential rainfall which set off 1,557 landslides and flooded over 27,000 homes, leaving 25,000 persons homeless, and 59 dead. More than 25 ships rain aground or were lost, over 100 bridges were washed out, and nearly 300 acres (741 hectares) of farmland were flooded.

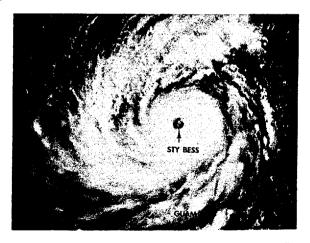
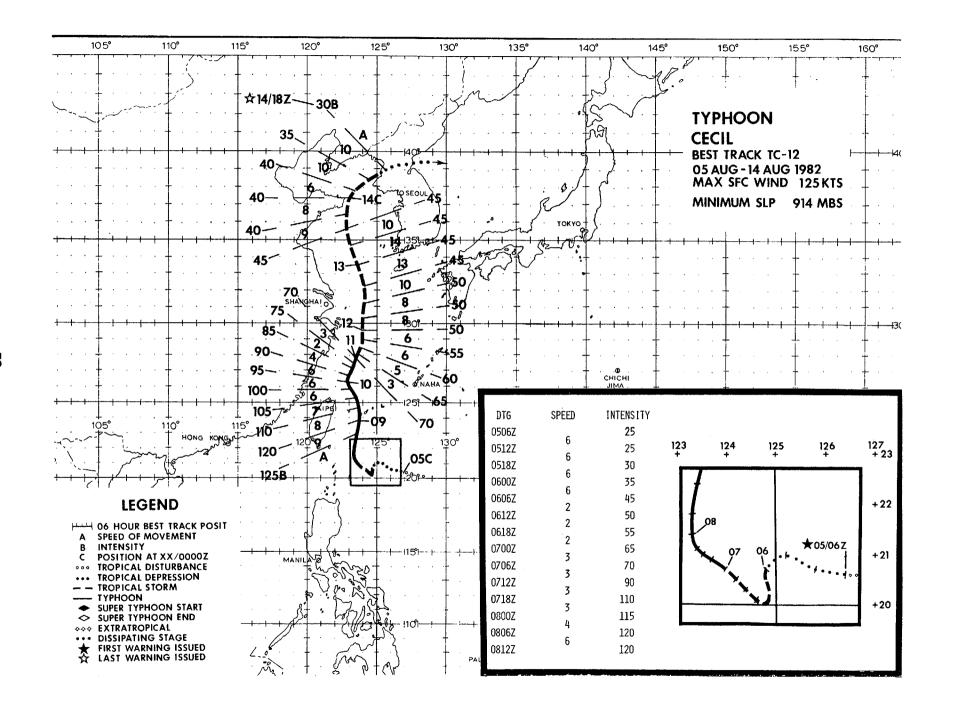


Figure 3-11-1. Super Typhoon Bess at maximum intensity. 290430Z August (NOAA 7 visual imagery).



The tropical disturbance which later became Typhoon Cecil was first distinguishable as a low-level circulation about 250 nm (463 km) north of Truk (WMO 91334) on 31 July. This disturbance persisted as a closed circulation on the surface streamline analyses and as an area of enhanced convective activity on satellite imagery that travelled westward along the monsoon trough for the next four days. Although mentioned in four consecutive Significant Tropical Weather Advisories (ABEH PGTW), a Tropical Cyclone Formation Alert (TCFA) was not issued on the system

during this period because a strong easterly flow at upper-levels was expected to inhibit development of the disturbance. Figure 3-12-1 is typical of the upper-level (200 mb) flow during this period. On 4 August, increased convective activity was apparent from satellite imagery, ship reports in the area indicated that central pressures had dropped to 1000-1003 mb and weakening of the upper-level easterlies was indicated by the 200 mb analysis data. When it became evident that the disturbance had indeed intensified, and that further intensification was likely, a TCFA was issued at 0414002.

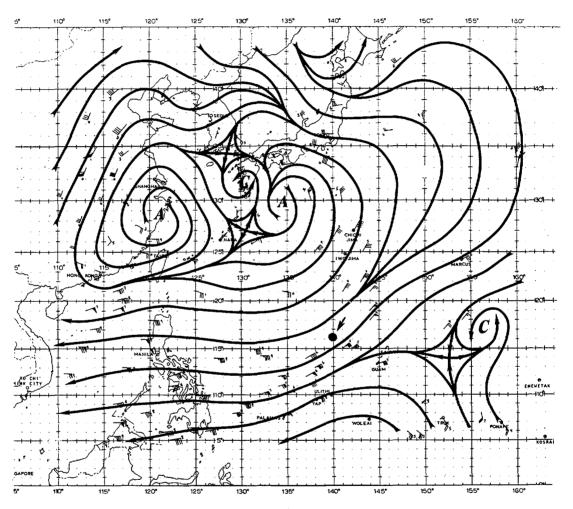


Figure 3-12-1. 030000Z August 200 mb streamline analysis. The location of the surface circulation is indicated by the dark circle.



Figure 3-12-2. 081838Z August (NOAA 7 infrared imagery).

The first warning on Tropical Depression 12 was issued at 050600Z after an aircraft reconnaissance mission observed sustained winds of 25 kt (13 m/sec) associated with the circulation. Tropical Depression 12 continued to track westward under the influence of easterly steering currents along the southern periphery of the subtropical ridge. Upgraded to tropical storm status on 6 August, Cecil turned southward, slowed to 3 kt (6 km/hr), and then turned northwestward. From 6 to 8 August, Cecil intensified from 35 kt (18 m/sec) to 115 kt (59 m/sec), reaching a peak intensity of 125 kt (64 m/sec) at 081800Z while located 120 nm (222 km) east of Taiwan (figures 3-12-2 and 3-12-3).

As Cecil approached Taiwan from the southeast, its track turned sharply northward until reaching 25N when Cecil once again assumed a more northwestward track. Although Cecil never approached closer than 80 nm (148 km) to Taiwan, heavy rains associated with its peripheral circulation touched off landslides which killed at least 19 people in Wu-Koo County, near Taipei.

On 10 August, Cecil turned toward the north-northeast and the combined effects of colder ocean temperatures, vertical wind shear, and copler surrounding air began to take their toll. Within three days after reaching maximum intensity, Cecil was downgraded to a tropical storm.

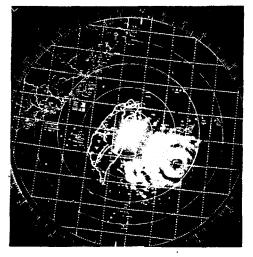


Figure 3-12-3. Typhoon Cecil as seen by radar from Hua Lien (WMO 46699) at 0819007 August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).

As a tropical storm, Cecil continued to move northward in response to steering from an extension of the subtropical ridge which had built northward into the Sea of Japan. The situation at 500 mb is illustrated by the 101200Z August 500 mb streamline analysis (Figure 3-12-4) which is typical of the mid-level synoptic pattern during Cecil's northward movement.

By 14 August, Cecil, located near 38N 124E, was beyond the northward influence of the subtropical ridge and entering an area of westerly flow. Cecil moved eastward in

response to its new environment and made landfall on Korea with 35 kt (18 m/sec) winds. Although, at this time, Cecil was a weak storm in terms of wind intensity, there was a great deal of precipitation associated with the circulation. Heaviest rains, 21.2 inches (55 cm), were recorded in Sanchong, resulting in severe flooding which left 35 dead, 28 missing, and 42 injured in addition to an estimated 30 million dollars in property damage. Cecil's circulation was unable to reorganize after crossing the Korean peninsula and dissipated in the Sea of Japan on 15 August.

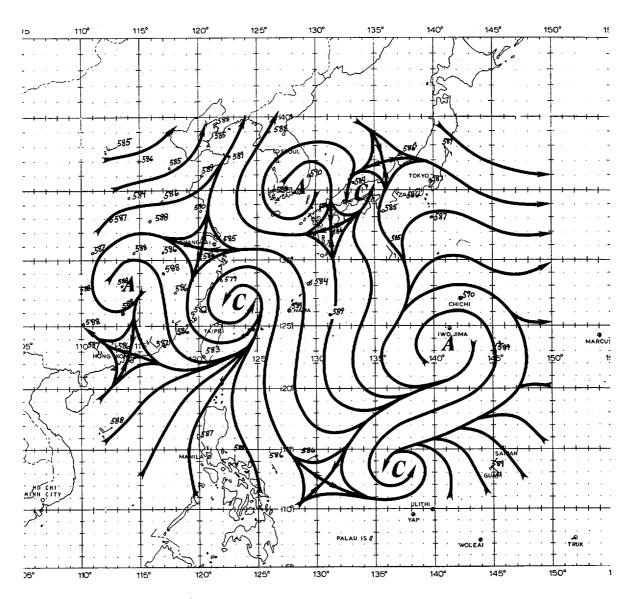
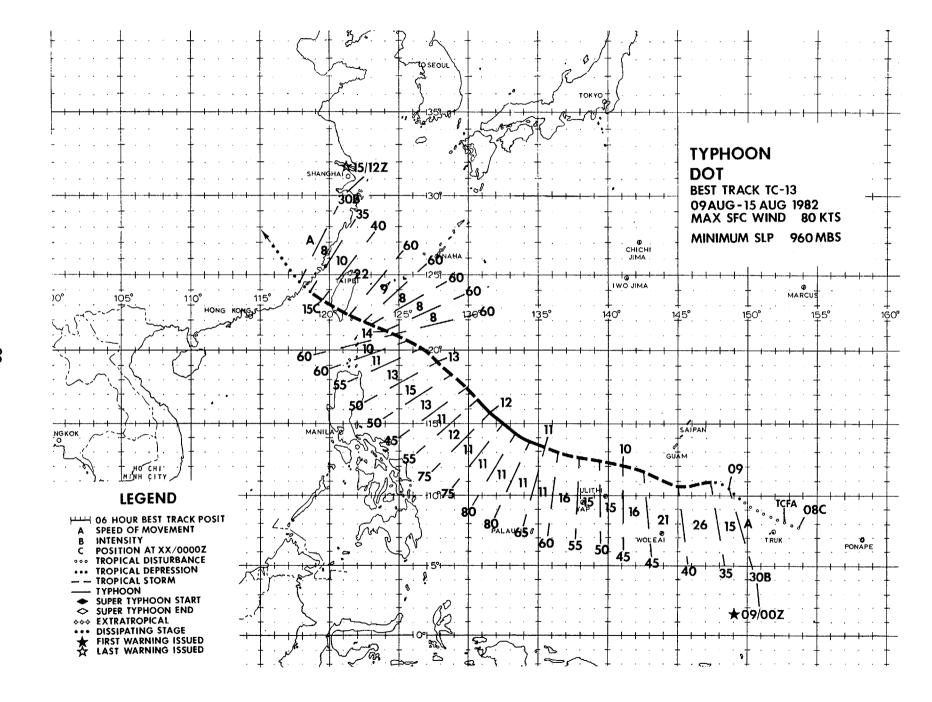


Figure 3-12-4. 101200Z August 500 mb streamline analysis.



The origins of Typhoon Dot can be traced back to a weak surface circulation located near Kwajelein (WMO 91366) on the 5th of August. Surface winds associated with this circulation were 5 to 10 kt (3 to 5 m/sec) and the minimum surface pressure was 1008 mb. Over the next two days, as the circulation drifted northwestward, it remained fairly weak with loosely organized convection and light winds. On 8 August, a reconnaissance aircraft mission into the area showed that the circulation had maximum sustained winds of 20 kt (10 m/sec) but that the surface circulation was still very broad with relatively unorganized convection. However, satellite imagery and 200 mb data indicated that an upper-level anticyclone was present in the area, although not vertically aligned with the surface center. A Tropical Cyclone Formation Alert (TCFA) was issued at 080500Z based upon the persistence of the system and the presence of upper-level conditions that could lead to intensification of the disturbance. The initial warning on Tropical Depression 13 was issued at 090000Z when satellite imagery indicated that the cloud pattern associated with the developing depression was becoming more organized along with increased convective activity.

A reconnaissance aircraft mission at 090118Z observed surface winds of 35 kt (18 m/sec) and an extrapolated minimum sea

level pressure of 1003 mb. Based on these data, Tropical Depression 13 was upgraded to Tropical Storm Dot at 090600Z. During this period, the subtropical ridge was well established to the north of the system; thus Dot was forecast to track westward and to continue to intensify. Dot lived up to these expectations, moving westward and reaching typhoon strength on 11 August. However, after reaching a maximum intensity of 80 kt (41 m/sec), Dot began to weaken as upper-level outflow channels became restricted due to interaction with Typhoon Cecil (12) located to the northwest. This interaction is easily seen on satellite imagery (Figure 3-13-1 shows the early stages of this interaction); at this time, Cecil was located northeast of Taiwan with maximum winds of 90 kt (46 m/sec) and Tropical Storm Dot, with maximum sustained winds of 50 kt (26 m/sec), was rapidly intensifying and would achieve maximum sustained winds of 80 kt (41 m/sec) on the following day. Although there was some interference in the upper-level outflow between the two cyclones, Dot's outflow channels to the northeast and southwest were well established. Figure 3-13-2 shows the relationship between the two cyclones two and one-half days later. Although the satellite pass was not optimally located, features of interest are readily observable, i.e., Dot's outflow channels to the north were completely cut off by the strong northeasterly winds associated with Cecil's outflow. The 200 mb analysis for

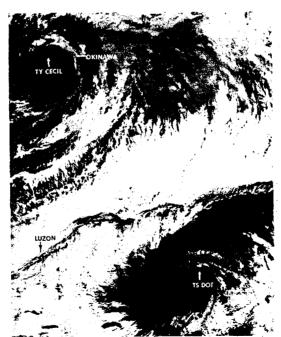
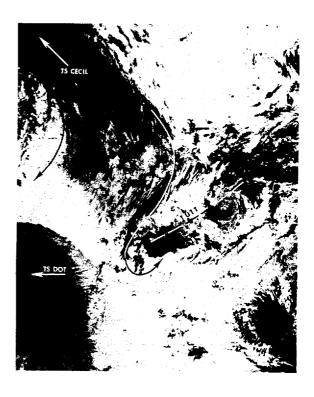


Figure 3-13-1. Satellite imagery shows Typhoon Cecil at the upper left and Tropical Storm Pot at the lower right. 1005297 August (NOAA 7 infrared imagery).

Figure 3-13-2. Satellite imagery shows Tropical Storm Cecil at the upper left and Tropical Storm Dot at the lower left. 121750Z August (NOAA 7 infrared imagery).

this period (Figure 3-13-3) shows that flow was unidirectional over Dot, with no indication of an anticyclone at that level.

As the distance between Cecil and Dot increased over the next few days, Dot regained intensity, reaching maximum sustained winds of 60 kt (31 m/sec) on the 13th. Figure 3-13-4 shows the relationship between Dot's intensity and the separation between the two cyclones. The data indicate a correlation between separation and Dot's intensity once the separation distance fell below 1000 nm (1852 km).



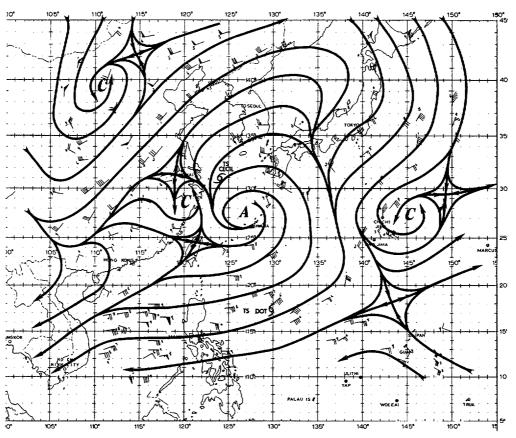


Figure 3-13-3. 121200Z 200 mb analysis with surface position of Tropical Storms Cecil and Dot superimposed.

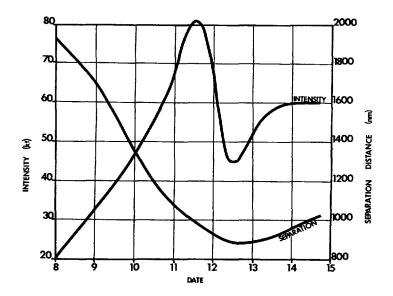


Figure 3-13-4. Variation in intensity as a function of time and separation between Dot

As Dot continued westward along the southern periphery of the subtropical ridge, several forecasts were issued indicating Dot would follow Cecil and turn toward the north prior to reaching Taiwan. However, the subtropical ridge was reestablished in the region to the north of Taiwan after Cecil's passage; subsiding air between the two tropical cyclones probably contributed to the ridging in this area, thereby causing Dot to continue its movement westward toward Taiwan. Although Dot's passage over

Taiwan was rapid, the rugged topography of the island had a devastating effect on Dot's low-level circulation. Figure 3-13-5 shows Dot as a well-organized tropical storm with maximum sustained winds of 60 kt (31 m/sec) prior to landfall. Figure 3-13-6 shows Dot 12 hours later in the Formosa Strait, barely distinguishable as a tropical storm. Dot never recovered from the effects of this crossing and dissipated less than a day later over the mountainous regions of eastern China.

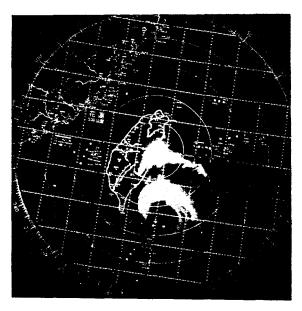


Figure 3-13-5. Tropical Storm Dot was approaching Taiwan from the southeast, as seen by radar from Hua Lien (WHO 46699) at 141400Z August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).

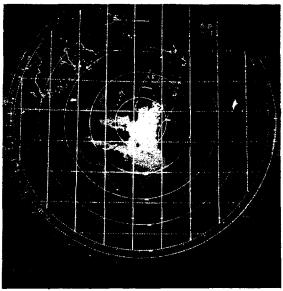
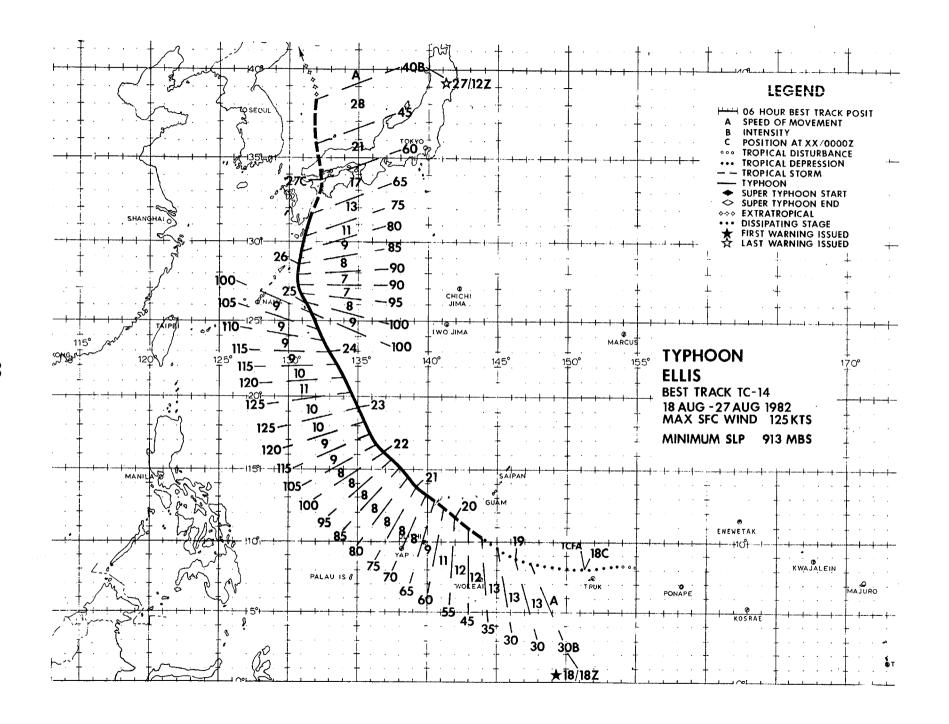


Figure 3-13-6. Tropical Storm Dot, located in the Formosa Strait after crossing southern Taiwan, as seen by radar from Kao-hsiung (WMO 46744) at 1502002 August (Photograph courtesy of the Central Weather Bureau, Taipei, Taiwan).



Typhoon Ellis developed from a disturbance that was first detected within the monsoon trough south of Ponape on 15 August. From initial detection to the issuance of a Tropical Cyclone Formation Alert (TCFA) on 18 August, the disturbance slowly acquired convective organization. Once organized, development was quite rapid, with Ellis reaching a peak intensity of 125 kt (64 m/sec) on 23 August.

The TCFA was issued at 1801002 when satellite imagery identified a cloud mass near 8N 151E that had acquired an upper-level outflow channel to the southwest. At 1804022, the initial reconnaissance aircraft mission located a 20 kt (10 m/sec) circulation center 85 nm (157 km) northwest of Truk Atoll. During the next 24 hours, satellite imagery provided fix positions on the convective center that showed movement toward the west-northwest at speeds approaching 16 kt (30 km/hr).

Based on continued convective organization, the first warning was issued

for Tropical Depression 14 at 1818002. At 191108Z, data from the second reconnaissance aircraft mission indicated maximum winds of 35 kt (18 m/sec) were present and, at 1912002, Tropical Depression 14 was upgraded to Tropical Storm Ellis. On the 19th Ellis began tracking more northwestward in response to weaker steering currents south of 15N. From the first warning until the seventh warning (200600Z) the forecast scenario anticipated an initial jog to the northwest then, as Ellis began interacting with the subtropical ridge it would return to a more westward heading. However, a deep mid-latitude trough (near 40N 115E at 200000Z) began to weaken the subtropical ridge southwest of Japan and the anticipated westward movement never materialized. By 201200Z, the effects of this mid-latitude trough on the strength of the subtropical ridge became evident and the forecast track was shifted toward the northwest.

On 20 August, satellite imagery (Figure 3-14-1) indicated the development of a banding-type eye. Ellis was upgraded to typhoon strength at 210000Z when both

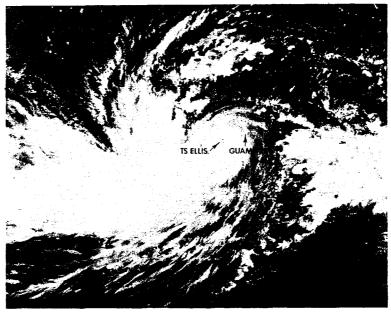


Figure 3-14-1. As an intense tropical storm, Ellis was exhibiting a strong southwest upper-level outflow pattern during a period when a banding-type eye was forming. 200510Z August (NOAA 7 visual imagery).



Figure 3-14-2. Typhoon Ellis, with strong upper-level outflow to the east and the southwest, was nearing a peak intensity of 125 kt (64 m/sec) at 2217302 August (NOAA 7 infrared imagery).

aircraft and satellite data supported an intensity greater than minimum typhoon strength (64 kt (33 m/sec)). In the following days, Ellis continued to develop rapidly, passing 100 kt (51 m/sec) intensity on 22 August and peaking at 125 kt (64 m/sec) on 23 August. Figure 3-14-2 shows Ellis just seven hours prior to reaching its maximum intensity.

By 230000Z, significant height falls were evident in the mid-tropospheric levels along the Ryukyu Islands, northwest of Ellis. The mid-latitude trough which had previously influenced Ellis's northwestward track was moving into the Yellow Sea. A day earlier, Ellis had shifted to

a north-northwestward track as the subtropical ridge continued to weaken south of Japan. Interestingly, the 14 warnings issued from 221800Z to 260000Z consistently identified Ellis track within 30 nm (56 km) of the eventual best track up to 29N. During this period, both the analyses and numerical forecast fields maintained a very good relationship between the mid-latitude trough near Korea and the subtropical ridge, east of Japan.

As Ellis moved east of Okinawa on 25 August (Figure 3-14-3) its movement shifted toward the north. As early as 240000Z, JTWC forecasts began to anticipate this movement

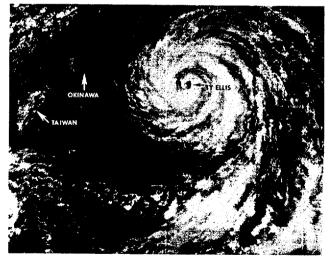


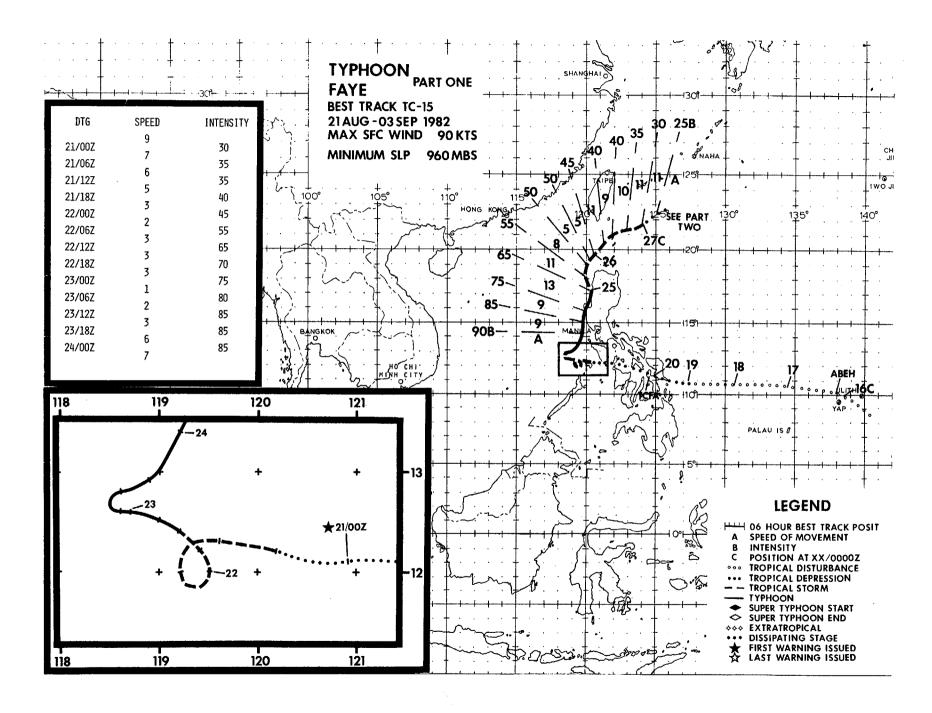
Figure 3-14-3. Typhoon Ellis, located 140 nm [259 km] east of Okinawa, was approaching the mid-latitude westerlies and subsequent acceleration toward the north. 2505512 August (NOAA 7 visual imagery).

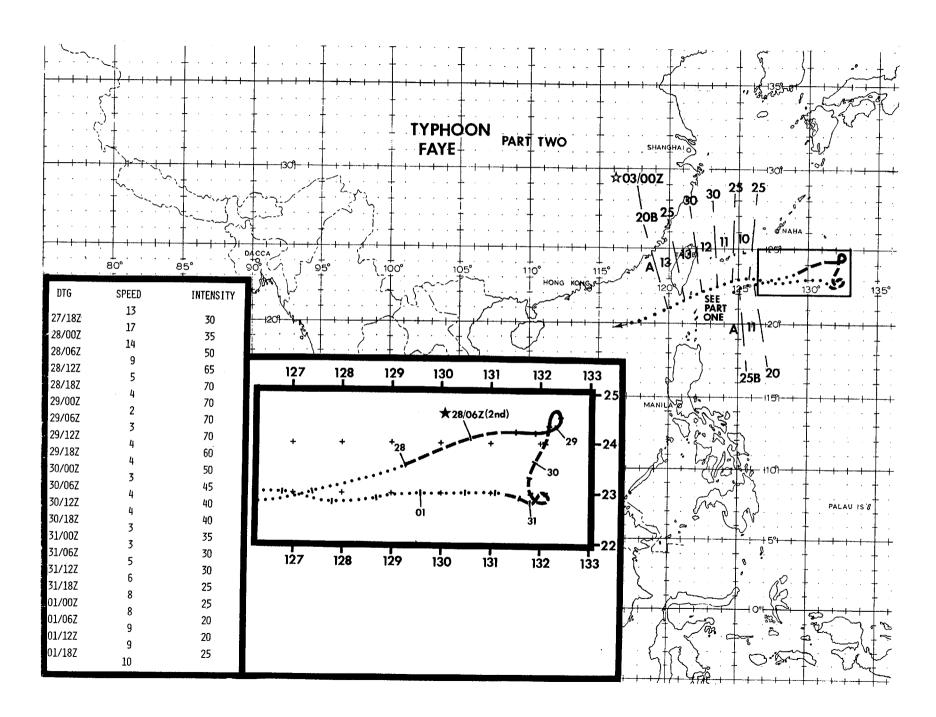
as well as significant acceleration as Ellis approached 28N, based on guidance from the Typhoon Acceleration Prediction Technique (TAPT) (Weir, 1982). Unfortunately Ellis slowed to 7 kt (13 km/hr) while approaching 28N and the early acceleration forecasts became premature in the timing of the initial acceleration. However, as Ellis crossed 28N, the predicted acceleration occurred and the speeds attained were very close to those predicted by TAPT.

Once the acceleration was underway, Ellis commenced a more rapid weakening trend as the combined effects of increasing vertical wind shear and interaction with the topography of Kyushu, Skikoku and western Honshu reduced Ellis to an estimated 45 kt

(23 m/sec) intensity as it entered the Sea of Japan.

Ellis moved toward the north-northeast on 26 August and passed along Kyushu's eastern coastline and then just west of Hiroshima on 27 August. This jog to the north-northeast was costly for the region, as torrential rains (as much as 28 inches (71 cm) in 24 hours), flooding, landslides, and high winds brought much of southwestern Japan to a virtual standstill. Having left much of its fury behind, Ellis entered the Sea of Japan on 27 August and rapidly transitioned into an extratropical low pressure system which would later move northwestward, passing 120 nm (222 km) west of Vladivostok, USSR.





Typhoon Faye (15) proved to be one of the more difficult tropical cyclones to forecast during the 1982 season (Figure 3-15-1). With forecast errors of 142, 384, and 629 nm (263, 711, and 1182 km) for 24, 48, and 72 hours, respectively, the forecast history for Typhoon Faye is a good example of what can happen when there is confusion in understanding the effect that the large-scale flow field and other larger tropical cyclones can have on a very small but intense cyclone. In this report the life history of Typhoon Faye is depicted in table form with seven segments (Table 3-15-1).

For each segment, key events along with the basic forecast philosophy and prognostic reasoning are described. A brief post-analysis description is then presented in order to compare the actual events of the tropical cyclone and the synoptic situation. In this presentation it will be evident how a basically sound and logical forecast can go astray when all the "facts" are not completely understood. Furthermore, an attempt has been made in this table to describe for the reader the basic forecast/thought process at the JTWC. Figures 3-15-2 to 3-15-7 depict several events along Typhoon Faye's track.

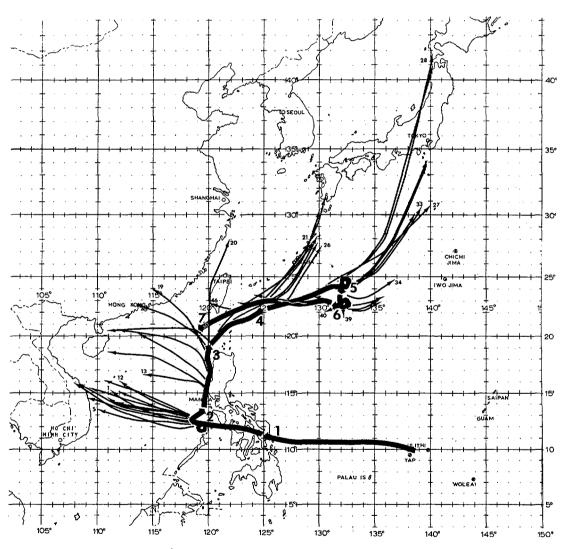


Figure 3-15-1. JTWC Windshield-wiper Chart. This chart depicts the forecast track for each warning issued for Faye. I deally, in a well-handled forecast situation, there is not a "windshield-wiper" (back and forth) effect but a superposition of one forecast track upon another. Forecast segments will be described in Table 3-15-1.

TABLE 3-15-1

Segment	Time Period (Warnings) *Events	Prognostic Reasoning	Post-analysis Discussion
1	16/00Z - 20/00Z Aug (none) *Weak disturbance moves westward in the Philippine Sea toward the southern Philippines *Monitoring disturbance for indication of convective development	Although an exposed low-level circulation could be identified on satellite imagery as well as on synoptic data, little development was expected due to the proximity of the Philippines and the dominance of the flow pattern around Typhoon Ellis (14) near Guam.	Little difference from prog reasoning. An upper-level anticyclone did develop over the area when an upper trough moved between the system and Ellis; however, convection remained unorganized due to orographic influences from the Philippines.
2	20/00Z - 24/00Z Aug (#1 - #12) *System organizes in the South China Sea *Tropical Cyclone Formation Alert at 200203Z *1st warning at 210000Z in South China Sea *Upgrading to tropical storm status at 210600Z *Upgrading to typhoon status at 221200Z	Movement: Subtropical ridge in the vicinity of Hong Kong was forecast by the FNOC models to persist and strengthen during the forecast period. This would cause the system to slowly increase its forward speed toward the west-northwest. All objective aids predicted a west to northwest movement. Intensification: Dominance of both the upper- and lower-level flow by Ellis in the Philippine Sea, as well as slight northerly shear from the 200 mb ridge over China, was expected to prevent much intensification.	Movement: The dominance of Ellis, as well as the slow encroachment of a frontal zone from central China, prevented much building of the ridge over Hong Kong resulting in weak steering flow near Faye - especially in the lower layers. Faye showed little trend in movement until a frontal/shear zone reached southeastern China on 23-24 Aug (height falls were seen at 500 and 700 mb throughout region). Intensification: Although the adverse vertical shear had an effect on the cyclone, it resulted in a small, restricted system rather than a weak one. A small TUIT cell which was analyzed near Hai-nan Island on 22 Aug appeared to aid Faye's upper-level outflow toward the northeast.
3	24/00Z - 25/18Z Aug (#13 - #19) *System continues northward *System reaches greatest strength (90 kt (46 m/sec)) at 240600Z *System reaches Luzon at 241800Z with significant damage to Wallace Air Station at 242200Z with gusts up to 100 kt (51 m/sec) *Downgrading to tropical storm status at 250000Z	Movement: A persistent northward movement was expected during the initial 24 hours with a more climatological northwestward track in the outlook period. Although the daily analysis indicated that the subtropical ridge over China was moving north and weakening, FNOC prog series continued to call for a gradual strengthening of the ridge with time. Further support of this prognosis was seen in the expected quick movement of Ellis toward the north. Since Ellis was dominating the subtropical regions between 20-30N, its acceleration to the north and out of the subtropics, would allow for the eventual reintensification of the ridge. Finally, a forecast of westward movement continued to be predicted because of two primary reasons: the hesitation to break from the forecast philosophy maintained through the first 19 forecasts and the almost total lack of climatological tracks eastward of the South China Sea. Intensification: Little change from the forecast reasoning in Segment 2. Although northeasterly vertical shear from Ellis continued to dominate, it was now generally thought that Faye would remain strong in spite of the adverse synoptic environment. Only after Faye made landfall on Luzon was a gradual weakening trend predicted.	Movement: Inspite of predictions to the contrary by the FNOC prog series, the ridge over southern China continued to retreat northward and weaken as strong troughing dominated the region between Ellis and Faye. This resulted in an almost due northward movement of Faye. Toward the end of this period, low- to mid-level westerly flow began to strengthen in the Luzon Strait while Ellis slowed its forward speed to 7 kt (13 km/hr) just east of Okinawa. Intensification: Faye continued to intensify until its circulation pattern began to interact with the mountainous terrain of western Luzon. Once landfall was made at 241800Z, a steady deterioration was observed as Faye had trouble maintaining good vertical alignment. The cause of this poor alignment appeared to come equally from the orographic effects of Luzon and the strong vertical shear north of Luzon initiated by Ellis's outflow pattern.

Segment	Time Period (Warnings) *Events	Prognostic Reasoning	Post-analysis Discussion
4	25/18Z - 27/06Z Aug (#20 - #26) *System begins to move northeastward at 251800Z *Initial final warning at 270600Z	Movement: Once Faye began to move northeastward at 11 kt (20 km/hr) along the low-level flow induced by Ellis, it was assumed that it would continue this motion until it reached Japan as FNOC prog series maintained a trough in this region throughout the period. Intensification: It was believed that if Faye could maintain its vortex, slow reintensification was possible once the strong shear from Ellis subsided. This scenario was abandoned for gradual dissipation when aircraft missions continued to show a weakening trend.	Movement: Initial northeast movement was well predicted; however, toward the end of the period the low-level flow began to split in the vicinity of Faye with a portion of the flow moving northward into the trough and the other portion moving east-southeastward toward the newly developed Tropical Storm Gordon (16). Faye began to follow this more eastward track near the end of the period. Intensification: Upper-level shear from the remains of Ellis continued to hamper Faye's efforts to reintensify. This adverse environmental effect reduced Faye to an exposed low-level circulation with only a few isolated convective cells.
5	27/06Z - 29/18Z Aug (#27 - #33) *System continues on a east-northeastward track *System reintensifies to tropical storm status at 280000Z *JTWC resumes warning status at 280600Z *System intensifies to typhoon strength at 280900Z *System weakens to tropical storm strength at 291500Z	Movement: After Ellis moved north of Japan, the long wave trough was positioned over western Japan and the Sea of Japan. Since FNOC Progs predicted little change in pattern, a forecast track toward the northeast appeared the most logical. This was also supported by the CYCLOPS steering aids and the dynamic models. The JTWC TAPT technique - which keys on the 200 mb flow - predicted rapid acceleration toward the northeast north of 25N was likely. The direction of movement was predicted along the 500 mb flow. Intensification: Wind intensities were forecast based on persistence in the near term and gradual weakening with increasing latitude in the outlook period.	Movement: Although the upper trough remained over Japan as predicted, Faye perhaps due to its small size, failed to entrain into this flow or move north of 25N. Instead it appeared to be trapped within the low-level trough between Faye and Gordon and after 281800Z it became quasi-stationary. This resulted in very large forecast errors for this period. Intensification: Once Faye moved out of the strong shearing environment, rapid intensification occurred. Faye went from a weak tropical depression to a typhoon in 27 hours. This reintensification was not well predicted nor was its extremely small size (smaller than that observed in the South China Sea). Aircraft at this time measured maximum surface winds of 70 kt (36 m/sec) out to only 10 nm (19 km) from the center and 30 kt (15 m/sec) winds out to 60 nm (111 km).



Figure 3-15-2. (Segment 1) Faye, as a tropical depression, crossing the southern Philippines. Although wind speeds were generally less than 25 kt (13 m/sec), widespread damage to property and agriculture was reported by Philippine newspapers due to flooding. 2006522 August (NOAA 7 visual imagery).

Segment	Time Period (Warnings) *Events	Prognostic Reasoning	Post-analysis Discussion
6	29/18Z - 31/06Z Aug (#34 - #39) *System shows little trend in movement and continues to weaken	Movement: Since it was apparent that Faye was not responding to the mid-latitude trough to the north, it was forecast to move eastward with the low-level flow directed toward Typhoon Gordon (16). Initially, movement was expected to be slow since the analysis fields indicated weak steering flow within the trough between Faye and Gordon. Once Gordon moved north, stronger westerlies were expected to accelerate Faye's low-level circulation eastward. Intensification: Dissipation was expected within 24 to 48 hours due to the proximity of Faye to Gordon's strong upper-level outflow pattern.	Movement: During this period, Gordon failed to maintain a steady northward motion. Instead, Gordon slowed its forward speed to 5 kt (9 km/hr). This, in turn, resulted in extremely weak steering flow at all levels around Faye. Toward the end of the period, a ridging pattern began developing over western Japan resulting in a slight increase in northerly and then northeasterly flow. Faye began to move slowly southwestward in response to this flow. Intensification: Although Faye continued to weaken as predicted, the cause was not from Gordon's upper-level wind pattern but from the movement of an upper trough from China to a position over Faye. This resulted in Faye being stripped of its convection, leaving an exposed low-level circulation.
7	31/06Z Aug - 03/06Z Sep (#40 - #50) *System weakens to a tropical depression at 310600Z *System drifts westward for three days as an exposed low-level circulation *Final warning issued by JTWC for Faye at 030000Z *System dissipates in the South China Sea at 030600Z	Movement: With the ridge well established north of the system and over western Japan, a predicted westward movement appeared to be best. Intensification: Aircraft reconaissance indicated that Faye's central pressure had risen to 999 mb and so each warning during this period predicted dissipation within 24 hours.	Movement: Forecast track was fairly accurate although Faye's increase in forward speed to 13 kt (24 km/hr) was not anticipated. Intensification: Although its wind intensities were only 20-30 kt (10-15 m/sec), Faye managed to survive as a low-level circulation much longer than predicted. Final dissipation did not occur until Faye's exposed low-level circulation became entrained into the monsoon circulation that was to become Typhoon Hope (17) in the South China Sea.

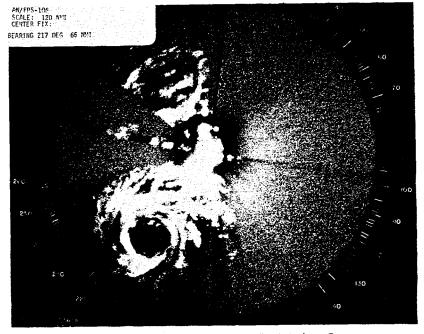


Figure 3-15-3. (Segment 3) The "eye" of Typhoon Faye as seen by radar 66 nm (122 km) southwest of Subic Bay at 2403587 August. (Photograph courtesy of NOCF, Cubi Pt, Republic of the Philippines)

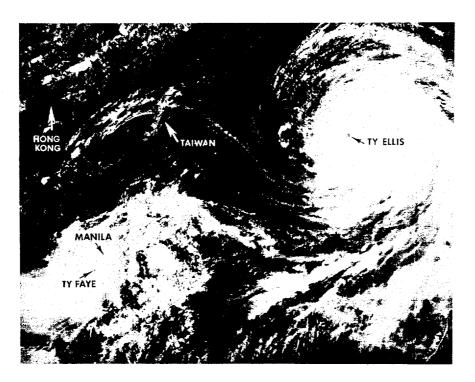


Figure 3-15-4. (Segment 3) Typhoon Faye at full strength, 90 kt (46 m/sec), just south of Luzon. The much larger Typhoon Ellis, 110 kt (57 m/sec), can be seen 925 mm (1713 km) northeast of Faye. 240603Z August (NOAA 1 visual imagery)



Figure 3-15-5. (Segment 4) Tropical Storm Faye just south of Taiwan weakening rapidly at 2605397.
August as it moves under the strong upper-level outflow of Typhoon Ellis. (NOAA 7 visual imagery)

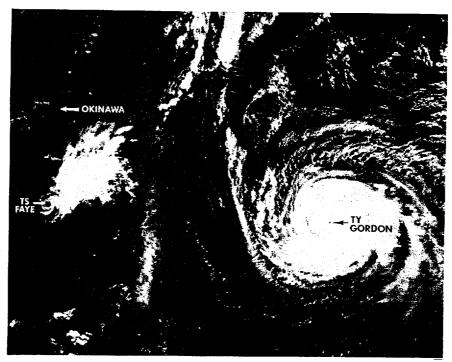


Figure 3-15-6. (Segment 6) Tropical Storm Faye, 50 kt (26 m/sec), once again being dwarfed by another tropical cyclone (Typhoon Gordon, 100 kt (51 m/sec)) at 3004512 August (NOAA 7 visual imagery)

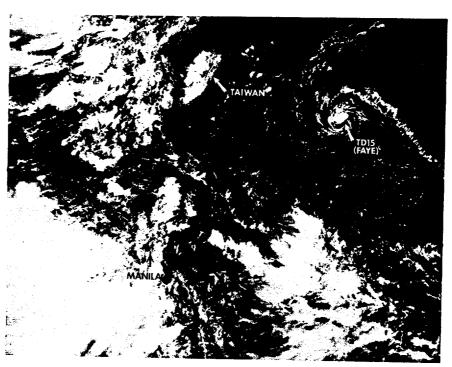
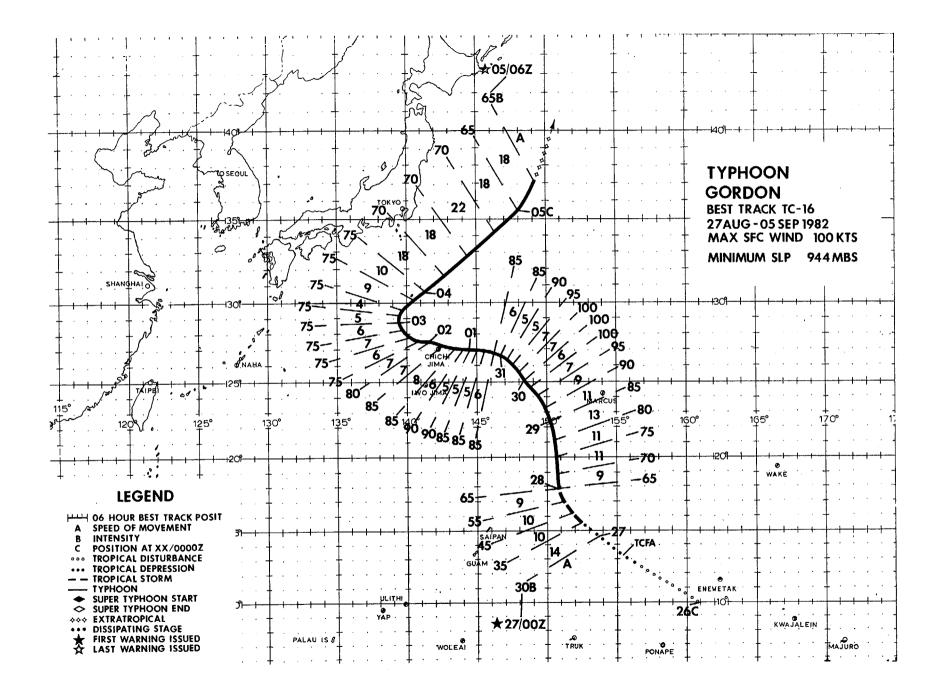


Figure 3-15-7. (Segment 1) An exposed low-level circulation can be seen just east of Taiwan as the remains of Typhoon Faye at 0106087 September. This weak circulation persisted for over three days. (NOAA 7 visual imagery)



Typhoon Gordon developed rapidly from a disturbance which was initially detected while it was embedded in an elongated monsoon trough along 8N between 145E and 175E. Within 48 hours of its initial detection, Gordon reached typhoon strength and eventually proved to be one of the most difficult typhoons of the season for JTWC forecasters.

On 25 August, a surface circulation was detected near 8N 163E associated with an area of strong, yet unorganized convection. During the ensuing 24 hours little increase in convective organization was noted on satellite imagery; however, an uppertropospheric pattern existed nearby that was conducive for further development. Analysis data indicated that outflow channels were readily available via an upper-level anticyclone centered near 10N 167E, further enhanced by a tropical upper-tropospheric trough (TUTT) north of Guam.

Rapid development did not occur until the upper-level anticyclone moved over the surface circulation. A TUTT cell located northwest of the disturbance enabled outflow channels to remain open to all quadrants and resulted in a significant increase in convection on 26 August. A Tropical Cyclone Formation Alert (TCFA) was issued at 261500Z during this burst in convective activity and organization. Synoptic data from Truk Atoll (WMO 91334) and Ponape (WMO 91348) at 261200Z also indicated intensification was occurring as gradient level winds increased to near 30 kt (15 m/sec) at both reporting stations.

A reconnaissance aircraft investigative mission at 262347Z was able to fix a circulation center near 14.5N 154E with associated surface winds of 30 kt (15 m/sec) and a 1001 mb sea level pressure. These data preceded the issuance of the first warning for Tropical Depression 16 at 270100Z. One day later, at 272335Z, reconnaissance aircraft data showed Gordon's central sea level pressure had dropped to

977 mb and surface winds of 65 kt (33 m/sec) were observed in the north semicircle. During this period of intensification, Gordon was upgraded to tropical storm status at 2706002 and typhoon status at 2800002 based on reported aircraft data and steadily increasing cloud system organization. At 2918002, four days after initial detection, Gordon's rapid intensification ended at 100 kt (51 m/sec) (See Figure 3-16-1).

The forecasts issued by JTWC during Gordon's developing stages anticipated a northwestward movement toward a weakness in the subtropical ridge located near 20N 150E. These forecasts anticipated recurvature to occur as Gordon moved north of the ridge axis along 23N and came under the influence of an advancing mid-latitude trough. In response to this synoptic situation, Gordon's forward speed slowed as it approached the ridge axis on 28 August; however, the midlatitude trough continued its eastward movement and by 29 August, its effects on Gordon's movement were no longer evident. Following the passage of this trough, the subtropical ridge was re-established north of Gordon and in response, Gordon resumed a northwestward track along the ridge's southwestern periphery. Forecasts issued on 29 and 30 August reflected Gordon's continued northwestward movement followed by a northward movement and acceleration toward Japan.

By 31 August, a different forecast scenario was gaining strength. At 310000Z, 500 mb and 700 mb height rises were observed over southern Honshu and north of Gordon, indicating the approaching short wave trough was weakening or moving more northeastward than previously forecast. During this period, Gordon, with 90 kt (46 m/sec) surface winds, was advecting large amounts of warm, moist air from the tropics and thereby strengthening the ridge to the northeast. This strengthening of the ridge, combined with changes in the short wave trough, forced Gordon toward

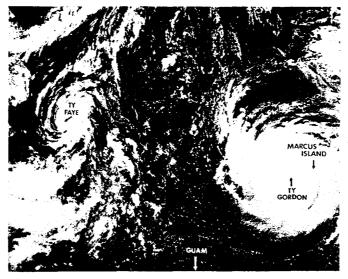


Figure 3-16-1. Typhoon Gordon near maximum intensity of 100 kt [51 m/sec] 640 nm [1185 km] northeast of Guam. Typhoon Faye is also seen in this picture south of Okinawa. 290502Z August (NOAA 7 visual imagery).

a more westward track which was maintained until late on 2 September.

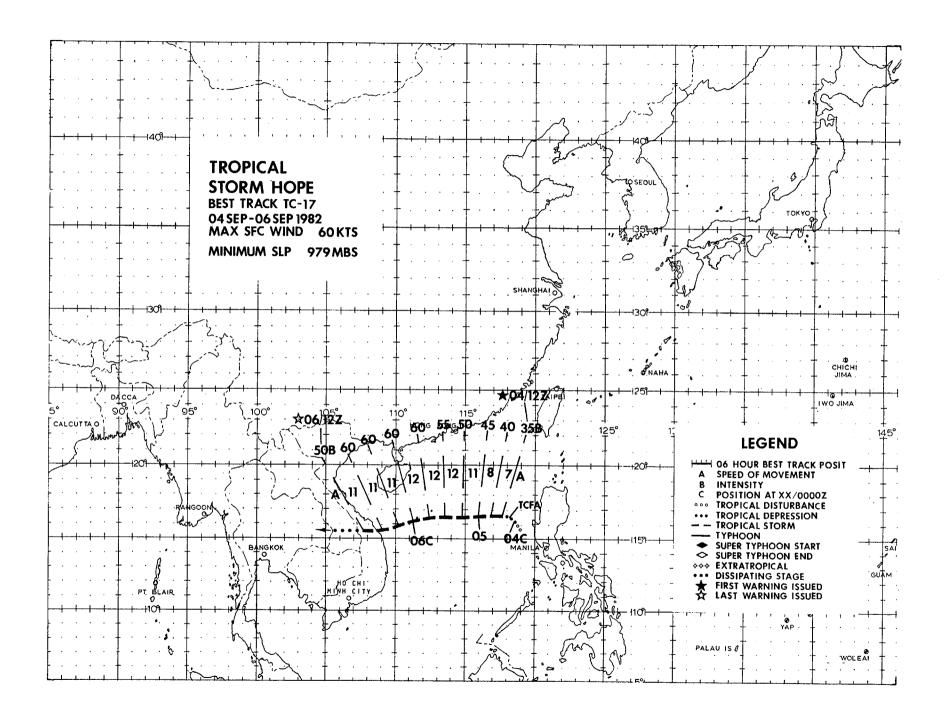
In response to numerical forecast fields which showed a low- to mid-level ridge near Korea building eastward over Japan, JTWC forecasts on 2 September began forecasting a continued westward movement along the southern periphery of the two ridges. By 030000Z, a conflicting forecast scenario began to develop. It was observed that 500 mb and 700 mb heights were falling over southern Honshu, indicating that the short wave trough, located over Hokkaido, was deepening once again. However, the numerical forecast fields provided by Fleet Numerical Oceanography Command (FNOC), Monterey, CA, did not reflect this tendency and continued to build the ridge behind the short wave trough and to the north of Gordon's track. At this time, two opposing forecasts were considered possible: one reflecting the westward track below the

ridge; the other, indicating a sharp recurvature and acceleration toward the northeast in response to the deepening trough. JTWC chose to maintain the westward prediction as the FNOC forecast fields appeared to be a meteorologically sound solution to the synoptic situation. Concurrently, an intensive meteorological watch was instituted whereby conventional analysis data and satellite imagery were closely monitored for indication of any changes which would mandate a change from the westward-moving forecast scenario.

On 3 September, Gordon slowed to 4 kt (7 km/hr) from 7 kt (13 km/hr) and took an increasingly more northward course. This movement, combined with the continued 500 mb and 700 mb height falls over Honshu prompted JTWC to abandon the westward forecast at 031200Z, and adopt a forecast toward sharp recurvature and acceleration to the northeast.

Subsequent to the change in the JTWC forecast toward recurvature, the FNOC forecast fields, produced from the 0312002 data base, changed significantly and supported the recurvature scenario. Had the numerical forecast series indicated this trend earlier and not persisted in building the low- to mid-level ridge eastward from Korea, the recurvature track would have been adopted much earlier or perhaps not even abandoned on 2 September. This forecast situation emphasizes the difficulty in issuing credible forecasts when there exists a conflict between the observed short-term changes in the analysis data and the numerically forecast changes beyond the analysis period. There are no easy answers in there situations and unfortunately, in similar future forecast situations, JTWC and its customers may well have to deal with alternating guidance from both analysis and forecast fields.

On 3 and 4 September, Gordon did sharply recurve to the east-northeast as it became embedded in the mid-latitude westerlies along the southeastern periphery of the short wave trough. A fairly rapid accleration to 22 kt (41 km/hr) was observed prior to extratropical transition near 37N at 050600Z. As Gordon recurved, it passed 260 nm (482 km) southeast of Tokyo. The U.S. Naval Oceanography Command Facility at Yokosuka, Japan, reported maximum sustained winds of 32 kt (16 m/sec) with a maximum gust of 44 kt (23 m/sec) during the period, 3 to 4 September. Fortunately, despite some difficult forecast situations, Gordon did not strike any major land mass and there was no significant damage to military or civilian interests in Japan.



Tropical Storm Hope developed from a monsoon depression which formed on 3 September along the northern edge of a strong southwest monsoon flow (25 to 30 kt (13 to 15 m/sec)) that was present over the southern portion of the South China Sea. During the formative stages of this rapidly deepening monsoon depression, shipboard synoptic observations provided essential data which enabled the JTWC to closely monitor the system's development.

At 0403452, a Tropical Cyclone Formation Alert was issued for an area west of central Luzon when shipboard observations revealed surface pressures had dropped to at least 1002 mb near the depression's center. The 0412002 synoptic data, indicating improved organization in the low-level wind flow, prompted the first warning which was issued at 0415002. In support of the first two warnings, satellite fix positions - based on a poorly-defined cloud signature - and surface observations did not correlate very well on the system's center. Thus, when a resources permitting aircraft reconnaissance mission at 0423572 located Hope well southwest of the previous warning position, with

maximum winds of 45 kt (23 m/sec) and a 994 mb central sea level pressure, the tropical cyclone was relocated and upgraded to tropical storm status on the 050000Z warning.

During the first 30 hours in warning status, Hope intensified to a peak of 60 kt (31 m/sec) which was maintained until landfall. On 6 September, Hope slammed into the coast of Vietnam, 25 nm (46 km) south of Da Nang, and subsequently dissipated over the mountainous terrain of Vietnam and Laos. Accompanying Hope's demise over Southeast Asia, widespread flooding was reported in Vietnam and northeastern Thailand, resulting in several thousand people fleeing their homes and extensive damage to the season's rice crop.

From the first warning, JTWC forecasts continued to anticipate that Hope would slow its forward movement, or move towards the west-northwest and slow. Hope, however, accelerated towards the west-southwest, paralleling the subtropical ridge axis to the north, and the expected forecast movement was never realized.

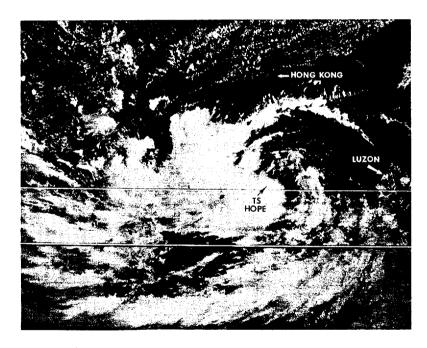
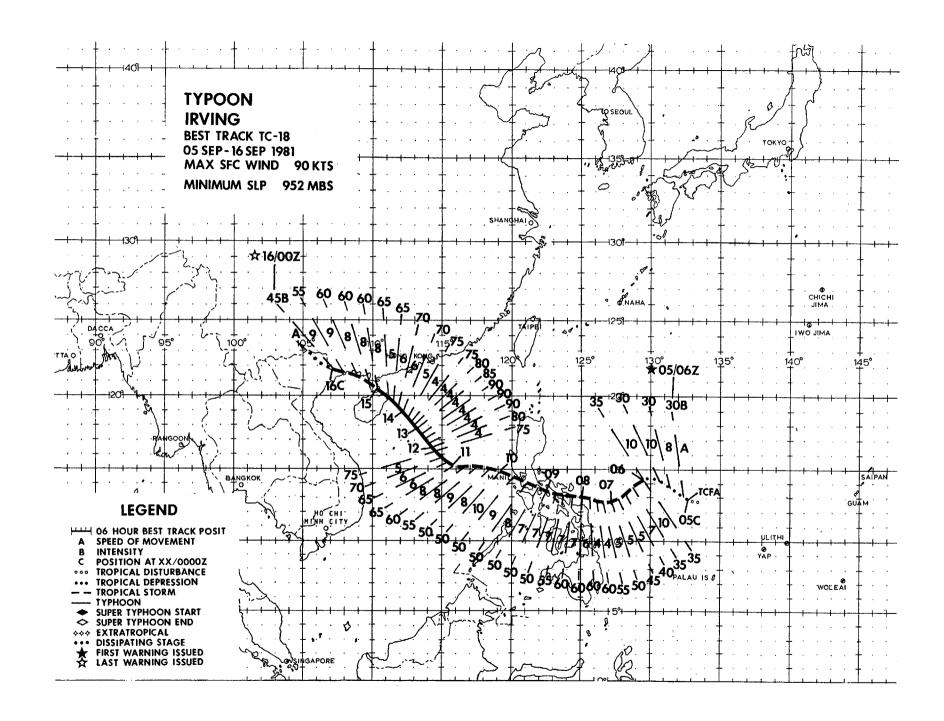


Figure 3-17-1. Tropical Storm Hope near 50 kt (26 m/sec) intensity in the central South China Sea. 0507002 September (NOAA 7 visual imagery).



Typhoon Irving developed within an area of unorganized convection associated with an active monsoon trough anchored south of Guam in early September. Surface pressures throughout the region between 125E to 165E and 8N to 13N were below 1004 mb, and the southwest monsoon flow averaged 20 kt (10 m/sec) over much of the region. By 040300Z, a low-level circulation was evident on visual satellite imagery near 11N 130E, although nearby convection had decreased during the preceding 12 hours. During this period, another tropical cyclone was developing in the monsoon trough near 12N 147E (Typhoon Judy (19)). The passage of Typhoon Gordon (16) east of Japan reestablished a low-level easterly flow to the north of both of the developing systems; thus increasing the potential for further development.

As the circulation near 130E (Irving) developed, an increase in cloud organization was seen on satellite imagery which led to the issuance of a Tropical Cyclone Formation Alert at 050000Z. An immediate, abbreviated warning bulletin for Tropical Depression 18

was issued by JTWC at 050855Z, when reconnaissance aircraft closed off a surface circulation with observed winds near 30 kt (15 m/sec). Based on continued convective organization, Tropical Depression 18 was upgraded to Tropical Storm Irving at 051800Z.

Early in its development, Irving was characterized as an exposed low-level circulation center to the east of the most active convection region of the disturbance. Visual satellite imagery and aircraft reconnaissance data enabled JTWC to follow the surface center, rather than the upper-level (convective) center, as Irving moved across the Philippine Sea.

From 6 to 8 September Irving remained equatorward of a strengthening subtropical ridge and maintained a westward track across the Philippine Sea. Irving made landfall at 080900Z, on the southern tip of Luzon (Figure 3-18-1). Maximum winds at landfall were 60 kt (31 m/sec). Thereafter, Irving assumed a more northwestward path (of least resistance) through the Sibuyan Sea

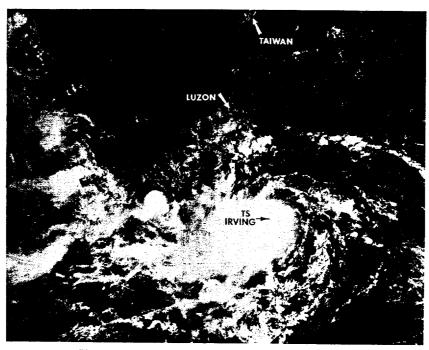


Figure 3-18-1. Tropical Storm Irving near landfall south of Luzon. 0816162 September (NOAA 7 visual imagery)

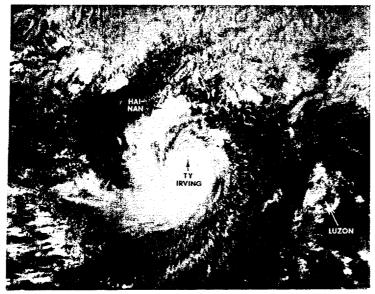


Figure 3-18-2. Typhoon Irving near maximum intensity in the South China Sea. 1307062 September [NOAA 7 visual imagery]

and remained over a marine pathway between the islands of the central Philippines. During this period, Irving maintained much of its intensity although some convective organization was lost. Irving entered the open waters of the South China Sea, 27 nm (50 km) southwest of Cubi Point Naval Air Station at 0917002. NAS Cubi reported sustained winds of 46 kt (24 m/sec) with a peak gust of 64 kt (33 m/sec) during Irving's transit of the region.

As Irving moved into the South China Sea, a return to a more westward track and gradual intensification were forecast, with the subtropical ridge anticipated to maintain itself north of Irving's track throughout most of the period. A more northwestward track became probable based upon analyses of 500 and 700 mb heights at 110000Z that indicated height falls at both levels were occurring over China. Irving, sensing this developing weakness in the subtropical ridge, maintained



Figure 3-18-3. Typhoon Irving approaching mainland China. 1506432 September [NOAA 7 visual imagery]

a slow, northwestward movement until 1412002, when a slight acceleration began. Aircraft reconnaissance at 1206302 reported a maximum observed surface wind of 90 kt (46 m/sec), well above the 50 to 65 kt (26 to 33 m/sec) range previously forecast. Figure 3-18-2 shows Irving near peak intensity. The aircraft data also indicated that Irving had a very tight circulation, with the radius of 50 kt (26 m/sec) winds within 60 nm (111 km) of the center during this period of maximum intensity. Radar observations, as well as synoptic reports from the Paracel Islands

(WMO 59981 and 59985) were very useful in accurately determining Irving's position and intensity during the period 12-13 September when reconnaissance aircraft fix missions could no longer be flown.

On 15 September, as the system began to interact with Hai-nan Island and the coast of China, Irving was downgraded to tropical storm strength (Figure 3-18-3). Irving made landfall 110 nm (204 km) northeast of Hanoi at 151800Z, and thereafter rapidly dissipated over the mountainous area of Vietnam.

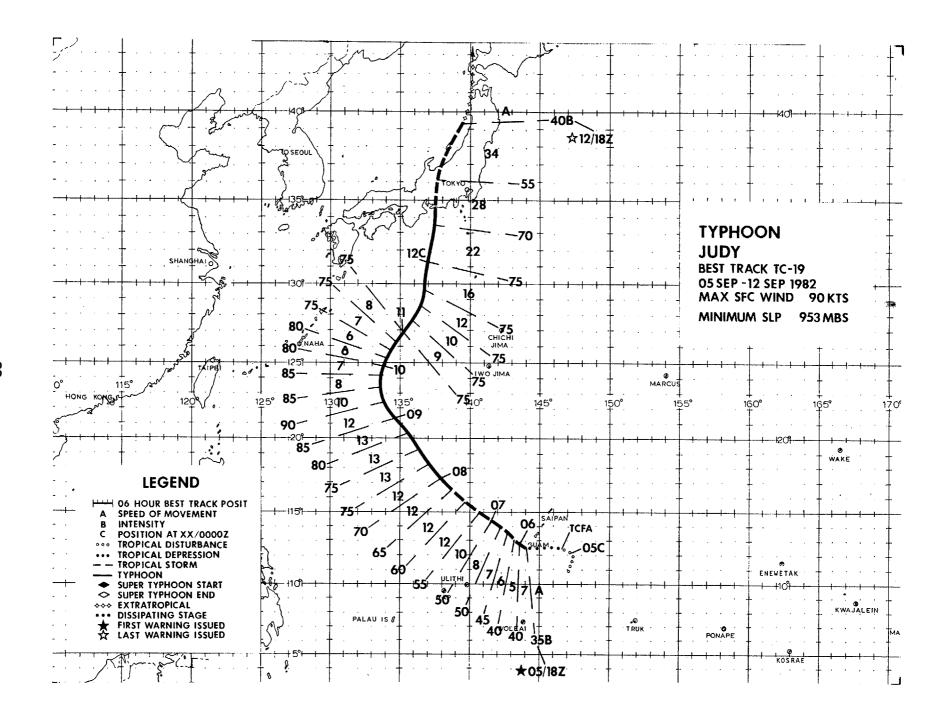




Figure 3-19-1. 050520Z September (NOAA 7 visual imagery).

Typhoon Judy, along with Typhoon Irving (18) developed within a very active monsoon trough that dominated the low-latitudes of the western North Pacific during the first week of September. At 041200Z, synoptic data indicated low-level winds were beginning to organize around the disturbances which later became Judy and Irving. This apparent organization prompted the reissuance of the Significant Tropical Weather Advisory (ABEH PGTW) at 041600Z which discussed each of these systems for the first time. The relatively continuous maximum cloud zone that spawned these two typhoons is shown in Figure 3-19-1, at about the time that a Tropical Cyclone Formation Alert was issued for Judy and the initial warning was issued for Tropical Depression 18 (Irving).

During the ensuing 24-hour period, Judy rapidly organized while Irving slowly intensified. It was during this period that satellite imagery showed the maximum cloud zone segmenting around the

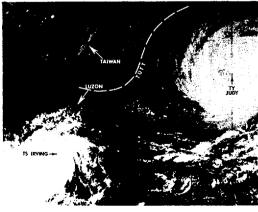


Figure 3-19-3. 090613Z September (NOAA 7 visual imagery).



Figure 3-19-2. 060508Z September (NOAA 7 visual imagery).

two systems (Figure 3-19-2). The first warning for Tropical Depression 19 was issued at 051600Z when satellite imagery indicated a progressive development of cloud features around the system. The first reconnaissance aircraft mission for Judy was conducted at 052239Z and reported 45 kt (23 m/sec) surface winds and a 994 mb minimum sea level pressure. Based on these data, Tropical Depression 19 was upgraded to Tropical Storm Judy on the 060000Z warning.

Initial forecasts for Judy anticipated a movement toward the west-northwest as the numerical forecast series built the subtropical ridge from 150E toward 130E along 25N. However, the subtropical ridge did not build from east to west but built northward along 150E instead. This change in ridge orientation, along with the eastward progression of a short wave trough over Asia, permitted Judy to track northwestward toward eventual recurvature east of Okinawa.



Figure 3-19-4. 0918582 September (NOAA 7 infrared imagery).

From 6 to 9 September, Judy developed at a fairly steady rate (15 to 20 kt (8 to 10 m/sec) per day) and reached a peak intensity of 90 kt (46 m/sec) on 9 September. This period of intensification was aided by a tropical upper-tropospheric trough (TUTT) that was located to the north and northwest of Judy through most of this period.

On 8 and 9 September, 200 mb data and satellite imageries suggested that Judy's upper-level circulation was moving into a region previously occupied by the TUTT. As depicted in Figure 3-19-3, the TUTT axis was contorted northward around the periphery of the advancing Judy. By 091858Z (Figure 3-19-4), satellite imagery revealed that the west quadrant was virtually devoid of deeplayer convection and Judy's center had expanded to more than 90 nm (167 km) in diameter. During this period, Judy exhibited a reversal in sea level pressure tendency and subsequent

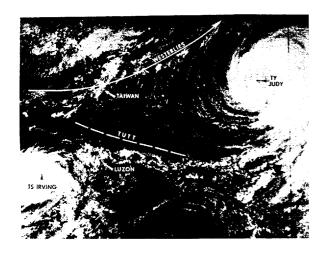


Figure 3-19-5. 1006012 September (NOAA 7 visual imagery)

On 10 September, Judy was moving slowly (6 to 7 kt (11 to 13 km/hr)) toward the north-northeast, satellite imagery (Figure 3-19-5) shows the cloud signature returning to a more circular appearance. Presumably, the interaction with the TUTT had ceased and the mid- and upper-levels were returning to a more typical environment for a mature typhoon.

Judy accelerated toward Japan on the llth; this movement had been expected as early as 9 September (near 24N) but was delayed until the influence of low-level

reintensification was not observed. Based on the interpretation of available data, it appears that at the mid- and upper-tropospheric levels, Judy may have ingested the remnants of the TUTT; and this entrainment of cooler air at these levels may have accounted for the changes in Judy's intensity trend and the resultant satellite signature that were observed on 9 September.

Prior to 081800Z, JTWC forecast tracks predicted that Judy would progress slowly toward the north in the 48- to 72-hour period with a close approach to Okinawa expected. However, with the issuance of warning number 13 at 081800Z, a significant change toward the north and recurvature toward eastern Honshu was forecast. This change in the forecast was prompted by the 081200Z 500 mb and 200 mb analyses data which showed a deeper penetration of a midlatitude trough, south of Korea, than was previously anticipated.

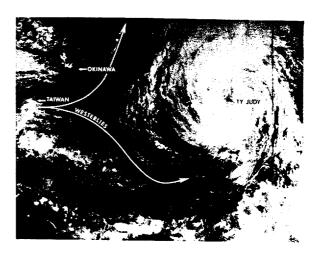


Figure 3-19-6. 110549Z September (NOAA 7 visual imagery)

steering became favorable for a sustained northward movement. A low-level anticyclone, centered near 45N 120E, had been exerting a relatively strong north to northeast flow over the Sea of Japan southward to 27N. On 11 September, this anticyclone began to weaken and its influence on the region north of Judy abated. In response, Judy accelerated from 8 kt (15 km/hr) at 110000Z to well over 25 kt (46 km/hr) before it struck Japan 38 hours later. Figure 3-19-6 shows Judy as this acceleration began.

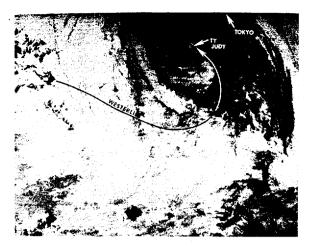


Figure 3-19-7. 111834Z September (NOAA 7 infrared imagery)

As Judy approached 30N, strong upper-level winds from the south-southwest began exerting considerable pressure on Judy. As seen in Figure 3-19-7, convective activity was eroding on the southwestern periphery of Judy's center. This process preceded and accompanied Judy through its extratropical transition (Figure 3-19-8).

At 1208002, Judy made landfall upon Omaezaki Point in Shizuoka Prefecture,

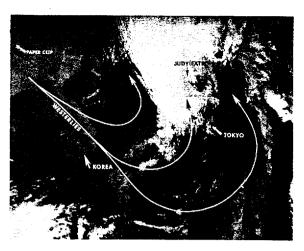
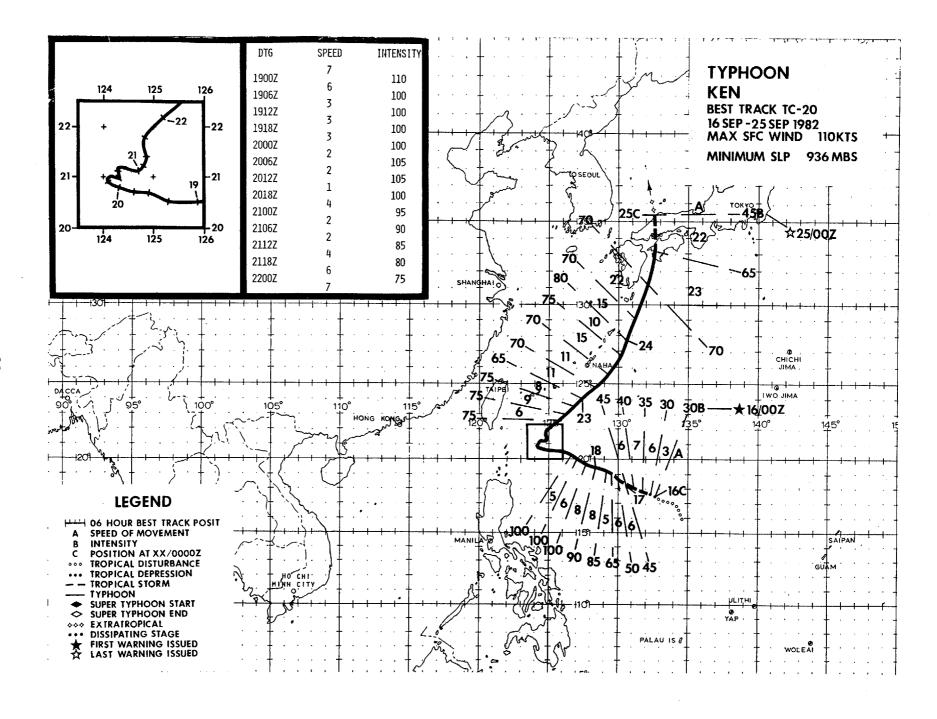


Figure 3-19-8. 1218102 September (NOAA 7 infrared imagery).

southeast of Nagoya. Judy moved rapidly over the mountainous region of central Honshu and entered the eastern portion of the Sea of Japan where extratropical transition followed. In its wake, Judy left at least 25 dead and the accompanying torrential rains and floods damaged more than 61,000 houses, washed out sections of 956 highways and swept away 46 bridges in an area stretching from Osaka in the south, to Hokkaido in the north.



Typhoon Ken formed in mid-September in the western portion of an elongated monsoon trough in the Philippine Sea. Satellite imagery on 14 and 15 September showed a persistent convective disturbance near 17N 134E with evidence of upper- and lower-level circulation centers. A reconnaissance aircraft mission early on 16 September closed off a surface circulation near 18N 133E, with 10 to 35 kt (5 to 18 m/sec) winds and a minimum sea level pressure of 1003 mb. Based on this information, JTWC elected to forgo the issuance of a Tropical Cyclone Formation Alert and, at 160300Z, the initial warning was issued on Ken as Tropical Depression 20.

Ken was upgraded to tropical storm status on the 161200Z warning after aircraft reconnaissance reported a 999 mb central pressure and sustained winds of 35 kt (18 m/sec). Initial warnings for Ken anticipated movement toward the west, passing near the northern tip of Luzon within 72 hours. The forecasts were based on the apparent strength of the mid-level steering flow along the southern periphery of the subtropical ridge which was centered between Taiwan and Okinawa. Thirty-three hours after the initial warning was issued, Ken was upgraded to typhoon status when aircraft reconnaissance data showed a central pressure of 976 mb, equivalent to an intensity of 65 kt (33 m/sec) (Atkinson and Holliday, 1977). Ken underwent a rapid intensification during the following 24 36 hours, with its intensity surpassing 100 kt (51 m/sec) on 18 September. Up to this point in its development Ken was characterized as a compact system; for example, aircraft data at 1806002 indicated a 938 mb central pressure in a 10 nm (19 km) diameter eye with a maximum surface wind of 100 kt (51 m/sec) located within a band of maximum winds only 15 nm (28 km) from the center.

Ken moved much slower than anticipated, and toward the west-northwest, for the first four days in warning status. During this period, a gradual but significant change in the subtropical ridge was taking place; by 19 September the ridge had retrograded southwestward and strengthened over southern China and the northern portion of the South China Sea. JTWC forecasts during this period expected this slow movement to be short-lived based on a forecast strengthening of the ridge north of Ken and a corresponding weakening of the ridge over the South China Sea which would allow Ken to resume its movement westward. This forecast scenario never materialized and, aided by analysis and prognostic fields from the 1912002 data base which provided indications that westward movement was not likely to occur, JTWC forecast tracks turned toward the north commencing with the 200000Z warning. Some of the indicators which prompted JTWC to change the forecast track were: the numerical forecast fields were starting to show a persistent break in the ridge north of Ken vice a strengthening of the ridge; the dynamic tropical cyclone models (OTCM, NTCM) began to consistently forecast a northward movement; and analysis data began to show significant height falls at the 700 mb level were starting to occur north of the ridge over southern Japan.

Despite all the signs predicting a northward movement, Ken eventually became quasi-stationary on 20 September (Figure 3-20-1 shows Ken at its westernmost position) and the character of the associated circulation pattern began to change dramatically; aircraft reconnaissance missions found the center expanding, with the strongest wind bands moving away from the center. The diameter and character of the eye (when observed) was also changing from mission to mission. A possible explanation of what

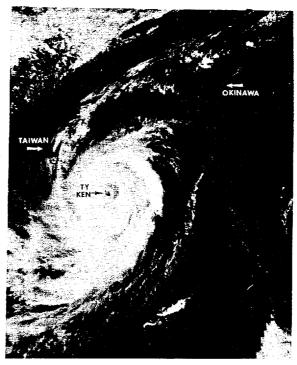


Figure 3-20-1. Typhoon Ken, at its westernmost position and just beginning a period of very little movement. Note the strong banding toward Ken's center. Within the next two days, much of this center would erode, leaving a nearly cloud-free area 60 nm [111 km] in diameter. 2005422 September {NOAA 7 visual imagery provided by Det 4, 1000 Clark AB RP}.

caused Ken to undergo such drastic changes could be the interaction with mid-latitude westerlies advecting much cooler air into Ken's center, thus accounting for formation of the large cloud-free center. The 201200Z 500 mb analysis (Figure 3-20-2) shows the winds from the west moving into Ken's circulation about the time that these changes began. However, this does not explain why Ken's eye dissipated and then reformed within the otherwise cloud-free center, unless the westerlies were diverted from the center for short periods of time, allowing warm, moist air to reenter the center and assist in the reformation of the eye.

Ken's eye was last observed at 2120112 during a double-fix aircraft mission. On the first penetration, the mission Aerial Reconnaissance Weather Officer (ARWO) indicated the eye was 7 nm (13 km) in diameter but on the second penetration, at 2123272, the ARWO reported "... the eye was so large we couldn't even pick it up on our radar ...". Further, the band of maximum winds were observed some 60 to 95 nm (111 to 176 km) from Ken's center.

On 21 September, satellite imagery and upper air analysis data indicated the trough north of the subtropical ridge had begun to

Candis L. Weatherford, Capt, USAF, mission ARWO.

deepen. In response, Ken began to move erratically toward the northeast and by 2118002 was on a steady course toward Okinawa. The possibility of significant acceleration was examined as continued interaction with the mid-latitude westerlies seemed likely. A recently developed JTWC forecast aid, TAPT (Weir, 1982), indicated Ken might undergo acceleration near 25N. Indeed, as Ken approached 26N, its forward speed began to increase and acceleration continued until landfall on the island of Shikoku, Japan. During this acceleration period Ken passed 78 nm (143 km) southeast of Okinawa; maximum winds recorded at Kadena AB were 35 kt (18 m/sec) at 2309552 and a peak gust of 58 kt (30 m/sec) at 2311352. Ken also brought a significant, and much needed, rainfall to Okinawa; 11.09 inches (28.2 cm) were recorded at Kadena on 23 September.

Once past Okinawa, Ken began to gradually weaken under strong mid- and upper-level

westerlies. Aircraft reconnaissance missions continued to find the belt of maximum surface winds moving farther away from the center with every fix. Satellite imagery showed a steady decline in convection as Ken continued to move toward Japan. Ken made landfall upon Shikoku at 241700Z, crossed the inland sea, and then moved through western Honshu into the Sea of Japan where it became extratropical at 25000Z.

Ken was the fourth typhoon of the season to hit the main islands of Japan; it brought torrential rains and high winds, which triggered mudslides that flooded or wrecked thousands of homes and paralyzed both air and ground transportation. Reports from the region indicated that a peak gust of 114 kt (59 m/sec) was recorded on Shikoku during Ken's passage along with 8.7 inches (22.1 cm) of rain over one six-hour period.

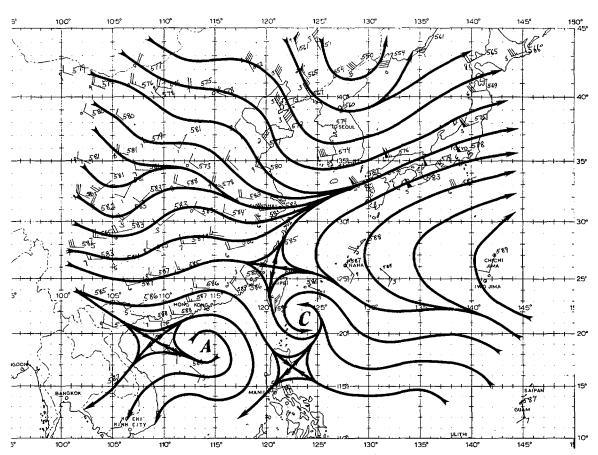
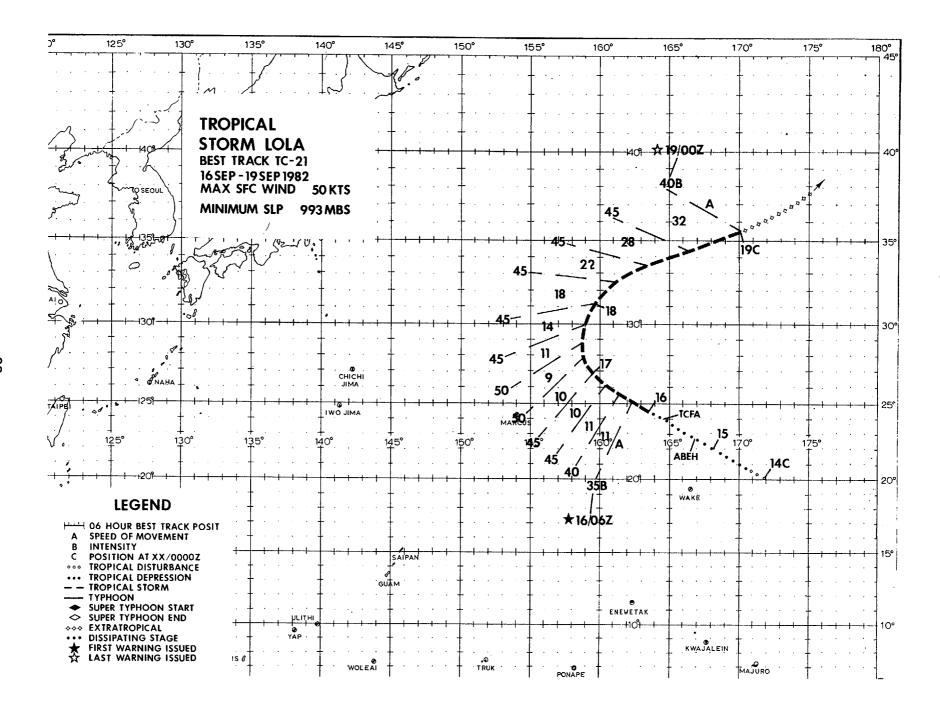


Figure 3-20-2. 500 mb analysis, valid at 2012007. The strength of the subtropical ridge over China had diminished during the previous 12-hour period. This process allowed mid-latitude westerlies to move further southward and become involved with Ken's circulation pattern. The break in the east-west extension of the ridge, north of Ken, can also be seen. Wind speeds are in knots.



Tropical Storm Lola was the third tropical cyclone of the season to form in the subtropical latitudes of the western North Pacific Ocean. Typical of tropical cyclones that form north of 20N in the mid- and late summer, Lola's formation was aided by its proximity to a tropical upper tropospheric trough (TUTT) cell (Sadler, 1976) and remained a small, compact tropical cyclone during its lifetime. Due to Lola's remote location, no successful reconnaissance aircraft missions were flown and all fix positions and intensity estimates were based on analyses from satellite imagery.

Lola was first detected on satellite imagery as a weakly organized band of convection near the dateline on 13 September. By 140000Z, this convection had moved westward to within 600 nm (1111 km) of a well-defined TUTT cell that was located in the vicinity of Wake Island (WMO 91245). During the ensuing 24 hours, the upper-tropospheric divergence fields appeared to increase in the area and a small anticyclone was soon detected on satellite imagery over the disturbance. During the same period, a low-level shear line from a cold front moved to within 200 nm (370 km), north of the convective disturbance. This shear line appeared to aid the development of the low-level

circulation center, as cumulus lines could be detected spiraling into the system's center from the north as early as 1500002.

Convection remained weak and variable over the next 18 hours; however, at 1518292 a Tropical Cyclone Formation Alert was issued when upper-level outflow increased around the system. During the next 12 hours, convective organization increased and at 1606002, the first warning was issued for Tropical Storm Lola when the intensity estimate from analysis of visual satellite imagery indicated the likelihood of 35 kt (18 m/sec) surface winds near Lola's center.

Lola's eventual recurvature around a mid-tropospheric anticyclone was well forecast due, in part, to good agreement from the very first forecast with the CYCLOPS steering aids and the One-Way Interactive Tropical Cyclone Model (OTCM).

As Lola approached 30N on 17 September, acceleration toward the northeast began in advance of a newly formed cold front which was moving toward Lola from the northwest. Extratropical transition was completed by 190000Z when Lola became totally entrained into the frontal system.

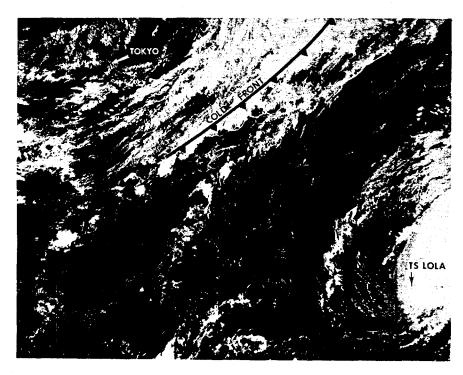
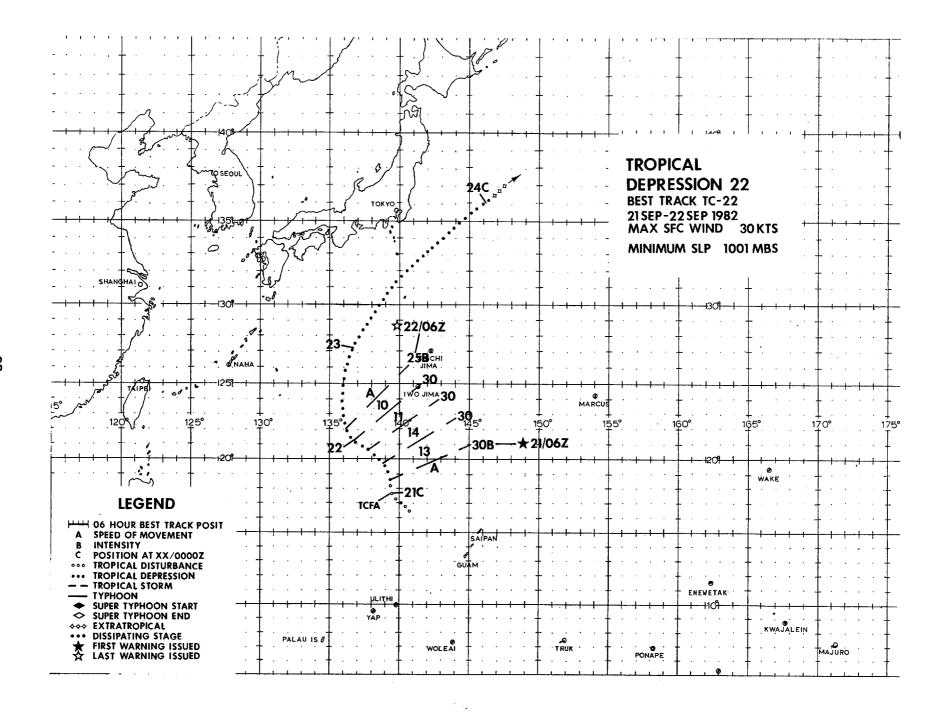


Figure 3-21-1. Tropical Storm Lola at the point of recurvature as a cold front approaches from the northwest. 1704362 September (NOAA 7 visual imagery).



Tropical Depression 22 began its brief existence as a significant tropical cyclone in the wake of Typhoon Ken (20). An exposed low-level circulation, with convection displaced well west-southwest of the circulation center, was a persistent feature of this system throughout its lifetime as it was apparently dominated by Typhoon Ken's upper-level outflow.

The first aircraft investigative mission flown on 20 September closed a surface circulation with 15 kt (8 m/sec) winds and a central sea level pressure of 1002 mb. The mission Aerial Reconnaissance Weather Officer reported no mid- or upper-level cloud features associated with the 10w-level center. A second investigative flight on 21 September reported winds had increased to 20 kt (10 m/sec) near the circulation center, while winds of 30 kt (15 m/sec) were evident 70 nm (130 km) south of the center. Convection was displaced 90 nm (167 km) west-southwest of the low-level center but was increasing in intensity. This information prompted the issuance of a Tropical Cyclone Formation Alert (TCFA) at 2101232.

Subsequent synoptic data carried a growing number of reports of 30 kt (15 m/sec) winds in the alert area, plus visual satellite imagery at 210300Z depicted a strengthening of the low-level circulation. Based on these factors, the first warning was issued

on Tropical Depression 22 at 210600Z calling for movement toward the northwest. At this time Typhoon Ken was 900 nm (1667 km) to the west-northwest but minimal interaction was expected. However, Ken's outflow pattern was expected to inhibit rapid development of Tropical Depression 22. Therefore intensification to only 55 kt (28 m/sec) was forecast by the end of 72 hours. (See Figure 3-22-1).

During the ensuing 24-hour period aircraft and satellite data showed no indication of vertical development. Synoptic data at 2200002 indicated that surface winds had weakened to 20 kt (10 m/sec) and surface pressures had not changed from the previous 1002 mb level. Because Tropical Depression 22 was continuing to move more rapidly toward the north-northeast, little opportunity for further development was expected. Additionally, satellite imagery continued to show a weakening of the low-level circulation, thus warnings were suspended at 2207002.

After dissipating as a significant tropical cyclone, a weak convective disturbance persisted and began accelerating northeastward. This disturbance did maintain enough integrity to induce the development of a small extratropical system upon merging with a frontal zone southeast of Japan on 24 September.

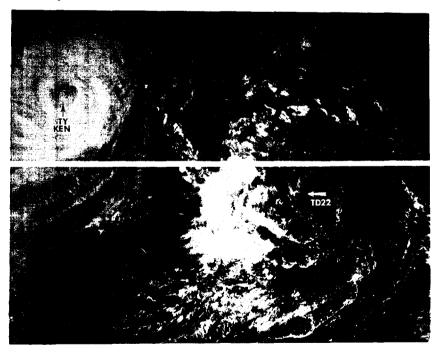
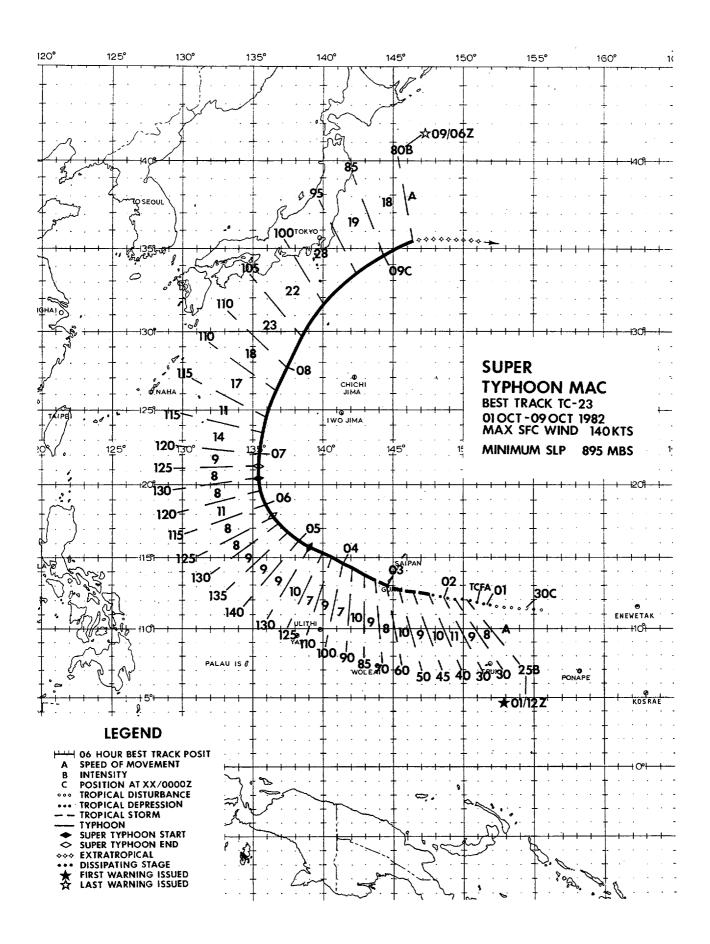


Figure 3-22-1. Tropical Depression 22 at 30 kt (15 m/sec) intensity as an exposed low-level circulation. Convection is displaced to the west-southwest. Typhoon Ken can be seen 900 nm (1667 km) to the northwest. 210529Z September (NOAA 7 visual imagery).



Super Typhoon Mac was spawned to the east of Ponape (WMO 91348) in an area which had been under close scrutiny by the Joint Typhoon Warning Center for several days. A persistent surface circulation, with an associated upper-level anticyclone, was closely monitored beginning on 28 September. No signs of significant development were evident until satellite imagery on 1 October revealed that the convective pattern was more conducive to intensification and the upper-level outflow signature was supportive of sustained further growth of the disturbance. Based upon this evidence, a Tropical Cyclone Formation Alert was issued at 010635Z. Further intensification was rapid; the first warning on Tropical Depression 23 was issued at 0112002 after nearby shipboard observations indicated that the surface pressure was as low as 1003 mb and that surface winds had risen to 25 kt (13 m/sec).

Because of Tropical Depression 23's location (near 12N 150E), it became apparent that the system presented a significant threat to the island of Guam. During its formative stages, Mac had moved somewhat erratically but had tracked generally west-northwestward under the influence of steering currents associated with the southern periphery of the subtropical ridge. Initially, numerical forecast fields indicated there would be no change in this steering flow over the next three days and Mac was predicted to continue on a westnorthwest course. During this period, rapid intensification was expected due to favorable upper- and lower-level conditions: the relatively small upper-level anticyclone over the system was in close proximity to strong upper-level outflow channels; and at the surface, there was a massive area of inflow from the west with virtually no competition from other circulation centers in the area (Figure 3-23-1).

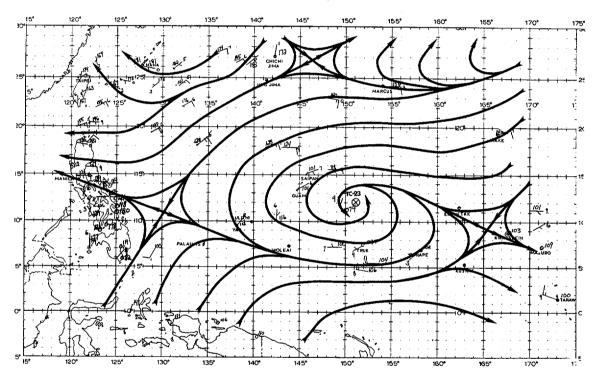


Figure 3-23-1. 0112002 October surface analysis. Wind speeds are in knots.

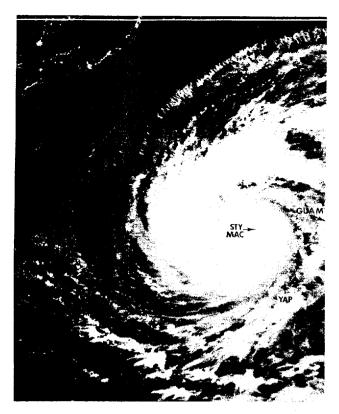


Figure 3-23-2. Super Typhoon Mac is shown 11 hours after maximum intensity, 0506407 October (NOAA 7 visual imagery).

Initial forecasts proved accurate as Mac passed 10 nm (19 km) southwest of Guam at 030000Z. Although maximum sustained winds within Mac were estimated to be 60 kt (31 m/sec) at closest point of approach to Guam, the highest sustained winds recorded at Nimitz Hill (24 nm (44 km) from Mac's center) were just 30 kt (15 m/sec). Guam experienced little structural or equipment damage because of the fortunate combination of adequate advance warning and preparation, and the compact wind radii associated with Mac. However, crop damage was extensive in the southern part of the island due to the heavy rains and relatively high winds experienced there; the Government of Guam Department of Agriculture estimated damages at 1.5 million dollars.

Mac continued to intensify rapidly after passing Guam. In two days, from the 3rd to the 5th, Mac more than doubled its intensity from 60 kt (31 m/sec) to 140 kt (72 m/sec) (Figure 3-23-2). Figure 3-23-3 shows the trends of various meteorological parameters over Mac's lifetime. The 700 mb data and minimum sea level pressure (MSLP) were derived from reconnaissance aircraft data. Items of particular note include: the dewpoint depression of 28°C, one of the largest ever recorded in a tropical cyclone; the redevelopment to super typhoon strength, only the sixth recorded instance since 1958; the correspondence of the MSLP trends and intensity peaks; and the relatively smooth intensity trend as presented by Dvorak analyses.

During its period of rapid intensification, Mac began to assume a more northwestward track in response to a developing weakness in the subtropical ridge near the Ryukyu Islands. On 5 and 6 October, after having attained super typhoon strength, Mac turned sharply north-northeastward and accelerated. Beginning with forecasts issued on 4 October, which keyed on the break in the subtropical ridge, JTWC anticipated this movement quite well. Because of a deep westerly flow which extended well to the south of the main islands of Japan, Mac never posed a threat to Japan even though it

appeared to be right on course toward Tokyo until 8 October.

Once embedded in the mid-latitude westerly flow, Mac accelerated to a maximum forward speed of 28 kt (52 km/hr) but lost little of its intensity. Two days after its recurvature, Mac's intensity had dropped only 30 kt (15 m/sec), i.e. from 125 to 95 kt (64 to 49 m/sec); although Mac remained intense, it rapidly lost its tropical characteristics and transitioned into an extratropical system on 9 October.

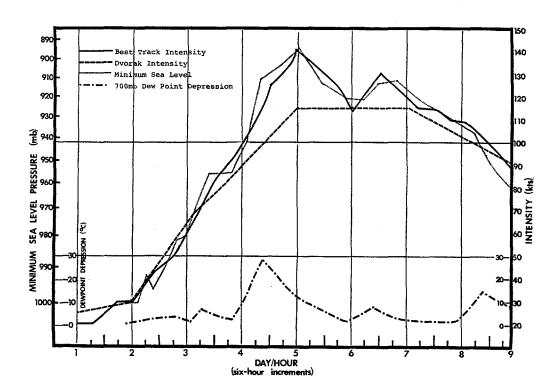
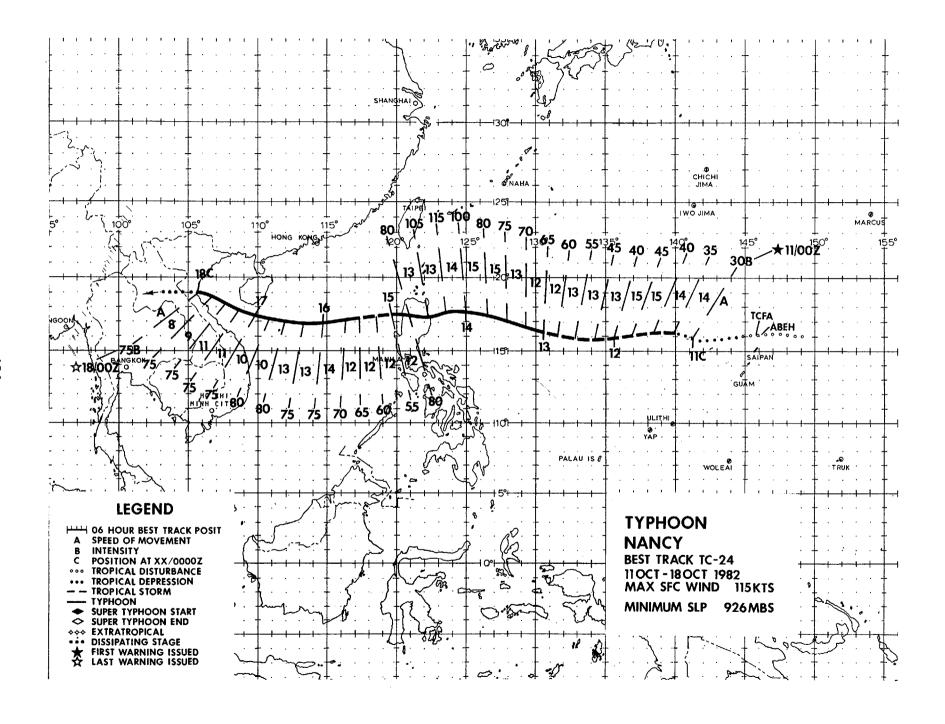


Figure 3-23-3. Comparisons of best track intensities, Dvorak intensity estimates, minimum sea level pressures, and 700 mb dewpoint depressions for the first eight days of Mac's existence.



A large area of weakly organized convection consolidated into a single mass on 8 October near 17N 158E in a region made favorable for cyclogenesis by the divergence aloft near an upper cold low. This convection was strong enough to become separate from the surrounding cloudiness lying south of an upper cold low embedded within a tropical upper-tropospheric trough (TUTT). Sustained surface pressure falls, however, weren't realized as this convective area degenerated later that day into a random pattern of cloudiness. The upper cold low continued to drift westward and was located

near 148E on 10 October. This time the conditions were right for cyclogenesis — the upper-level divergence coupled with a pre-existing low-level cyclonic circulation and a tropical depression formed in the enhanced cloudiness just south of the TUTT. This cloudiness was separate and distinct from the routinely observed maximum cloud zone, which lay to the south, between 7N and 10N.

A Tropical Cyclone Formation Alert was issued at 100730Z for the area 200 nm (370 km) north of Guam due to the 1005 mb surface pressures and the significant

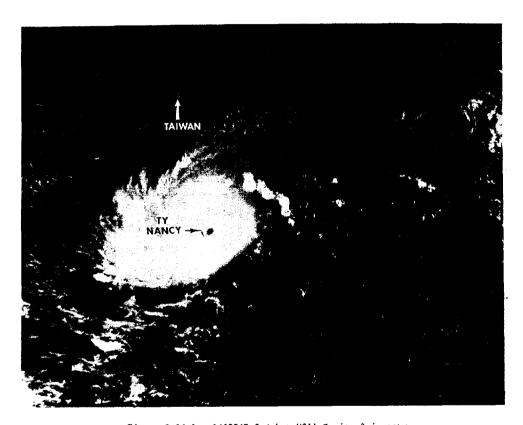


Figure 3-24-1. 1405567 October NOAA 7 visual imagery shows Typhoon Nancy at its peak intensity of 115 kt (59 m/sec) and approximately six hours away from landfall on northern Luzon. Note the island of Taiwan can be seen to the north of Nancy's cloud shields.

increase of cloud pattern organization. Again, because of the sparse conventional data, satellite images had been the key indicator of cyclogenesis and aircraft reconnaissance could not be scheduled to investigate the area until the following day.

The initial reconnaissance aircraft located a closed circulation and surface winds of 25 kt (13 m/sec) which prompted the first warning at 110200Z. Upgrading from tropical depression to tropical storm status followed within six hours, when the follow-on aircraft fix found 35 kt (18 m/sec) winds and a minimum sea level pressure of 999 mb. Nancy stabilized at moderate tropical storm strength and maintained a westward track for the next 24 hours.

Much of Nancy's early warning period was marked by several changes in the basic forecast track. The first four warnings anticipated that

Nancy would track northward toward recurvature; however, due in part to the strengthening of the low-level easterly winds north of Nancy, this forecast movement did not occur and Nancy moved rapidly westward with the low-level steering flow. The next four warnings anticipated a west-northwestward movement and through the Bashi Channel, north of Luzon. This track was abandoned at 130000Z when analysis and numerical prognostic data showed evidence that a midlatitude trough would deepen south of Korea and lessen the influence of the low-level steering on Nancy. Thus until 140600Z (warning 14), the JTWC forecasts showed a pronounced northwestward track toward Taiwan and mainland China. On 14 October, as it became evident that the forecast weakening of the low-level steering current would not materialize, the JTWC forecasts turned toward the west-southwest.

During this period of changing forecast scenarios, Nancy began to intensify. On 13

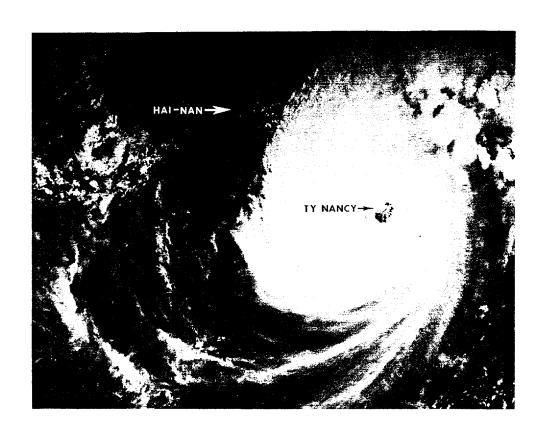


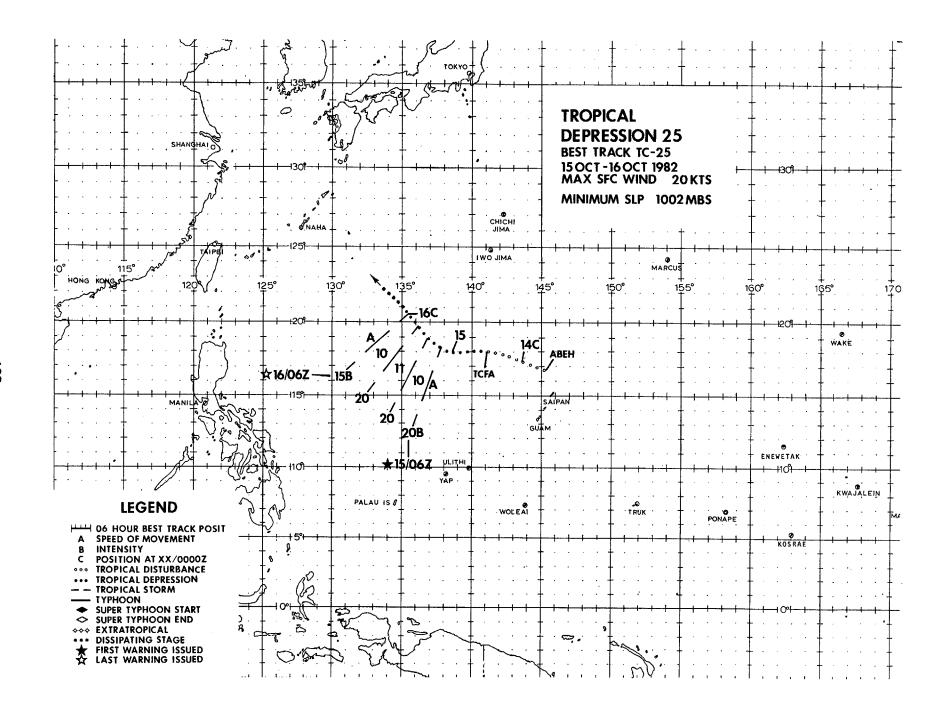
Figure 3-24-2. Typhoon Nancy was located near 17.0N 113.8E or 210 nm (389 km) east-southeast of the island of Hai-Nan at 1607142 October. Hai-Nan island was located on the northwestern edge of Nancy's cirus cloud cover. Note the fair weather as indicated by the small, fair weather cumulus over the island and coastal areas of Vietnam, in sharp contrast to the approaching typhoon. (NOAA 7 visual imagery).

October, Nancy attained typhoon strength and then rapidly deepened to a peak intensity of 115 kt (59 m/sec) just six hours prior to landfall on northeastern Luzon. Nancy was reduced to tropical storm strength by a rugged overland transit, but was quick to regain typhoon strength upon reaching the open waters of the South China Sea. Nancy was the most intense typhoon to strike the Republic of the Philippines this year; in its wake, Nancy left at least 110 dead, 12,000 people homeless, and caused an estimated 46 million dollars damage.

The presence of a continuing strong midand upper-level circulation pattern made Nancy's reintensification in the South China Sea possible. At 1612002, Nancy reached a second peak intensity of 80 kt (41 m/sec) as it passed just north of the Paracel Islands (WMO 59981). The influence of a subtropical ridge over

southern China and the continuing presence of of the low-level northeasterly (monsoon) flow across the South China Sea kept Nancy on a westward track until it approached Hai-Nan Island late on 16 October. From near Hai-Nan until landfall, Nancy maintained a slower, northwestward track along the southern periphery of the subtropical ridge.

On 18 October, Nancy crossed the coast of Vietnam 15 nm (38 km) north of the city of Vinh (18.7N 105.7E) in the Nghe Tinh province, causing at least 71 deaths, leaving 194,200 people homeless, and devasting 185 square miles (48,000 hectares) of winter rice crops that wcre ready for harvest. Later satellite imagery (at 180600Z) indicated that Nancy's central convection had dissipated over the mountains of Vietnam.



On 14 October, surface observations indicated a weak circulation center near 18N 141E. Satellite analysis of the area revealed the presence of an upper-level anticyclone with potential to enhance the ventilation of the surface system. Expecting further development once the system attained vertical alignment, JTWC issued a Tropical Cyclone Formation Alert (TCFA) at 141200Z.

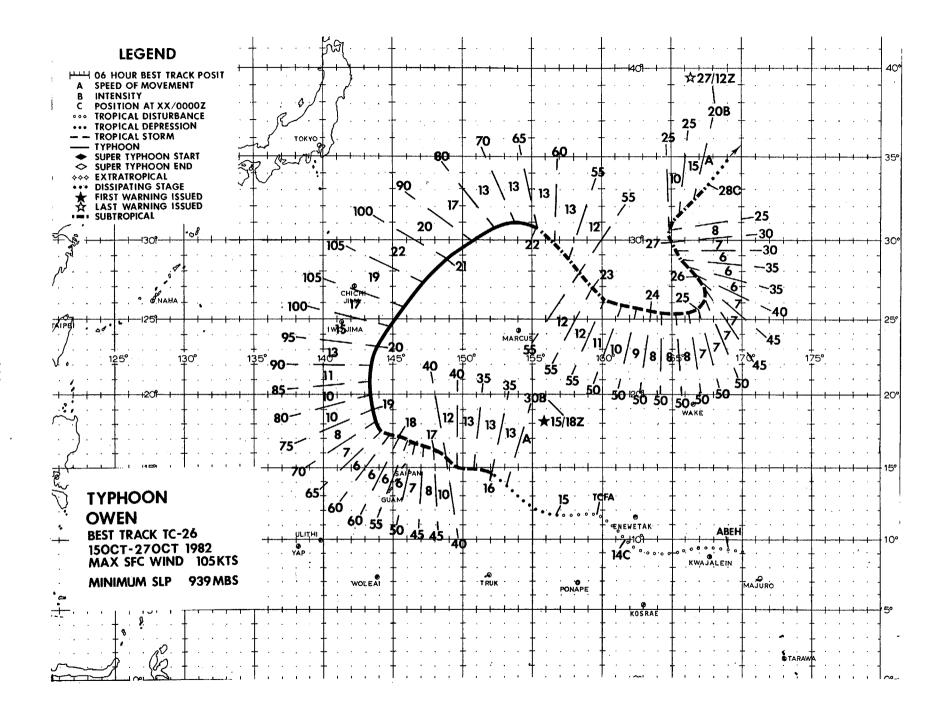
Aircraft reconnaissance at 142336Z located a weak surface circulation near 18N 139E, with central pressures estimated to be near 1006 mb. The initial warning on Tropical Depression 25 was issued after 150000Z satellite imagery showed the convective area near the center was becoming more organized.

Subsequent aircraft reconnaissance of the system at 1509002 reported maximum winds less than 10 kt (5 m/sec), and the circulation center could not be fixed by either winds or pressures. Satellite imagery indicated that the convection associated with the system had greatly weakened, and the overall organization had decreased. The subsequent warning, at 1512002, anticipated further

weakening of Tropical Depression 25 and the forecast period was shortened to 24 hours. On the following day, visual satellite imagery at 1600002, with corroborative synoptic data, indicated that Tropical Depression 25 had become a fully exposed low-level circulation with no associated major convection. Thus, the final warning on Tropical Depression 25 was issued at 1606002.

For the next 48 hours, this exposed low-level circulation remained evident on visual satellite imagery, as it progressed to the northwest. Re-development of some convective banding, curving into the system was observed on 18 October. The development of a weak anticyclonic pattern aloft prompted the issuance of a TCFA for the area, near 21N 134E, at 180800Z. A low-level aircraft investigative mission was conducted at 190200Z, but was unable to locate a closed circulation center.

Early on 19 October, when the remains of Tropical Depression 25 were entrained into the expanding low-level inflow pattern associated with Typhoon Owen (26), the TCFA was cancelled.



Typhoon Owen culminated an active 14-week period (22 July through 27 October) during which 17 tropical cyclones reached warning status in the western North Pacific. During this period, only 10 calendar days did not have at least one tropical cyclone in warning status, with five days (26 to 30 September) the longest period without warnings. So obvious was the cessation of this period that four weeks elapsed between the final warning on Owen and the initial warning on the next tropical cyclone, Pamela (27).

Owen developed from a disturbance which was first detected on 13 October east of Kwajalein Atoll. On 14 October increased convective organization became evident on satellite imagery and, at 141200Z, a Tropical Cyclone Formation Alert was issued. During the subsequent 36-hour period, the disturbance slowly organized, e.g. a reconnaissance aircraft investigative mission conducted on 14 October located a weak surface circulation approximately 100 nm (185 km) east of the convective center. However, by 151800Z the convective features were indicative of a

system of sufficient intensity to warrant transition to warning status, thus the initial warning was issued for Tropical Depression 26.

During the first 24 hours in warning status, positioning from aircraft and satellite data became more consistent, e.g. the 1523172 aircraft fix was located approximately 90 nm (167 km) east of the 160002 satellite fix; by 1621002 the difference was less than 20 nm (37 km). As Figure 3-26-1 depicts, a strong upper-level tilt to the south was evident, but low-level cumulus cloud lines, detected north of the main convective mass, provided evidence of Owen's continued organization. Owen is another example of non-vertical alignment of developing tropical cyclones (Huntley and Diercks, 1981). Such systems normally become better aligned as they mature and Owen was no exception; on 18 and 19 October, the tilt became less evident and Owen responded by attaining typhoon strength at 1812002 and developing a banding-type eye on 19 October.

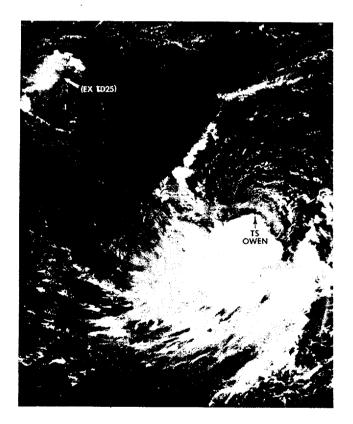


Figure 3-26-1. Low-level cumulus cloud lines can be seen entering Owen's center while the main convective features are displaced equatorward of the low-level center. Strong upper-level northeasterly winds are providing a unidirectional outflow channel toward the southwest. 1705202 October (NOAA 7 visual imagery).

While Owen was aligning in the vertical, it also began to slow its forward movement appreciably, from 13 to 6 kt (24 to 11 km/hr). Track forecasts (describing a west-northwest movement) were adequate until the system reached 17.5N 144E at 181200Z, when Owen turned sharply northward. Although most forecasts up to this point had anticipated an eventual northward movement, none fully anticipated the extent of Owen's turn on 18 October. This movement can be related to the development of a blocking high east of Japan. (Actually, the FNOC prognostic series more than adequately forecast this development, but an extension of the mid-tropospheric (500 mb) subtropical ridge north of Owen and westward to 135E was seen by forecasters as an inhibiting factor to more significant northward movement). development of the block increased the south-to-north flow in the mid-levels, leading to an erosion of the subtropical ridge north of Owen and thus, allowed the typhoon to move northward.

From 19 to 21 October, Owen accelerated northward toward an anticipated extratropical transition, reaching a peak intensity of 105 kt (54 m/sec) (Figure 3-26-2). Speed of movement forecasts during this period were quite good and fully anticipated Owen's acceleration from 10 to 22 kt (19 to 41 km/hr). However, the track forecasts did not fair as well, primarily due to the conflicting options presented by the flow around the block. Figure 3-26-3 shows the configuration of the mid-tropospheric (500 mb) flow near the block on 20 October, as well as the various forecast tracks issued (from 190000Z to 210000Z) and Owen's eventual best track. As can be seen, forecasts 14 through 17 tended toward the east (south of the blocking high), forecasts 18 and 19 anticipated that Owen would move northward toward an occluded low near Kamchatka, and forecasts 20 through 22 seemed to split the difference. On 21 October, Owen's anticipated extratropical transition was well underway; its associated convective features



Figure 3-26-2. Typhoon Owen near maximum intensity, 710 nm (1315 km) south-southeast of Tokyo, Japan at 200443Z October (NOAA 7 visual imagery)

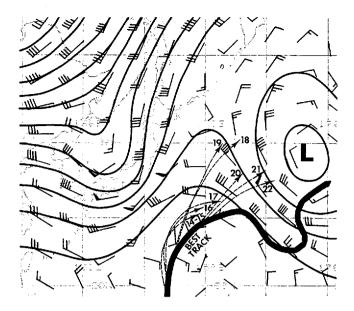


Figure 3-26-3. FNOC 500 mb analysis at 2000002 October with warnings 14 through 22 and Owen's best track superimposed. Wind speeds in knots.

were being sheared northward (away from the surface center), low-level inflow from the mid-latitudes dominated Owen's surface circulation pattern, and aircraft reports showed the band of maximum winds moving further from the center (135 nm (232 km) at 210704z).

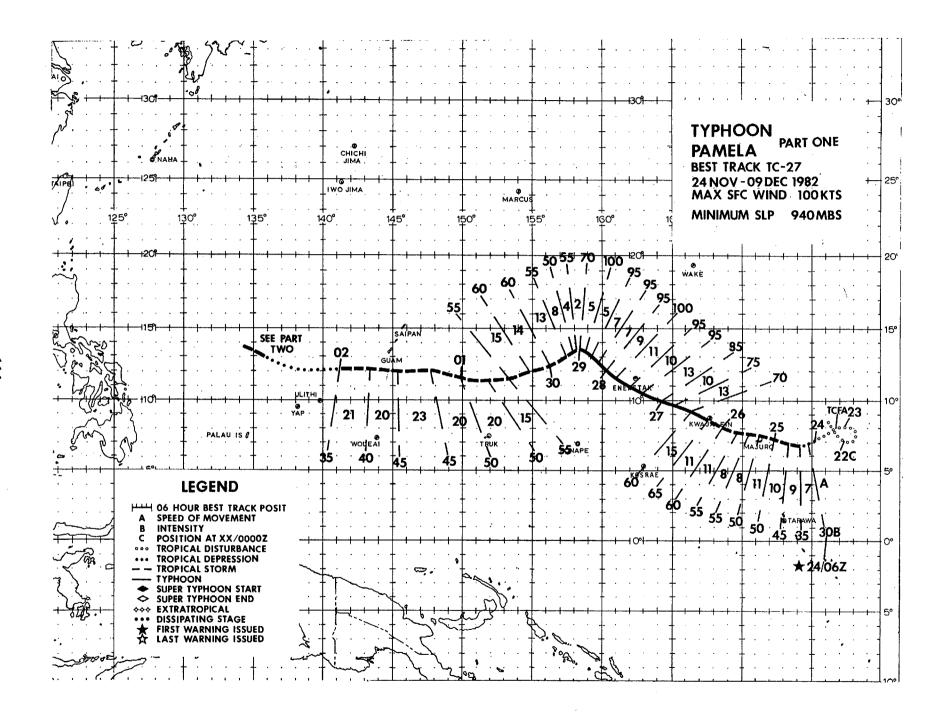
Numbered tropical cyclone warnings ended at 220000Z when satellite imagery indicated that Owen had transitioned to an extratropical low. During the next two days, extratropical gale warnings were issued by the NOCC Operations Department as the system tracked southeastward and south of the blocking high. On 23 October an increase in convective activity was noted equatorward of the system center (Figure 3-26-4) and during the next 24 hours it was closely monitored for possible reclassification as "tropical" vice "extratropical" or "subtropical" cyclone. The decision to redesignate Owen as a tropical cyclone occurred on

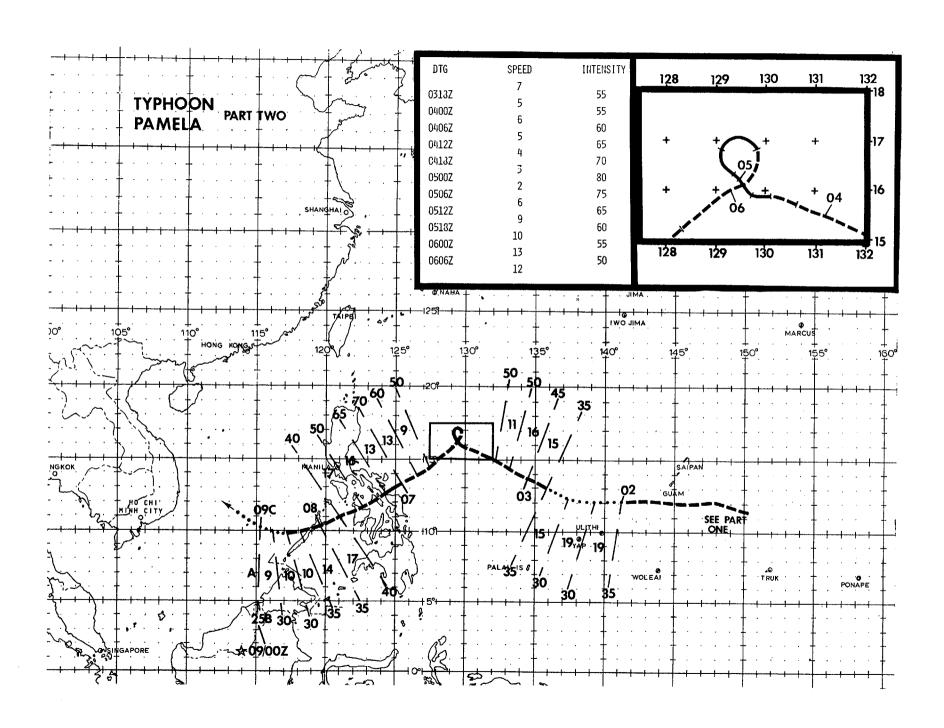
24 October when the convection began to reorganize around the system's center.

For the next 24 hours, Owen tracked eastward and maintained an estimated 50 kt (26 m/sec) intensity. Satellite fixes on 25 October began to indicate a pronounced northward track and a steady decrease in convective activity. From 25 to 27 October, the block, which had dominated the region for more than one week, began to break down and move eastward toward the International Dateline. As Owen moved northnorthwestward then northeastward, it slowly weakened and dissipated in the warm sector of an advancing frontal system. The final tropical cyclone warning was issued for Owen (as Tropical Depression 26) at 271200Z some 1400 nm (2593 km) north of its point of initial detection after completing a track in excess of 3600 nm (6668 km).



Figure 3-26-4. At 2403552 October, a significant increase in convection is evident near the system's center; at the time Owen was in warning status as an extratropical low (NOAA 7 visual imagery).





Typhoon Pamela, the 27th significant tropical cyclone of the season, formed east of the Marshall Islands on 24 November. Uncommon for a late season tropical cyclone, Pamela went on to become the longest running, in terms of time and distance, tropical cyclone of the year before dissipating in the South China Sea on 9 December. During its active warning period, Pamela was upgraded to typhoon status on four distinct occasions (reduced to three in post-analysis), a very rare phenomenon.

Development was first observed on 21 November with the formation of an upper-level anticyclone which had some convective activity along its northern outflow band. Visual satellite imagery on 22 November showed a low-level circulation was present near 6N 177E. During the next 48 hours, this disturbance lingered in the region east of 175E with convective activity fluctuating near the center; however, a slow increase in organization, conducive to further development, was observed.

The slow development of this disturbance is attributed to the proximity of Hurricane Iwa (04C) in the eastern North Pacific. As Iwa moved northeastward and passed the Hawaiian Islands, the disturbance (Pamela) began moving westward. A noticeable increase in convection was observed, leading to the

issuance of a Tropical Cyclone Formation Alert at 230600Z for an area east of Majuro Atoll. The system further organized, thus prompting the initial warning on Tropical Depression 27 at 240600Z. When the system developed a central convective feature, accompanied by a well-defined upper-level outflow pattern, it was upgraded to Tropical Storm Pamela at 241200Z.

The first several warnings called for movement toward the west-northwest with gradual intensification. These warnings were based on a forecast weakening of the subtropical ridge northwest of the system under the influence of a mid-latitude trough moving eastward from Japan. Indeed, Pamela moved west-northwestward through the Marshall Islands in the ensuing 84 hours. Satellite and aircraft reconnaissance data confirmed the gradual intensification of the system, with Pamela attaining typhoon status at 2606002 while passing approximately 60 nm (111 km) south-southeast of Kwajelein Atoll. By the time Pamela passed 35 nm (65 km) southwest of Enewetak Atoll at 271200Z, its intensity was estimated (from aircraft data) to be 95 kt (49 m/sec) (Figure 3-27-1). Initial reports from the Marshall Islands indicated moderate to severe damage to buildings and crops from those islands affected by Pamela's passage, but there were no reports of loss of life.

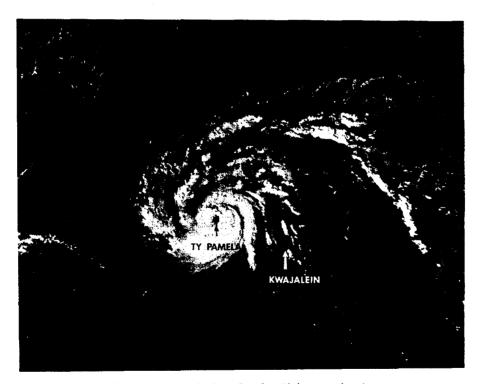


Figure 3-27-1. Typhoon Pamela, 15 hours prior to reaching maximum intensity of 100 kts [51 m/sec], 2703487 November (NOAA 7 visual imagery).

Once past the Marshall Islands, Pamela's forward speed began to slow as the system started to come under the influence of a mid-latitude trough passing to the north. Pamela approached 19N it began to rapidly weaken as it encountered a mid- to upper-level shear zone associated with the trough. Evidence of the rapidity with which Pamela weakened is seen in the aircraft reconnaissance data. At 282105Z, a central pressure of 950 mb and an observed 100 kt (51 m/sec) surface wind were reported. A second reconnaissance mission about nine and onehalf hours later (at 290640%) reported a 979 mb central pressure and observed surface winds of only 50 kt (26 m/sec). This second report necessitated the downgrading of Pamela to tropical storm status on the subsequent warning. A much-weakened Pamela then moved toward the southwest and began to accelerate after breaking away from the effects of the trough and shear zone. This movement was in response to a strong northeast monsoonal flow which was present in the wake of the eastward-moving mid-latitude trough.

Commencing with the 291800Z warning, Pamela was forecast to reintensify and move westward along the southern periphery of the subtropical ridge, eventually passing near the island of Guam. The residents of Guam, remembering the devastation caused by Super Typhoon Pamela (May, 1976), had been nervously watching "Pamela's" progress since its designation while still some 1800 nm (3335 km) east of Guam. Needless-to-say, island residents began to prepare for a possible repeat of the conditions associated with Pamela's 1976 namesake.

Pamela continued to accelerate toward the southwest until 3012002 when it began to move westward. During this period, Pamela continued to weaken; instead of gaining the expected mid- and upper-level support for reintensification, Pamela remained disorganized and the anticapted intensification did not materialize. The 0112002 December 500 mb analysis, for example, did not show any mid-tropospheric circulation center near Pamela's low-level vortex.

Although Pamela was still weakening, it was considered a potentially dangerous tropical cyclone. At 011200Z, Pamela was located 90 nm (169 km) southeast of Guam and was moving westward at 23 kt (42 km/hr); its closest point of approach (to Guam) came two hours later with the maximum recorded wind (gust) of 40 kt (21 m/sec), far below the 138 kt (71 m/sec) gust observed during Super Typhoon Pamela in 1976.

At 011532%, a reconnaissance aircraft was able to locate Pamela's 700 mb center 90 nm (169 km) southwest of Guam. this fix indicated that Pamela's intensity had decreased to 49 kt (21 m/sec). The same aircraft was tasked to provide another fix of the 700 mb center at 0118002 but was unable to close off the circulation (the surface center was not observable due to darkness). The mission Aerial Reconnaissance Weather Officer (ARWO) felt that the 700 mb center had dissipated into a trough, providing further evidence that Pamela was continuing its weakening trend. A "resources permitting" "first-light" aircraft fix was requested for 012200Z. The aircraft orbited south of the main convection until daybreak; then, responding to a satellite position provided to JTWC by Det 1, lWW, the aircraft was able to locate the surface center at 012150Z with an estimated 35 kt (19 m/sec) intensity.

During the next 24 hours, Pamela continued to move westward and weaken. Satellite imagery (Figure 3-27-2) and aircraft reconnaissance data revealed that Pamela had become a tropical depression by 020600Z. During this period, JTWC was forecasting Pamela to dissipate as a significant tropical cyclone over water within 48 hours.

Pamela, again as Tropical Depression 27, started to slow its forward speed and began to move toward the northwest, responding to another mid-latitude trough moving off the coast of Asia. Once this northwest movement began, indications that Pamela might reintensify became evident. First, the 0212002 500 mb analysis suggested that a mid-tropospheric circulation had reformed; and second, aircraft reconnaissance at 0221262 was once again able to close off a 700 mb center with data indicating that an intensity of 35 kt (18 m/sec) had been reached. Later reconnaissance aircraft missions showed that Pamela was continuing its reintensification and it passed from tropical storm status to typhoon status (again) at 041200Z. During this period of reintensification, Pamela reached a maximum intensity of 80 kt (41 m/sec) while concurrently slowing to a minimum speed of 2 kt (4 km/hr) at 0500002 (Figure 3-27-3).

JTWC objective forecast aids and FNOC prognostic fields began to indicate the potential for recurvature once Pamela approached the axis of the (mid-tropospheric) subtropical ridge, near 17N. The 040000Z warning was the first to reflect a recurvature scenario. The numerical prognostic

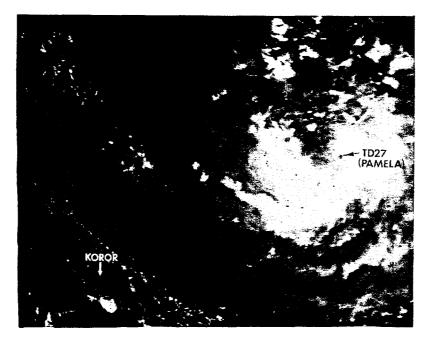


Figure 3-27-2. Pamela, now Tropical Depression 27, with estimated intensity of 30 kts (15 m/sec). 0:0611Z December (NOAA 7 visual imagery).

fields, from which this scenario was derived, forecast the subtropical ridge to weaken at all levels as a mid-latitude trough deepened in the East China Sea. This meteorological situation would allow Pamela to recurve toward the northeast, accelerate, and undergo an extratropical transition. However, the low-level (850 mb and below) ridge did not weaken as indicated by the prognostic series, and Pamela went on to complete a small anticyclonic loop and moved southwestward toward the Philippines. Early in the loop, Pamela began to interact with the mid-latitude westerlies and once again the effect of increased vertical wind shear weakened Pamela from 80 kt (41 m/sec) to 50 kt (26 m/sec) over a 30-hour

period. However, as Pamela moved southwestward, the subtropical ridge to the north began to strengthen at all levels, allowing Pamela to reintensify to a typhoon for the third time. Pamela reached a maximum intensity of 70 kt (36 m/sec) about six hours prior to entering the islands of the central Philippines.

As Pamela moved through the Philippines and weakened, Tropical Depression 28 (Roger) formed in the Philippine Sea. The combined effects of interaction with the topography of the islands and a shift in the low-level wind regime toward Roger caused Pamela to weaken rapidly and eventually brought on its dissipation over the South China Sea.

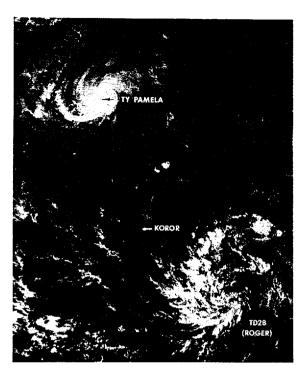
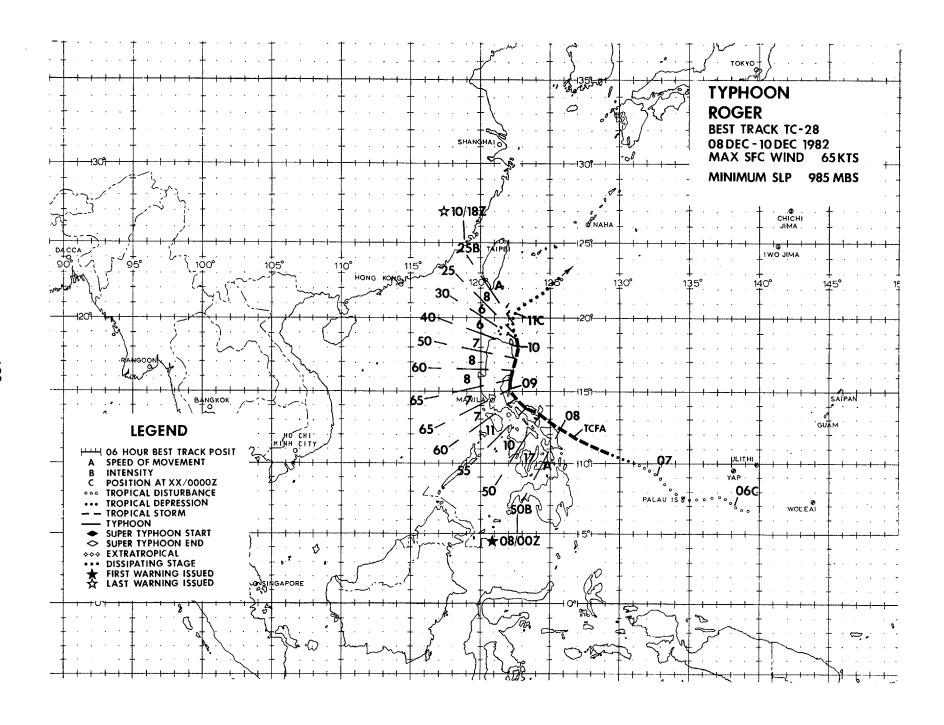


Figure 3-27-3. Typhoon Pamela, nearly six kours after attaining a second maximum intensity of 80 kts (41 m/sec). To the south, this imagery also shows Tyhpoon Roger in its formative stages. 0505342 December (NOAA 7 visual imagery).



Roger was particularly interesting in that it followed closely on the heels of Typhoon Pamela (27). Both systems remained south of the subtropical ridge axis, moved to a mid-tropospheric neutral point near northern Luzon and were profoundly affected by the passage of a mid-latitude trough. In sharp contrast to Pamela, which was a long-lived, significant tropical cyclone, Roger remained an incipient circulation for four days, and required three Tropical Cyclone Formation Alerts (TCFA) before attaining warning status on 7 December.

The first hint of formation occurred at 030600Z when a large area of convection appeared in an upper-level divergence pattern 1200 nm (2222 km) southeast cf Typhoon Pamela. This pattern persisted aloft and drifted west-northwestward at 240 nm (444 km) per day. The low-level circulation center was displaced 150 nm (278 km) south of the cloud

system center. This incongruity, or tilt, was present until 7 December and was, most probably, responsible for the long period of slow development.

The persistent convection feeding an outflow pattern aloft developed into a cloud system center, which prompted a TCFA at 04200Z and its reissuance for relocation at 050800Z. Development was arrested late on 5 December and the TCFA was cancelled at 350600Z. The upper-level mechanism (troughing off Asia) that was inhibiting Roger's development (in addition to contributing to its vertical tilt) was also affecting Pamela. During this period, Pamela slowed its forward motion, weakened, and changed course from the northwest to the southwest along the periphery of the northeast monsoon. By 061600Z Pamela and (formative) Roger had approached to within 600 nm (1111 km) of each other.

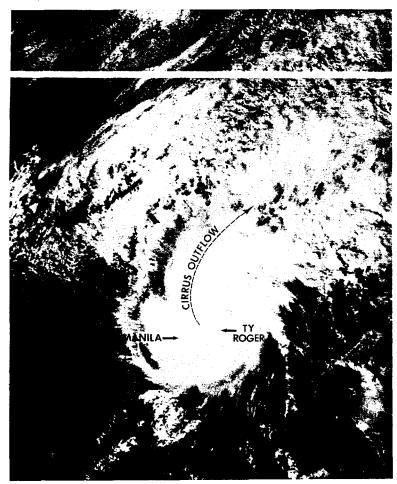


Figure 3-28-1. Expanded visual data of Roger just after reaching typhoon strength off the east coast of Luzon. The extensive low-level cloud deck to the north and northwest of the typhoon's cirrus outflow is embedded in the northeast monsoon. 0906272 December (NOAA 1 visual imagery)

During the next 24 hours the conditions for tropical cyclone development were favorable. Rawinsonde data from southwestern Taiwan (Tung-Chiang, Taiwan (WMO 46747)) indicated a 40 m height rise at 500 mb and reduced vertical wind shear. While Pamela moved into the central Philippines and weakened, Roger remained over water and underwent rapid intensification. The low-level wind circulation center and the cloud system center became vertically aligned and Roger gained tropical storm strength at 0712002. Because of the sparse conventional data and the system's small maximum wind radius, the Joint Typhoon Warning Center could not verify the change in vertical alignment. a reconnaissance aircraft deployed, a TCFA was issued at 072000Z. The first fix from the aircraft indicated a small, tight, 50 kt (26 m/sec) circulation with a minimum central pressure of 1002 mb, which prompted the initial warning at 080000Z.

Roger continued to move toward the northwest along the coast of the Philippines and intensified to typhoon strength at 090000Z. At 091200Z the 500 mb heights to the north at Tung-Chiang (WMO 46747) began to fall due to an approaching mid-latitude trough; the 700 mb flow had changed from northerly to southerly and the low-level northeast monsoonal flow weakened. Roger weakened to tropical storm intensity and moved northward along the east coast of northern Luzon. Satellite imagery revealed that a long cirrus plume was developing from Roger and streaming northeastward as the vertical shear increased aloft.

Increasing vertical shear, the approaching trough, and southerly low-level steering flow hinted at both recurvature (with sudden acceleration) and rapid shearing. Because of Roger's close proximity to land, aircraft reconnaissance was unable to monitor which scenario was taking place and, as a result, satellite data became the major input to the warnings. This posed a problem for the satellite analysts who could only position the top of the cloud system, which was becoming featureless and shearing off to the east. By 100600Z the cloud system center had been poorly organized for 12 hours and the apparent location of the low-level circulation center was highly suspect. Fortunately, by this time Roger had sufficient land clearance for the aircraft to be used. The fix located a greatly weakened center just off the northeastern tip of Luzon. These data required amendment of the 1006002 warning; downgrading Roger to a tropical depression, and relocating the circulation center 80 nm (148 km) to the northwest. The increasing vertical shear caused by the mid-latitude trough dropping southeastward across mainland China had disrupted the vertical linkage between the upper- and lower-level circulations and displaced the convection to the southeast.

The remains of the system were monitored for regeneration until 1018002 when the final warning was issued. The exposed low-level center continued to track northeastward for a day and was ingested into the frontogenic zone east of Taiwan.

2. NORTH INDIAN OCEAN TROPICAL CYCLONES

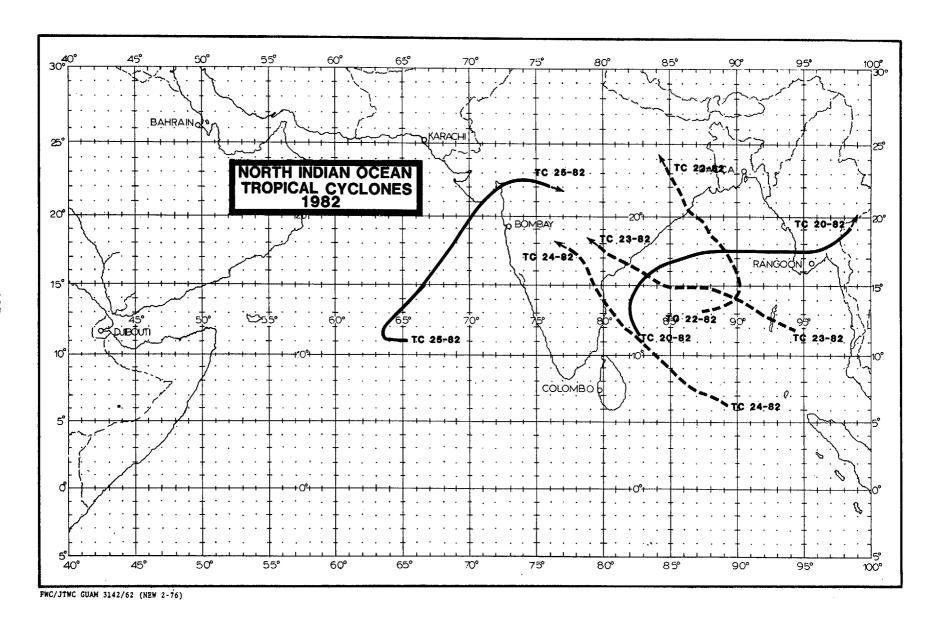
The 1982 North Indian Ocean tropical cyclone season was near normal. Five tropical cyclones reached warning status, two developed during the spring (monsoon) transition season and three developed during the fall transition season. One tropical

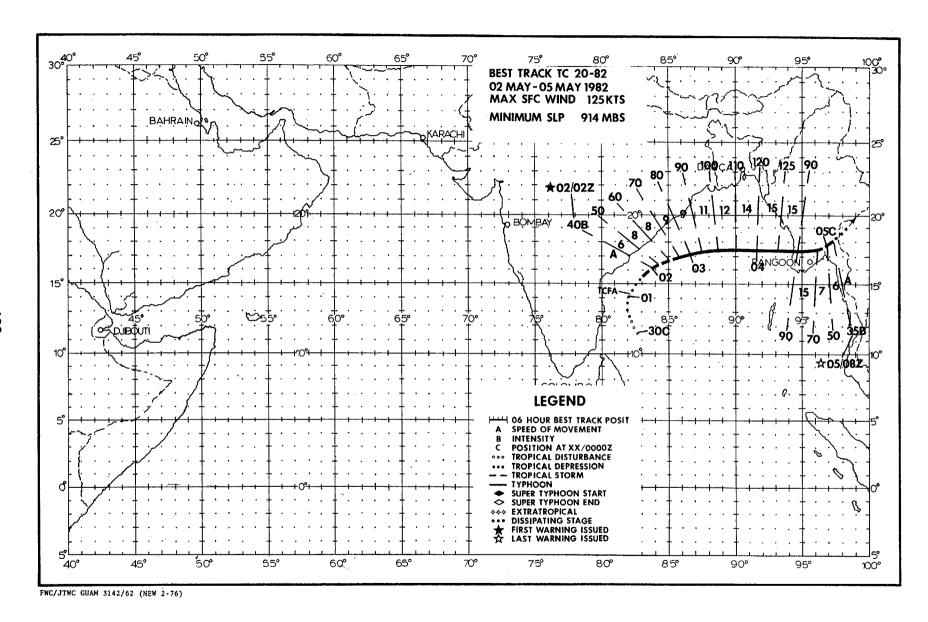
cyclone developed in the Arabian Sea and the remaining four tropical cyclones developed in the Bay of Bengal. Tables 3-6 through 3-8 provide a summary of North Indian Ocean tropical cyclones, Tropical Cyclone Formation Alerts and Warnings.

TABLE 3-6.					NORT	H INC	IAN	OCEAN						_	
1982 SIGNIFICAN	T TRO	PICAL	CYCL	ONES											
TROPICAL CYCLON	<u>е Р</u>	ERIOD	OF W	ARNIN	Г	ALEND AYS O ARNIN	F	NUMBER WARNIN ISSUED	GS	MAXIM SURFA WIND	CE		MATED (MB)	BEST TRAC DISTANCE TRAVELED	
1. TC 20-82		2 MA	.у –	5 MA.Y	•	4		14		125		914		1135	
2. TC 22-82		2 JU	N -	4 JUN		3		8		55		983		482	
3. TC 23-82		14 OC	14 OCT - 16 OCT		•	3		9		50		986		681	
4. TC 24-82		17 oc	T - 1	9 OCT		3	7			50		987		389	
5. TC 25-82		5 NO	v -	9 NOV	•	5		17		90		952		949	
* IN ADDITON, TABLE 3-7. NORTH INDIAN OCEAN ALL TROPICAL CYCLONES 1975-1981 AVERAGE CASES	JAN 0 .1 1			RNING	S WER			CAL CYC	198	s .	NOV 1 1.4 10	DEC 0 .4 3	5 4.6 32		
FORMATION ALERT	S:	Fiv	e of i	the n nto s	ine F ignif	ormat icant	ion tro	Alert	Even cycl	ts dev	elope	đ			·
WARNINGS:		Num	ber o	f war	ning	days: days nes i	with	n egion:		18					
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TABLE 3-8.													
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YEAR	JAN	FEB	MAR	APR	MAY	JUN	JUL	AUG	SEP	OCT	NOV	DEC	TOTAL
1971*	-	_	_		_	0	0	0	0	1	1	0	2
1972*	0	0	0	1	0	Ö	0	0	2	0	1	Ö	4
1973*	0	0	0	0	0	0	0	0	0	1	2	1	4
1974*	0	0	0	0	0	0	0	0	0	0	1	0	1
1975	1	0	0	0	2	0	0	0	0	1	2	0	6
1976	0	0	0	1	0	1	0	0	1	1	0	1	5
1977	0	0	0	0	1	1	0	0	0	1	2	0	5
1978	0	0	0	0	1	0	0	0	0	1	2	0	4
1979	0	0	0	0	1	1	0	0	2	1	2	0	7
1980	0	0	0	0	0	0	0	0	0	0	1	1	2
1981	0	0	0	0	0	0	0	0	0	1	1	1	3 5
1982	0	0	0	0	1	1	0	0	0	2	1	0	5
1975-1982													
AVERAGE	.1	-	-	.1	.8	.5	-	-	. 4	1.0	1.4	. 4	4.6
CASES	1	0	0	1	6	4	0	0	3	8	11	3	37

^{*} JTWC warning responsibility began on 4 June 1971 for the Bay of Bengal, east of 90E. As directed by CINCPAC, JTWC issued warnings only for those tropical cyclones that developed or tracked through that portion of the Bay of Bengal. Commencing with the 1975 tropical cyclone season, JTWC's area of responsibility was extended westward to include the western portion of the Bay of Bengal and the entire Arabian Sea.





During late April, the monsoon trough was anchored in the latitudes south of Sri Lanka and extended eastward into the central portion of the Bay of Bengal. On 26 April, an area of convection associated with this trough became suspect and was discussed in the Significant Tropical Weather Advisory (ABEH PGTW); however, center fixes from satellite data were not available until 30 April when an upper-level circulation center was analyzed over the convection. On 1 May, a Tropical Cyclone Formation Alert was issued as a central dense overcast (CDO) formed over the system.

During this period, there was some concern about the actual intensity of the system at the surface. Surface observations from India, Sri Lanka, and throughout the Bay of Bengal indicated light and variable winds close to the developing system and the strongest winds (15 to 20 kt (8 to 10 m/sec)) far removed from the convection. Additionally, satellite fixes lacked continuity in tracking the system and the possibility that a significant surface circulation had not yet established itself seemed very realistic. However, NOAA 7 satellite imagery at 012132Z, received and analyzed at Air Force Global Weather Central (AFGWC), indicated a substantial increase in the system's convective organization which prompted the issuance of the first warning for Tropical Cyclone 20-82 at 0202002. From the initial warning 0202002. From the initial warning position 440 nm (815 km) north-northeast of Sri Lanka, Tropical Cyclone 20-82 moved northeastward, remaining approximately 120 nm (222 km) east of India. Fix positions remained somewhat erratic in the early stages but improved when satellite imagery (021327Z NOAA 7) indicated that an eye had developed. The appearance of the eye also laid to rest any lingering doubts as to whether Tropical

Cyclone 20-82 had developed into a significant tropical cyclone.

Track forecasts for Tropical Cyclone 20-82 were very good. From the first warning, Tropical Cyclone 20-82 was expected to move northeastward and turn more eastward with time. As Tropical Cyclone 20-82 approached 18N, it's movement became virtually eastward across the Bay of Bengal until landfall. While crossing the Bay of Bengal, Tropical Cyclone 20-82 continued to intensify and reached an estimated maximum intensity of 125 kt (64 m/sec) just prior to landfall. Best track intensities were based almost exclusively on Dvorak intensity estimates received from AFGWC and from Detachment 1,1WW, Nimitz Hill, Guam. However, despite the absence of verifying synoptic reports, satellite imagery (Figure 3-29-1) and later, casualty reports from Burma were convincing evidence that Tropical Cyclone 20-82 was a very intense (although quite compact) tropical cyclone.

The value of the meteorological satellite, especially in data sparse regions, has once again proven itself. In the era prior to the availability of imagery from satellites, Tropical Cyclone 20-82 would have been an undetected storm of great intensity that would strike without warning. A news release from Rangoon, Burma on 6 May, reported 7,000 homes destroyed in one township, and 85% of the homes and buildings in another township had their roofs blown away. Elsewhere, along Tropical Cyclone 20-82's path, schools, industries and hospitals were damaged or destroyed. Yet despite this extensive destruction, there were just five deaths reported in a region of the world where loss of human life is frequently in the hundreds from the effects of tropical cyclones.

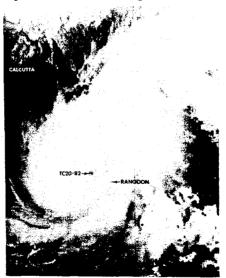
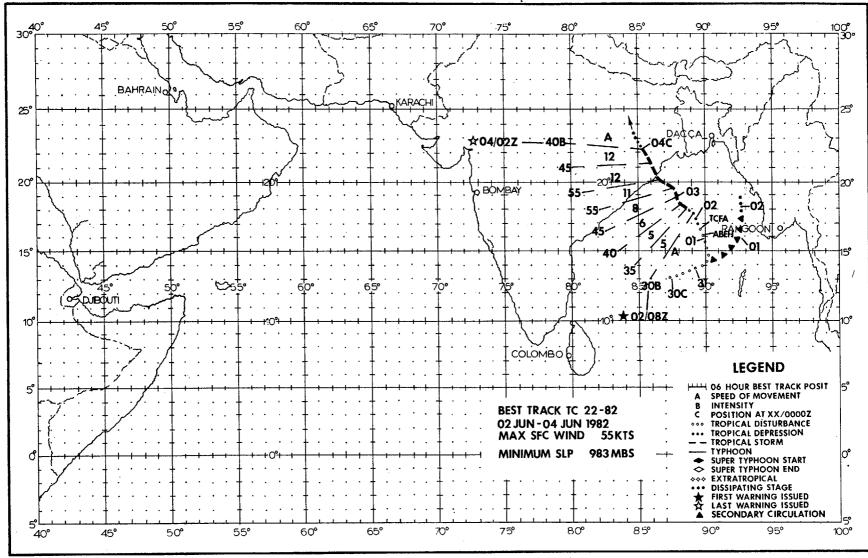


Figure 3-29-1. Tropical Cyclone 20-82 near maximum intensity, just west of Burma, 0504232 May. (NOAA 7 visual satellite imagery from AFGWC, Offutt, AFB, Nebraska)



FWC/JTWC GUAM 3142/62 (NEW 2-76)

Tropical Cyclone 22-82 was the second significant tropical cyclone to develop in the Bay of Bengal during the spring (monsoon) transition season. During the last week of May, there was considerable convective activity over the central Bay of Bengal, resulting in two Tropical Cyclone Formation Alerts (TCFA) that were issued for a disturbance which tracked northeastward and moved into Burma on 29 May.

At 290000Z, a new convective area could be detected on satellite imagery moving out of a monsoon cloud band near 9N in the central Bay. During the ensuing three days, the convective area drifted northward with little evidence of a closed surface circulation. The synoptic environment in the Bay of Bengal at this time was dominated by strong (30 to 40 kt (15 to 21 m/sec)) westerly flow south of 9N, and by a 996 mb heat low over northern India.

By 0106002 June, the convective mass became more organized as an upper-level anticyclone could be analyzed from synoptic data, while visual satellite imagery revealed an exposed low-level circulation some 120 nm (222 km) to the northeast of the convective area. During the next 12 hours, satellite imagery indicated continued convective organization and at 011835Z, a TCFA was issued with the stipulation that the potential for significant tropical

cyclone development was good, provided that either the low-level and upper-level features became better aligned or a new circhlation developed under the convection. By 0208002, when satellite data suggested that the latter case had occurred (the convective system had continued to develop and the exposed low-level circulation could no longer be detected on visual imagery), the first warning was issued for Tropical Cyclone 22-82.

During its short lifetime, Tropical Cyclone 22-82 followed a fairly straight, and climatological, northwestward track. Initially moving at 5 kt (9 km/hr), Tropical Cyclone 22-82 steadily increased it forward speed to 12 kt (22 km/hr) and intensified until making landfall at 031400Z. Satellite data from Air Force Global Weather Central (AFGWC) (Figure 3-30-1) and radar reports received at the Indian regional forecast center, indicated that Tropical Cyclone 22-82 was developing an eye when landfall was made just north of Paradip, 150 nm (278 km) southeast of Calcutta. In the coastal districts near Paradip and Orissa, where the tropical cyclone hit hardest, casuality reports indicated that more than 140 people were killed and more than 500,000 homes were destroyed. After landfall, Tropical Cyclone 22-82 rapidly dissipated as it tracked into the extreme southern portion of the Ganges River Valley.

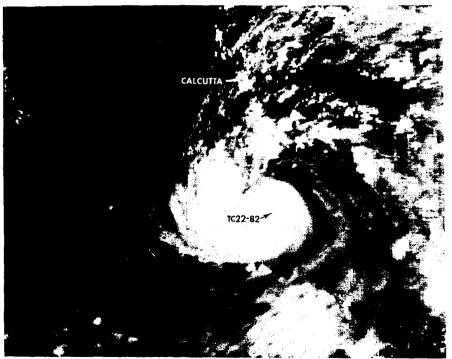
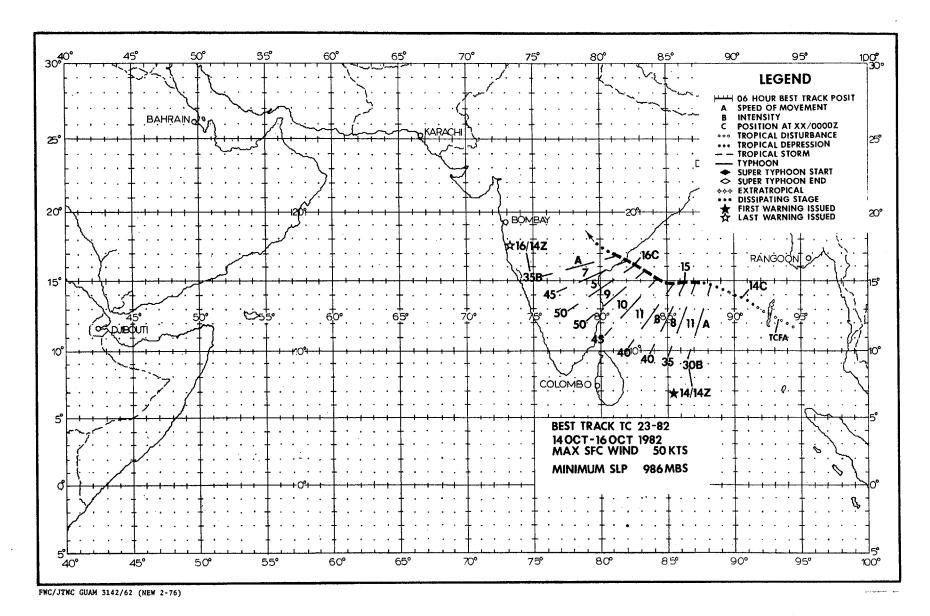


Figure 3-30-1. Tropical Cyclone 22-82 about five hours prior to landfall with an irregular 15 nm (28 km) eye near the center of the central dense overcast, 0308587 June [NOAA 7 visual satellite imagery from AFGWC, Offutt AFB, Nebraska].



The initial stages of Tropical Cyclone 23-82's development were characterized by a persistent upper-level anticyclone and a weak surface disturbance associated with a broad area of convection. Initially detected on 9 October, JTWC tracked a westward-moving surface circulation from the Gulf of Thailand across the Malay Peninsula. Little development was evident from synoptic or satellite data as the system entered the southern Bay of Bengal. On 13 October, convection began to increase and show signs of organization while the system moved west of the Andaman Islands. A Tropical Cyclone Formation Alert was issued at 1306002 when satellite imagery revealed that the system's convection had organized under a more distinctly defined upper-level anticyclone. Late on 14 October satellite imagery showed that a strong central convective feature had developed and that upper-level outflow had increased. Based on these data, and the

expectation of further development, the initial warning was issued at 141400Z for Tropical Cyclone 23-82.

The forecast tracks issued throughout Tropical Cyclone 23-82's lifespan anticipated movement toward the west-northwest in response to a mid-level steering current induced by a subtropical ridge centered over Burma. Tropical Cyclone 23-82 proved to be a "well-behaved" system and followed the forecast track toward the east coast of India. While in warning status Tropical Cyclone 23-82 gradually intensified and reached a peak intensity of 50 kt (26 m/sec) six hours prior to landfall. At approximately 161200Z, Tropical Cyclone 23-82 passed 35 nm (65 km) south of Kakinada, India (WMO 43189) with observed maximum sustained winds of 20 kt (10 m/sec). From Kakinada, Tropical Cyclone 23-82 proceeded inland and gradually dissipated.

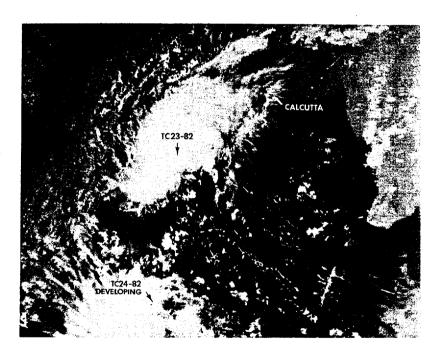
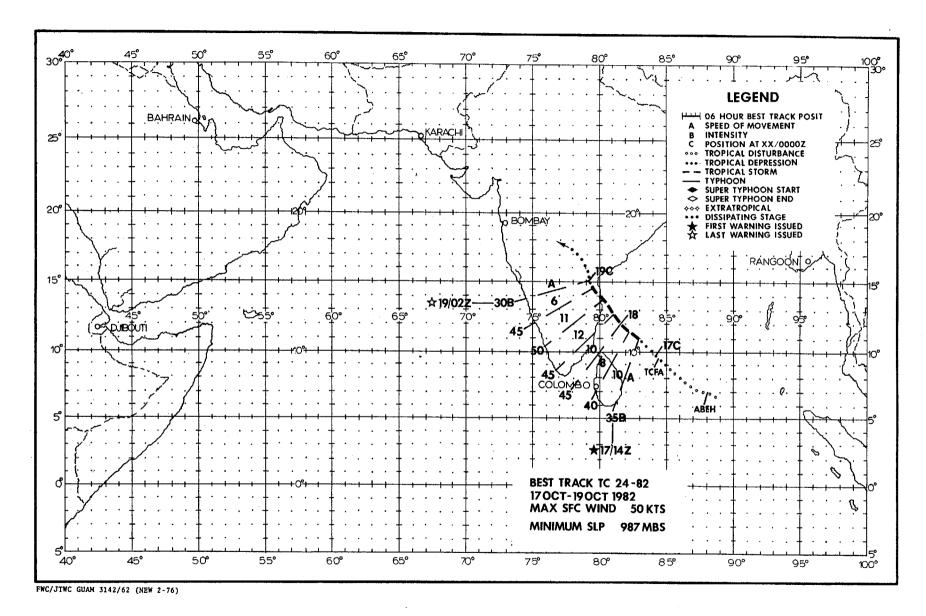


Figure 3-31-1. Tropical Cyclone 23-82 near landfall along the east coast of India with surface winds near 45 kt (23 m/sec). Tropical Cyclone 24-82 can be seen in its formative stages near Sri Lanka, 1608562 October (NOAA 7 visual imagery from AFGWC Offutt AFB, Nebraska).



Tropical Cyclone 24-82 developed from an area of convective activity first observed on 15 October about 400 nm (740 km) east of Sri Lanka in the Bay of Bengal. No surface circulation was present but a weak upperlevel anticyclone was evident on satellite imagery. During the next two days, the area was monitored for further development as it drifted slowly to the northwest. On the 16th, synoptic data and satellite imagery indicated that a loosely organized surface circulation had developed. In combination with the upper-level anticyclone, this circulation was considered to have good potential for intensification and a Tropical Cyclone Formation Alert was issued at 162300Z.

Subsequent satellite imagery indicated that the circulation had come together at the surface and mid-levels. JTWC issued the

first warning on Tropical Cyclone 24-82 at 171400Z. Mid-level steering flow at the time was from the southeast due to the presence of a 500 mb anticyclone over Indochina. Numerical forecast products indicated that this mid-level anticyclone would retain its intensity and location throughout the ensuing 72 hours, thus, Tropical Cyclone 24-82 was forecast to continue moving northwestward. The system did move as expected, making landfall near Sriharikota Island at 181400Z with maximum sustained winds of 50 kt (26 m/sec).

Damage to private dwellings in Nellore District was extensive with an estimated 10,000 collapsed huts. Casualties were reported to be 5 dead and 10 injured. Tropical Cyclone 24-82 continued drifting northwestward after landfall and dissipated over central India.

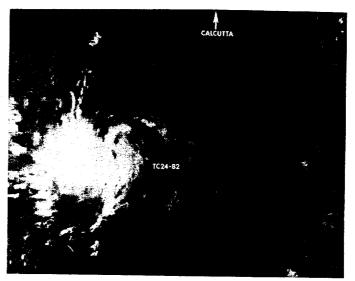
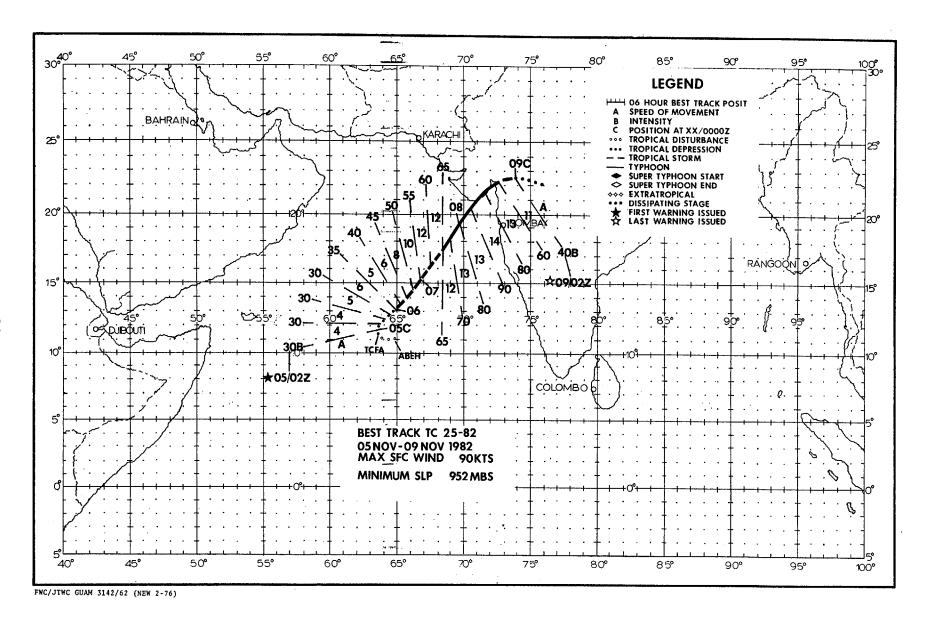


Figure 3-32-1. This satellite imagery indicated Tropical Cyclone 24-82 had organized sufficiently to warrant the issuance of tropical cyclone warnings. 170843Z October (NOAA 7 visual imagery from AFGWC Offutt AFB, Nebraska).



Tropical Cyclone 25-82 developed from an area of loosely organized convection in the central Arabian Sea. Although satellite images indicated that the convection and cloud system organization were increasing, shipboard synoptic reports were the first data to accurately describe the low-level circulation center. At 042000Z November, a Tropical Cyclone Formation Alert was issued when nearby shipboard observations indicated pressures near 1004 mb and winds of 20 kt (10 m/sec), confirming intensity estimates from earlier satellite data. Satellite and synoptic data during the subsequent 12-hour period indicated that development was continuing, prompting the first warning on Tropical Cyclone 25-82 at 050200Z.

Tropical Cyclone 25-82 slowly consolidated during the initial 24-hour period in warning status. Based on guidance from virtually every forecast aid, the first

six warnings anticipated a movement toward the west-northwest. However, once the system organized and satellite fixes became more consistent, it became evident that Tropical Cyclone 25-82 was not moving westward as forecast. In the same time frame, a break developed in the mid-level subtropical ridge, which lay along 23N. As height falls occurred across the northern Arabian Sea coast, the tropical cyclone responded by accelerating toward the northeast and intensifying. Tropical Cyclone 25-82 continued to deepen until landfall at 081000Z near the Indian port city of Veraval (20.9N 70.4E). Veraval was particularly hard hit as the cyclone moved onshore with sustained winds of 90 kt (46 m/sec).

Once overland, and deprived of the low-level moist layer over water, Tropical Cyclone 25-82 rapidly dissipated, leaving in its wake at least 50,000 homes damaged or destroyed and a death toll in excess of 341.

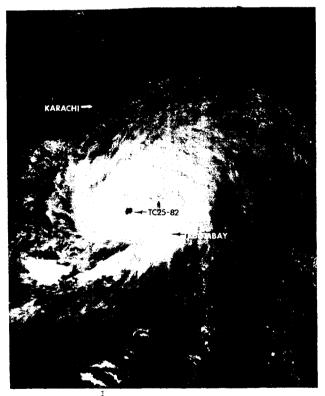
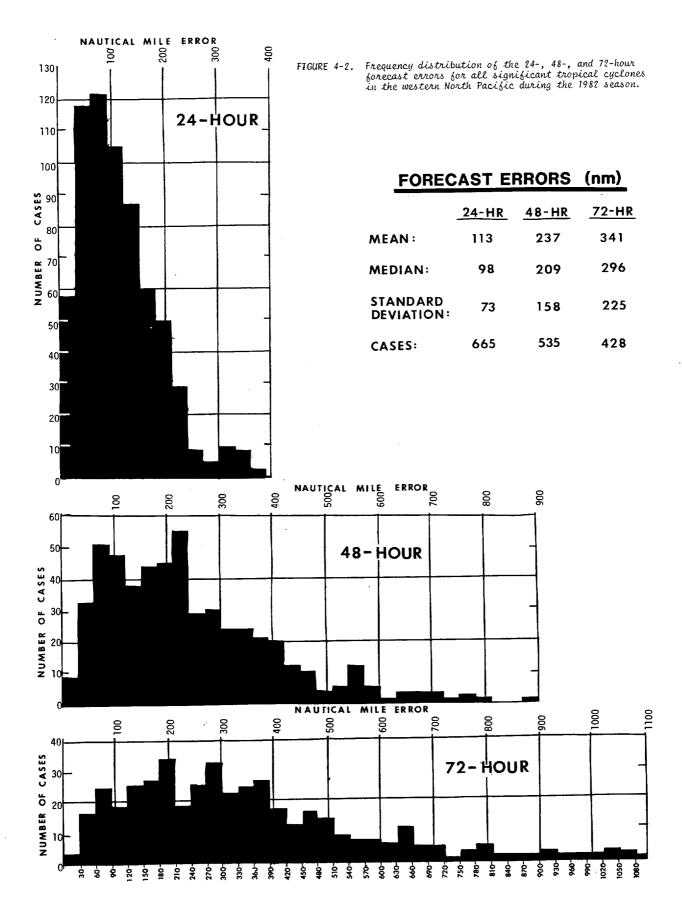


Figure 3-33-1. Tropical Cyclone 25-82 is at peak intensity with maximum winds of 90 kt (46 m/sec) and just making landfall on India's northwestern coast. 0809212 November (NOAA 7 visual imagery from AFGWC Offutt AFB, Nebraska)



CHAPTER IV - SUMMARY OF FORECAST VERIFICATION

1. ANNUAL FORECAST VERIFICATION

a. Western North Pacific Ocean

The positions given for warning times and those at the 24-, 48-, and 72-hour fore-cast times were verified against the post-analysis "best-track" positions at the same valid times. The resultant vector and right angle (track) errors (illustrated in Figure 4-1) were then calculated for each tropical cyclone and are presented in Table 4-1. Figure 4-2 provides the frequency distributions of vector errors for 24-, 48- and 72-hour forecasts of all 1982 tropical cyclones in the western North Pacific. A summation of the mean errors, as calculated

for all tropical cyclones in each year, is shown in Table 4-2 for comparative purposes. The data used in this table are not to be confused with that presented in earlier years where the sample was restricted to tropical cyclones that reached typhoon intensity and then had the forecast errors calculated only for that portion of the life-cycle when the intensity was greater than 34 knots (last published as Table 5-1, 1977 Annual Typhoon Report). A comparison of the results using the truncated data set and those obtained for all tropical cyclones can be seen directly in Table 4-3. The annual mean vector errors are graphed in Figure 4-3.

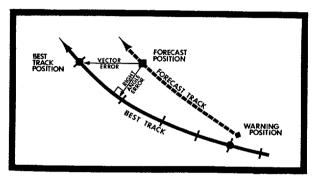


FIGURE 4-1. Illustration of the method to determine vector error and right angle error.

				FOI	RECAST PR	ROR SUMMAR	Y FOR THI	WESTERN	NORTH PAG	TFIC				
						TROPICAL ((ERRORS					
			WARNING			24-HOUR			48-ROUR		72-HOUR			
		POSIT	RT ANGLE ERROR	NR OF WRNGS	POSIT	RT ANGLE ERROR	NR OF WRNGS	POSIT	RT ANGLE ERROR	NR OF WRNGS	POSIT	RT ANGLE ERROR	NR OF WRINGS	
ı.	TY MAMIE	25	14	35	93	48	32	188	86	24	276	115	23	
2.	TY NELSON	24	13	53	95	57	49	180	114	44	170	72	37	
3.	TY ODESSA	29	16	25	228	113	21	520	226	17	742	385	13	
4.	TY PAT	28	24	23	149	134	19	299	237	15	583	394	11	
5.	TY RUBY	27	12	23	144	64	19	275	143	15	425	326	11	
6.	TS TESS	15	9	14	107	73	10	217	142	3	144	41	1	
7.	TS SKIP	16	15	7	95	32	3							
8.	TS VAL	29	22	5	363	33	1							
9.	TS WINONA	22	13	21	100	42	16	175	93	13	224	121	9	
10.	TY ANDY	24	14	32	99	50	28	168	106	23	231	144	19	
11.	STY BESS	18	13	43	121	64	39	267	122	35	396	198	31	
12.	TY CECIL	14	9	39	102	41	33	172	75	30	219	141	23	
13.	TY DOT	22	17	27	108	68	24	218	172	20	262	208	16	
14.	TY ELLIS	14	8	36	76	42	32	171	81	26	263	153	22	
15.	TY FAYE	18	8	50	142	89	41	384	273	33	639	445	27	
16.	TY GORDON	15	11	38	100	63	34	214	101	30	364	210	26	
17.	TS HOPE	19	9	10	186	79	6	426	118	2				
18.	TY IRVING	13	9	44	73	42	40	110	72	35	172	126	32	
19.	TY JUDY	19	15	29	125	73	25	298	126	19	401	262	13	
20.	TY KEN	15	9	37	75	49	33	201	134	29	344	263	25	
21.	TS LOLA	21	14	12	88	68	8	232	152	4				
22.	TD 22	35	21	5	155	83	1							
23.	STY MAC	14	13	32	90	63	28	162	104	24	294	149	20	
24.	TY NANCY	12	10	29	86	74	26	213	175	21	430	333	17	
25.	TD 25	35	33	5	113	119	1							
26.	TY OWEN	24	18	40	146	103	32	36∠	236	24	550	285	18	
27.	TY PAMELA	20	14	60	139	79	56	263	149	45	280	140	34	
28.	TY ROGER	17	17	12	129	116	8	383	329	4				
ALL I	FORECASTS:	19	13	786	113	67	665	237	139	535	341	206	428	

TABLE 4-2. ANNUAL MEAN FORECAST ERRORS (NM) FOR THE WESTERN PACIFIC 24-HOUR 48-HOUR 72-HOUR YEAR VECTOR RIGHT ANGLE VECTOR RIGHT ANGLE VECTOR RIGHT ANGLE 1981* 1982*

^{*} The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

TABLE 4-3.	ANNUAL MEAN FO	RECAST ERRORS (NM) FOR WES	STERN NORTH PAG	CIFIC	
	2	4-HOUR	48	B-HOUR	72	-HOUR
YEAR	ALL	TYPHOON*	ALL	TYPHOON*	ALL	TYPHOON*
1950-58		170				
1959		117**		267**		
1960		177**		354**		
1961		136		274		
1962		3.44		287		476
1963		127		246		374
1964		133		284		429
1965		151		303		418
1966		136		280		432
1967		125		276		414
1968		105		229		337
1969		111		237		349
1970	104	98	190	181	279	272
1971	111	99	212	203	317	308
1972	117	116	245	245	381	382
1973	108	102	197	193	253	245
1974	120	114	226	218	348	351
1975	138	129	288	279	450	442
1976	117	117	230	232	338	336
1977	148	140	283	266	407	390
1978	127	120	271	241	410	459
1979	124	113	226	219	316	319
1980	126	116	243	221	389	362
1981	123	117	220	215	334	342
1982	113	114	237	229	341	337

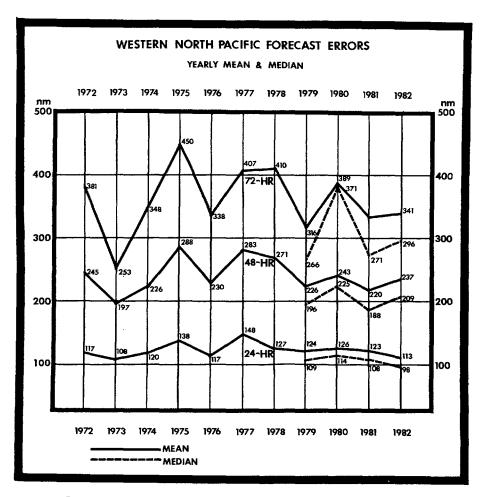


FIGURE 4-3. Annual mean and median vector errors (nm) for all tropical cyclones in the western North Pacific.

b. North Indian Ocean

The positions given for warning times and those at the 24-, 48- and 72-hour valid times were verified for tropical cyclones in the North Indian Ocean by the same methods used for the western North Pacific. It should be noted that due to the low number of North Indian Ocean tropical cyclones,

these error statistics should not be taken as representative of any trend. Table 4-4 is the forecast error summary for the North Indian Ocean and Table 4-5 contains the annual average of forecast errors back through 1971. Vector errors are plotted in Figure 4-4. (Seventy-two hour forecast errors were evaluated for the first time in 1979).

TAB	LE 4-4.												
ł				F	ORECAST E	RROR SUMMA	RY FOR	THE NORTH	INDIAN OCH	AN			
ľ				SIG	NIFICANT	TROPICAL C	YCLONES	OF 1982.	(ERRORS)	(NM NM			
ı			WARNING			24-HOUR			48-HOUR			72-HOUR	
		POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF	POSIT	RT ANGLE	NR OF
ŀ		ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS	ERROR	ERROR	WRNGS
1.	T,C 20-82	23	14	14	118	43	10	283	87	6	340	116	2
2.	TC 22-82	22	16	8	106	36	5	238	85	1			
3.	TC 23-82	34	18	9	88	49	6	151	86	2			
4.	TC 24-82	22	15	7	68	22	.3						
5.	TC 25-82	55	34	17	205	113	13	487	264	9	931	519	5
l													
ALL	FORECASTS	35	21	55		66	37	368	175	18	7 6 2	404	. 7

	ANI	NUAL MEAN FORE	CAST ERROI	RS FOR THE NORT	H INDIAN (CEAN
	24	4-HOUR	41	3-HOUR	7:	2-HOUR
YEAR	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE	VECTOR	RIGHT ANGLE
1971*	232	-	410	-	-	-
1972*	224	101	292	112	-	_
1973*	182	99	299	160	-	-
1974*	137	81	238	146	-	-
1975	145	99	228	144	-	_
1976	138	108	204	159	-	-
1977	122	94	292	214	-	-
1978	133	86	202	128	-	-
1979	151	99	270	202	437	371
1980	115	73	93	87	167	126
1981**	109	65	176	103	197	73
1982**	138	66	368	175	762	404

- * The western Bay of Bengal and the Arabian Sea were not included in the JTWC area of responsibility until the 1975 tropical cyclone season.
- ** The technique for calculating right angle error was revised in 1981; therefore, a direct correlation in right angle statistics cannot be made for the errors computed before 1981 and the errors computed since 1981.

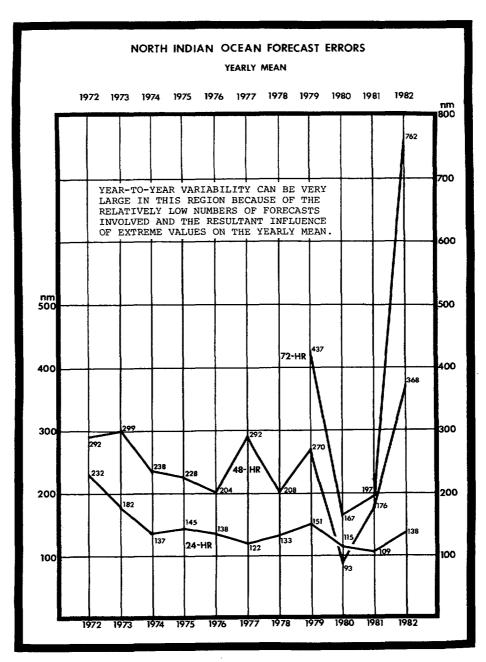


FIGURE 4-4. Annual mean vector errors (nm) for all tropical cyclones in the North Indian Ocean.

2. COMPARISION OF OBJECTIVE TECHNIQUES

a. General

Objective techniques used by JTWC are divided into five main categories:

- (1) climatological and analog techniques;
- (2) extrapolation;
- (3) steering techniques;
- (4) dynamic models;
- (5) empirical and analytical techniques

In September 1981, JTWC began to initialize its array of objective forecast techniques (described below) on the six-hour-old preliminary best track position (an interpolative process) rather than the forecast (partially extrapolated) warning position, e.g. the 0600Z warning is now supported by objective techniques developed from the 0000Z preliminary best track position. This operational change has yielded several advantages:

*techniques can now be requested
much earlier in the warning
development time line, i.e. as
soon as the track can be approximated by one or more fix positions
on, or after the valid time of the
previous warning;
*receipt of these techniques is

*receipt of these techniques is virtually assured prior to development of the next warning *improved (mean) forecast accuracy. er aspect arises because JTWC now

This latter aspect arises because JTWC now has a more reliable approximation of the short-term tropical cyclone movement. Further, since most of the objective techniques are biased for persistence, this new procedure optimizes their performance and provides more consistent guidance on short-term movement, indirectly yielding a more accurate initial position estimate as well as lowering 24-hour forecast errors.

- b. Description of Objective Techniques
- (1) CLIM -- A climatological aid providing 24-, 48- and 72-hour tropical cyclone forecast positions (and intensity changes in the western North Pacific) based upon the position of the tropical cyclone. The output is based upon data records from 1945 to 1981 for the western North Pacific Ocean and 1900 to 1981 for the North Indian Ocean.
- (2) TYAN78 -- An updated analog program which combines the earlier versions TYFN 75 and INJAH 74. The program scans history tapes for tropical cyclones similar (within a specified acceptance envelope) to the current tropical cyclone. For the western North Pacific Ocean, three forecasts of position and intensity are provided for 24-, 48- and 72-hours: RECR a weighted

mean of all accepted tropical cyclones which were categorized as "recurving" during their best track period; STRA - a weighted mean of all accepted tropical cyclones which were categorized as moving "straight" (westward) during their best track period; and TOTL - a weighted mean of all accepted tropical cyclones, including those used in the RECR and STRA forecasts. For the North Indian Ocean, a single (total) forecast track is provided for 12-hour intervals to 72 hours.

- (3) BPAC -- A program which generates 12- to 72-hour forecast positions based on blending the past motion of the tropical cyclone with the CLIM forecast positions. The blending routine gives less weight to persistence at each succeeding forecast interval.
- (4) XTRP -- Forecast positions for 24- and 48-hours are derived from the extension of a straight line which connects the most-recent and 12-hour-old preliminary best track positions.
- (5) HPAC -- 24- and 48-hour forecast positions are derived by merely connecting the mid-points of straight lines which connect these positions on the XTRP and CLIM tracks, respectively.
- (6) CYCLOPS -- An updated version of the HATTRACK/MOHATT steering program which can provide geostrophic steering forecasts at the 1000-, 850-, 700-, 500-, 400-, and 200-mb levels. The program can be run in a modified (includes a 12-hour persistence bias) or unmodified mode applied to either analysis or prognostic fields. The program advects a point vortex on a preselected analysis and/or smoothed prognostic field at designated levels in six-hour time steps through 72 hours. In 1982, only the modified version, in the prognostic mode for the 500-mb level was verified; however, JTWC routinely uses many of the other levels and modes as operational forecast aids.
- Cyclone Model) A coarse-mesh, three-layer in the vertical, primitive equation model with a 205 km grid spacing over a 6400 x 4700 km domain. The model's fields are computed around a bogused, digitized cyclone vortex using FNOC Global Bands prognostic fields for the specified valid time. The past motion of the tropical cyclone is compared to initial steering fields and a bias correction is computed and applied to the model. FNOC hemispheric prognostic fields are used at 12-hour intervals to update the model's boundaries. The resultant forecast positions are derived by locating the 850 mb vortex at six-hour intervals to 72 hours. In 1982, the OTCM was requested for each warning; and when computer resources were available, the OTCM forecast was normally available to the TDO within one hour of the request.

- (8) NTCM -- (Nested Tropical Cyclone Model) A primitive equation model with similar properties as the OTCM. The NTCM differs by containing a finer scale "nested" grid, initializing on Global Bands analysis fields, not containing a (persistence) bias correction, and being a channel model which runs independent of FNOC prognostic fields (not requiring updating of its boundaries). The "nested" grid covers a 1200 x 1200 km area with a 41 km grid spacing which moves within the coarsemesh domain to keep an 850 mb vortex at its center. In 1982, the NTCM was incorporated into the FNOC job-stream and 72-hour forecast tracks were produced automatically from analysis fields, utilizing the 0000Z and 12002 warning positions. These fore-casts were normally received within 12 hours of their valid times and provided guidance for 1200Z and 0000Z warnings, respectively.
- (9) TAPT -- A technique which utilizes upper-tropospheric wind fields to estimate the latitude of initial acceleration associated with the tropical cyclone's interaction with the mid-latitude westerly steering currents. Further, the technique provides speed of movement guidelines for duration and upper-limits, and insight on the probable path of the tropical cyclone, given a prevailing upper-wind pattern during the acceleration process.
- (10) THETA E -- An empirically derived relationship between a tropical cyclone's minimum sea level pressure (MSLP) and (700 mb) equivalent potential temperature ($\theta_{\rm e}$) was developed by Sikora (1976) and Dunnavan (1981). By monitoring MSLP and $\theta_{\rm e}$ trends, the forecaster can evaluate the potential for sudden, rapid deepening of a tropical cyclone.

- (11) WIND RADIUS -- Following an analytic model of the radial profiles of sea level pressures and winds in mature tropical cyclones (Holland, 1980), a set of radii for 30-, 50-, and 100-knot winds based on the tropical cyclone's maximum intensity and radius of maximum winds have been produced to aid the forecaster in determining forecast wind radii.
- (12) DVORAK -- An estimation of a tropical cyclone's current and 24-hour forecast intensity is made from interpretation of visual satellite imagery (Dvorak, 1973) and provided to the forecaster. These intensity estimates are used in conjunction with other intensity-related data and trends to forecast tropical cyclone intensity.

c. Testing and Results

A comparison of selected techniques is included in Table 4-7 for all western North Pacific tropical cyclones and in Table 4-9 for all North Indian Ocean tropical cyclones. In these tables, "X-AXIS" refers to techniques listed vertically. The example in Table 4-7 compares CY50 to OTCM, i.e. in the 435 cases available for a (homogeneous) comparison, the average vector error at 24 hours was 111 nm for CY50 and 119 nm for OTCM. The difference of 8 nm is shown in the lower right. (Differences are not always exact, due to computational round-off which occurs for each of the cases available for comparison).

A comparison of mean and median forecast errors (for a non-homogeneous data set) is provided for selected techniques in Table 4-6 for all western North Pacific tropical cyclones and in Table 4-8 for all North Indian Ocean tropical cyclones.

TABLE 4-6.

COMPARISON OF FORECAST ERRORS (NM) BY TECHNIQUE IN 1982 FOR THE WESTERN NORTH PACIFIC

		24-HOUR	RESUL	TS*		48-HOUR	RESUL	TS*		72-ROUR	RESUL	TS*
TECHNIQUE	MEAN	MEDIAN	STD DEV	(CASES)	MEAN	MEDIAN	STD DEV	(CASES)	MEAN	MEDIAN	STD DEV	(CASES)
JTWC	113	98	73	(665)	237	209	158	(535)	341	296	225	(428)
RECR	116	97	77	(588)	237	203	144	(504)	387	344	243	(423)
STRA	121	101	85	(589)	258	205	185	(513)	434	312	271	(434)
TOTL	112	96	72	(612)	230	197	145	(523)	440	321	246	(440)
CY50	112	100	69	(579)	277	236	184	(496)	408	407	315	(408)
NTCM	143	128	85	(181)	238	208	140	(153)	353	347	180	(124)
OTCM	122	108	73	(479)	232	206	134	(405)	330	289	220	(330)
BPAC	123	104	79	(613)	248	207	169	(527)	442	309	285	(442)
CLIM	150	126	100	(648)	272	226	182	(554)	467	323	295	(467)
XTRP	117	101	89	(635)	264	229	168	(542)				
HPAC	112	98	76	(633)	217	183	143	(540)				

THIS DATA SET REPRESENTS ALL FORECAST ERRORS FOR EACH TECHNIQUE LISTED AGAINST THE CORRESPONDING BEST TRACK POSITIONS AT 24, 48, AND 72 HOURS.

TABLE 4-7. 1982 ERROR STATISTICS FOR SELECTED OBJECTIVE TECHNIQUES IN THE WESTERN NORTH PACIFIC OCEAN

									24-HC	UR FO	RECAST	ERRO	RS (N	I)								
24-	Jī	WC	RE	CR	SI	'RA	TO	TL	CY	50	NT	CM	01	'CM_	BP	AC	CI	.IM	ХТ	RP	HP	AC
JTWC	665 113	113 0																				
RECR	583 115	113 2	588 116	116								NUMB	ED		-AXIS	7						
STRA	584 121	110 11	561 120	114 7	589 121	121 0						OF CASE		TEC	CHNIQUI ERROR							
TOTL	607 112	112 0	583 110	116 -5	583 110	121 -10	612 112	112 0				Y-AX ECHNI			RROR	Œ						
CY50	575 112	112 0	534 110	114 -2	532 107	119 -11	554 110	111 0	579 112	112 0) _	ERRO	R	Υ	7 – X							
NTCM	179 143	102 40	163 141	111 30	159 137	120 17	167 141	108 33	159 142	113 29	$\begin{vmatrix} 181 \\ 143 \end{vmatrix}$	143 0										
OTCM	477 122	113 9	441 123	119 4	436 118	122 -2	455 122	113 9	435 119	8	138 120	137 -15	479 122	122 0								
BPAC	610 122	111	556 121	114 8	559 120	119 1	580 121	110 12	548 119	110 9	170 119	140 -20	458 121	120 1	613 123	123 0						
CLIM	643 150	112 38	585 148	116 32	587 146	121 25	609 150	112 38	574 149	111 38	176 148	142 7	476 150	122 28	611 147	122 24	648 150	150 0				
XTRP	630 117	112 5	575 114	116 -1	575 110	121 -10	599 113	112	566 115	111	171 113	142 -29	469 119	121 -1	600 116	121 -4	633 117	150 -32	635 117	117 0		
HPAC	628 111	111 0	573 109	116 -5	575 107	121 -14	597 110	112 -1	564 110	110 0	171 108	142 -33	468 113	121 -8	600 109	121 -11	633 112	150 -37	633 112	117 -4	633 112	112
										UR FO												
48-		WC	RE	ECR	ST	RA	TO	TL	CY	50	NT	CM	OT	CM	ВР	AC	CL	IM	XT	RP	НР	AC
JTWC	535 237	237	50/	222											JTW	C - OF	FICIA	JTWC	FOREC	CAST		7
RECR	476 233	233	504 237	237		250									STR	A - ST	CURVE	AYT) 1	N 78)			L
STRA	486 258 493	231 26 234	489 256 498	234 22 238	513 258 508	258 0 257	523	230							CY50) - CY 1 - NE	STED 1	MODIF ROPIC	IFD 50	CLONE	MODEL	
CY50	228 466	-5 235	227 458	-10 239	228 468	-28 261	230 475	0 231	496	277					BPAG	C - BL		PERSI	CAL CY STENCE			
NTCM	267 145	32 221	277 139	39 231	272 139	12 258	277 141	46 224	277 139	0 291	153	238							POLATI AND CI			
OTCM	238 384 229	16 237	237 373	6 248	237 380	-20 264	243 384	19 233 0	371 322	-47 270	238 122	238	405 232	232								
BPAC	498 240	-7 232 8	232 479 249	-14 233 17	231 493 247	-32 258 -9	233 499 249	226 23	228 473 251	-41 275 -23	236 146 245	-1 239 6	386 250	229 21	527 248	248 0						
CLIM	521 267	234 32	501 271	237 34	512 270	258 12	520 275	230 45	492 273	275 -1	151 273	238 36	402 277	233 45	526 266	248 18	554 272	272 0				
XTRP	509 262	234 28	491 260	237	501 255	258 -2	510 258	230 28	485 262	275 -12	147 262	237 24	397 266	232	517 264	248 16	540 263	270 -6	542 264	264 0		
НРАС	507	233 -20	489	237 -21	501	258 -45	508	230 -13	483 218	273 -53		237 -16	396 223	232 -8	517	248 -32	540 217	270 -52	540	263 -45	540 217	217 0
		, ., 								UR FO		~										
72-	JΊ	wc	RE	CR	ST	`RA	TO	TL_		50		СМ		:CM	BF	AC	NT	CM	_			
JTWC	428 341	341 0														-						
RECR	378 365	328 37	423 387	.387 0																		
STRA	393 386	333 53	413 385	383 2	434 390	390 0																
TOTL	396 360	336 25	419 364	387 -22	430 368	388 -19	440 373	373 0														
CY50	366 433	345 88	375 465	384 82	387 463	393 70	390 466	377 89	408 463	463 0												
NTCM	113 356	326 30	116 355	387 -30	116 356	418 -61	116 360	378 -17		487 -128	124 353	353 0										
OTCM	299 332	326 7	303 342	390 -47	310 341	391 -49	312 348	364 -16	293 340	440 -99	98 356	338 19	330 346	346 0								
BPAC	402 364	336 28	399 384	379 4	414 384	390 -4	417 389	369 20	388 389	465 -75	119 375	359 17	313 375	341 34	442 388	388 0						
CLIM	420 390	340 50	420 399	387 12	432 406	389 17	437 415	373 42	405 405	464 -58	123 399	355 45	327 410	346 64	442 402	388 14	467 409	409 0	_			

TABLE 4-8.

COMPARISON OF FORECAST ERRORS (NM) BY TECHNIQUE IN 1982 FOR THE NORTH INDIAN OCEAN

		24-HOUR	RESUL	TS*		48-HOUR	RESUL STD	TS*		72-HOUR	RESUL STD	TS*
TECHNIQUE	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)	MEAN	MEDIAN	DEV	(CASES)
JTWC	138	115	93	(37)	368	277	189	(18)	762	887	277	(7)
TOTL	132	120	82	(20)	375	307	181	(7)	883	870	13	(2)
NTCM	319	338	69	(7)	556	578	161	(5)	918	923	80	(3)
CY85	159	142	82	(27)	289	248	136	(13)	426	405	212	(5)
CY50	192	166	129	(27)	433	628	283	(13)	940	1119	420	(5)
OTCM	235	235	66	(13)	522	522	77	(7)	765	798	224	(4)
BPAC	134	133	73	(29)	340	336	127	(12)	853	666	283	(4)
CLIM	218	242	78	(29)	483	523	123	(13)	818	838	51	(4)
XTRP	128	104	75	(28)	326	297	150	(14)				
HPAC	159	167	65	(27)	385	403	112	(13)				

^{*} THIS DATA SET REPRESENTS ALL FORECAST ERRORS FOR EACH TECHNIQUE LISTED AGAINST THE CORRESPONDING BEST TRACK POSITIONS AT 24, 48, AND 72 HOURS.

TABLE 4-9. 1982 ERROR STATISTICS FOR SELECTED OBJECTIVE TECHNIQUES IN THE NORTH INDIAN OCEAN

24-HOUR FORECAST ERRORS (NM)

									24-HU	JR FOR	ECAST	ERROR	5 (NM)							
24-	J _T	WC	TO	OTL	N7	гсм	CY	85	CZ	750	07	CM	BP	AC	CI	LIM	хт	RP	нР	AC
JTWC	37 138	138 0																		
TOTL	20 132	133 0	20 132	132 0							_	NUMB	FR	v	-AXIS	_				
NTCM	7 319	201 118	4 268	166 102	7 319	319 0						OF CASE	.	TEC	HNIQUI RROR	E				
CY85	27 159	153 7	20 164	132 31	6 170	301 -130	27 159	159 0			3	Y-AX TECHNI			RROR	Ε				
CY50	27 192	153 40	20 179	132 47	6 219	301 -81	27 192	159 33	27 192	·192	┸	ERRO	R	Y	- X					
OTCM	13 235	172 63	9 223	128 95	280	329 - 47	13 235	140 95	13 235	208	13 235	235 0								
BPAC	29 134	137 -2	19 129	121 8	5 170	293 - 123	26 134	165 - 30	26 134	186 - 51	13 153	235 -81	29 134	134 0						
CLIM	29 218	137 81	19 198	121 77	5 210	293 -82	26 217	165 53	26 217	186 31	13 235	235 0	29 218	134 84	29 218	218 0				
XTRP	28 128	149 -20	19 126	134 -7	5 195	310 -114	25 130	150 -19	25 130	194 -63	12 135	237 -101	27 120	136 -15	27 120	219 -98	28 128	128 0		
HPAC	27 159	141 18	18 155	122 33	4 185	304 -117	24 165	155 10	24 165	187 -21	12 183	237 -53	27 159	136 23	27 159	219 -59	27 159	120 39	27 159	159 0
	-							-	48-HOL	JR FOR	ECAST	ERROR	S (NM)							
48-	J	TWC	TO	OTL	N7	CM	CY	85	CZ	750	on	CM	BP	AC	CI	LIM	ХТ	RP	HP	AC
JTWC	18 368	368 0																		7
TOTL	7 375	371 4	7 375	375 0									TOTL	- AN	ALOG ((TYAN	FOREC 78) SAL CYC		MODEL	
NTCM	5 556	444 112	2 423	404 18	5 556	556 0							CY85 CY50	- CY	CLOPS CLOPS	MODIF MODIF	TED 85	0 MB 0 MB	PROG PROG	
CY85	13 289	397 -107	7 290	375 -84	4 261	564 -302	13 289	289 0					BPAC	- BL		PERSI	STENCE		CLIM	
CY50	13 433	397 36	7 465	375 90	4 568	564 4	13 433	289 144	13 433	433 0							POLATI AND CL			
OTCM	7 522	473 49	3 557	449 108	2 566	705 -138	7 522	238 284	7 522	528 -5	7 522	522 0								
BPAC	12 340	356 -15	6 354	331 23	2 260	494 - 233	11 326	300 26	11 326	386 -59	6 417	504 -86	12 340	340 0						
CLIM	13 483	370 113	6 432	331 101	3 436	559 - 122	12 480	298 181	12 480	406 73	7 549	522 27	12 475	340 135	13 483	483 0				
XTRP	14 326	392 -64	7 355	375 -19	4 419	564 -144	13 324	289 36	13 324	433 -107	7 386	522 -136	12 295	340 -43	13 307	483 -175	14 326	326 0		
HPAC	13 385	370 15	6 370	331 38	3	559 - 177	12 381	298 82	12 381	406 -25	7 452	522 -70	12 375	340 36	13 385	483 - 97	13 385	307 78	13 385	385 0
									72-HOI	JR FOR	ECAST	ERROR	s (NM)							
72-	<u>J</u> 1	wc	то	OTL	ทา	CM	CY	85		750		:CM		AC	CI	LIM	_			
JTWC	7 762	762 0					-										_			
TOTL	2 883	983 -99	2 883	883 0																
NTCM	3 918	943 -23	1 923	870 53	3 918	918 0														
CY85		801 -374		883 - 549		918 -552	5 426	426 0												
CY50		801 139	2 1218	883 335	3 1105	918 187	5 940	426 515	5 940	940 0										
OTCM	4 765	746 20	1 899	896 3	2 885	916 -30	4 765	467 298		884 -118	4 765	765 0								
BPAC	4 853	746 107	1 935	896 39	2 906	916 -9	4 853	467 386	4 853	884 -30	4 853	765 88	4 853	853 0						
CLIM	4 818	746 72	1 838	896 - 57		916 -122	4 818	467 351	4 818	884 -65	4 818	765 53	4 818	853 -34	4 818	818 0	-			

CHAPTER V - APPLIED TROPICAL CYCLONE RESEARCH SUMMARY

1. JTWC RESEARCH

With the addition of the Southern Hemisphere to the JTWC area of responsibility, JTWC's applied research has been substantially reduced. The goal of JTWC's effort in the research area has been to improve the timeliness and accuracy of operational tropical cyclone warnings. During 1982, JTWC continued to pursue projects of merit as summarized below:

WEIGHTED STEERING PROGRAM

(Allen, R.L: NAVOCEANCOMCEN/JTWC)

A forecast position aid is currently under development which applies an empirically-derived bias to CYCLOPS unmodified steering prognostics. Preliminary results indicate that the 700 mb steering flow (with bias) is the best predictor of meridional motion and a biased average of 850 and 500 mb flow is the best predictor of zonal motion. Initial results from verification studies are promising; further investigation will be conducted during the 1983 tropical cyclone season.

JTWC FORECASTER'S HANDBOOK

(Wells, F.H.; Edson, R.E.; Weir, R.C.: NAVOCEANCOMCEN/JTWC)

An ambitious project to accumulate, in one compendium, the practical information necessary for an operational tropical cyclone forecaster in the western Pacific and Indian Ocean regions.

COMBINED TROPICAL CYCLONE FORECASTING AIDS

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The project objective was to receive all FNOC tropical cyclone forecasting aids as the result of a single request. Several decoder problems were tested and corrected. Additionally, procedures were developed to automate execution of the Nested Tropical Cyclone Model when a tropical cyclone was in warning status.

CLIMATOLOGY (CLIM) FORECAST AID UPDATE

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The CLIM data base was updated through the 1981 tropical cyclone season. In the western North Pacific, five years of new data increased the data base by 16 percent. In the other JTWC regions, the data base was increased by 30 percent with the addition of 10 years of tropical cyclone best track data.

TYAN OBJECTIVE FORECAST AID UPDATE

(Edson, R.E., et al: NAVOCEANCOMCEN/JTWC)

The TYAN data base for the Southern Hemisphere and the North Indian Ocean was updated through the 1981 tropical cyclone season, yielding a 30 percent increase in tropical cyclone positions. Procedures were developed to implement the annual update more efficiently. It was also recommended that the western North Pacific model classification of tropical cyclone tracks (RECR, STRA and TOTL) be modified to increase the model's resolution.

CYCLOPS OBJECTIVE FORECAST AID UPDATE

(Edson, R.E.: NAVOCEANCOMCEN/JTWC)

In light of the recent development of dynamic tropical cyclone models, CYCLOPS could best serve the forecaster as a "plain" steering aid. This would require:

- a) Removal of the, sometime aberrant, persistance correction.
- b) Changing of the long wave filter to more accurately depict wave numbers.
- c) Testing the size/strength of the tropical cyclone for significance.

After testing for effectiveness with the NOGAPS global model, the updated CYCLOPS would be used in conjunction with the dynamic models to indicate expected steering flow at specific levels.

NAVY OPERATIONAL GLOBAL ATMOSPHERIC PREDICTION SYSTEM (NOGAPS) EVALUATION

(Edson, R.E.: NAVOCEANCOMCEN/JTWC)

JTWC participated in evaluating the tropics portion of FNOC Monterey's new global model.

2. NEPRF RESEARCH

TROPICAL CYCLONE STORM SURGE

(Brand, S., NAVENVPREDRSCHFAC; Jarrell, J.D., Compton, J., Science Applications Inc.)

A tropical cyclone storm surge evaluation has been initiated to establish the following: (a) the needs of the Navy in forecasting tropical cyclone storm surge in the western Pacific; (b) the state of the art of storm surge forecasting techniques; and (c) the best approach to solving the Navy's problems associated with tropical cyclone storm surge.

THE NAVY TWO-WAY INTERACTIVE NESTED TROPICAL CYCLONE MODEL (NTCM)

(Fiorino, M., NAVENVPREDRSCHFAC)

Testing of the NTCM concept continued throughout the 1982 season on two versions of the model - the current Cyber 175 version automatically run using the tropical NVA (global bands) analysis, and an improved model coded for the Cyber 205, (NTCM205) the results of which were clearly superior. The NTCM205 performance was markedly reduced when initialized with NOGAPS analyses compared to the NVA analyses. This discrepancy was attributed to a combination of NOGAPS initialization and data assimulation procedures and the high degree of NTCM sensitivity to the large-scale initial wind fields.

Testing will continue on the one-way influence lateral boundary conditions developed at the National Meteorological Center (NMC) which are designed to force outside-the-domain information into forecasts of a limited area model. Experiments will be conducted on expanding the domain of the NTCM Coarse Grid (the large-scale tropical model) to minimize the influence of the channel boundary conditions.

TROPICAL CYCLONE OPTIMUM FORECAST AID

(Tsui, T., NAVENVPREDRSCHFAC)

A comprehensive review of the performance of all JTWC objective tropical cyclone forecast aids has shown that during 19"9-1981 --- if JTWC could have selected the "correct" or the "optimum" forecast aid every time --- the average forecast error could be reduced to 71, 119 159 nm (132, 220, 295 km) for the 24-, 48-, and 72-hour forecasts respectively. The question remains as to which technique is the optimum aid for each situation.

A full-scale test of the optimum-aid concept is now underway. The logical first step of this study is to assess the strength and the characteristics of each objective forecast aid.

TROPICAL CYCLONE OBJECTIVE FORECAST CONFIDENCE AND DISPLAY TECHNIQUE

(Tsui, T., NAVENVPREDRSCHFAC; Nuttal, K., Systems and Applied Sciences Corp.)

In July 1982, forecasters at JTWC could operationally issue a single ARQ command to activate all 11 objective tropical cyclone forecast aids for North Pacific tropical cyclones.

When the system is completed in 1983, a weighted combined tropical cyclone forecast composed from all available objective aids will be issued upon each combined ARQ request. The weights of the combination are deduced from the past (1979-1981) performance of the aids.

SPEED OF RECURVING TYPHOONS

(Sadler, J.C. and B. Cheng-Lan University of Hawaii)

Western North Pacific tropical cyclone data were evaluated to determine the characteristics of recurving typhoons, near and after the time of recurvature, during the 10-year period 1970-1979. Three recurving typhoons which produced large forecast errors after recurvature were selected for case studies in search of aids for anticipating the acceleration in speed of movement after recurvature. Analyses of the upper-troposphere poleward of the typhoons revealed a good relation between the future storm speed and the averaged wind speed between 500 and 200 mb, observed, at and 12 hours prior to recurvature, along the future storm track.

SATELLITE BASED TROPICAL CYCLONE INTENSITY FORGCASTS

(Cook, J. and Tsui, T., NAVENVPREDRSHFAC; F. Nicholson, Systems Control Technology)

Software development is currently underway, for implementation on the NAVENVPREDRSCHFAC Satellite-data Processing and Display System (SPADS), to enable study of cloud structures in the newly developed spherical - spiral coordinate system. A Fourier analysis is performed on the cloud structure in spiral space with various harmonics correlated with atmospheric parameters.

Also under investigation is a method of studying the relationship between cyclone intensity and IR radiances/patterns in Lagrangian coordinates. Satellite images of tropical cyclones are rotated and the image parameters are correlated with the cyclone intensity and rate of intensity change.

TROPICAL CYCLONE INTENSITY FORECAST

(Tsui, T. and Cook, J., NAVENVPREDRSCHFAC; Hamilton, H., System and Applied Sciences Corporation)

A study of the western North Pacific tropical cyclone intensity forecast program (MAXWND) showed that two synoptic parameters—the central equivalent potential temperature and the large-scale vertical wind shears—correlate highly with the intensity change. Efforts have been initiated to quantify the relationships between: (1) the equivalent potential temperature and the central sea surface pressure when below 999 mb; and (2) the NOGAPS large-scale vertical wind shear and the tropical cyclone intensity change.

TROPICAL CYCLONE GUST AND SUSTAINED WIND FORECAST AIDS FOR YOKOSUKA AND CUBI POINT

(Jarrell, J.D. and Englebretson, R.E., Science Applications Inc.)

Forecast aids were developed for predicting wind conditions at Yokosuka and Cubi Point when a tropical cyclone passed within 360 nm (667 km). The forecast aids were produced by analyzing a data set comprising the ratios of station wind values to tropical cyclone center wind values. Ratio values were then assigned to the position of the cyclone center. The 360 nm (667 km) radius circle about the station was divided into 71 equal area segments and the values of the mean and maximum ratio within each segment were subjectively analyzed to produce the forecast aids.

TROPICAL CYCLONE STRIKE AND WIND PROBABILITIES

(Brand, S., NAVENVPREDRSCHFAC; Jarrell, J.D., Science Applications Inc.; Chin, D., Systems and Applied Sciences Corp.)

Tropical cyclone strike and wind probability is a method for determining up through 72 hours that a tropical cyclone will affect geographical points of interest to the user. Applications presently being developed, tested and implemented for the western North Pacific, North Indian Ocean, western North Atlantic, and Gulf of Mexico include: strike/wind probabilities and geographical depictions; optimum track ship routing (OTSR) aids; HP-9845/Tactical Environmental Support System (TESS) software for shipboard environmentalists and decison makers; terrain adjusted probabilities; and—condition setting aids

3. PUBLICATIONS

Diercks, J.W., R.C. Weir and M.K. Kopper, 1982: Forecast Verification and Reconnaissance Data for Southern Hemisphere Tropical Cyclones. NAVOCEANCOLICEN/JTWC TECH NOTE: NOCC/ JTWC 82-1.

The Joint Typhoon Warning Center (JTWC) area of responsibility now includes the Southern Hemisphere, from 180° longitude westward to the east coast of Africa. This technical note documents forecast verification and reconnaissance data for those Southern Hemisphere tropical cyclones that occurred between 1 July 1980 and 30 June 1982.

Weir, R.C., 1982: Predicting the Acceleration of Northward-moving Tropical Cyclones Using Upper-Tropospheric Winds. NAVOCEANCOMCEN/JTWC TECH NOTE: NOCC/JTWC 82-2.

Inconsistent forecasting of the acceleration of northward-moving tropical cyclones entering the domain of the mid-latitude westerlies has been a long-standing weakness in tropical cyclone forecasting. The tracks of tropical cyclones traversing a relative high-density data area of the western North Pacific have been analyzed to verify the acceleration phenomenon, and to correlate the movement with features of the uppertropospheric wind field. The resultant forecast technique is described and the results obtained with its use during the 1982 tropical cyclone season in the western North Pacific are presented.

ANNEX A TROPICAL CYCLONE DATA

1. WESTERN NORTH PACIFIC CYCLONE DATA

TROPICAL STORM MAMIE BEST TRACK DATA

	BEST TRAC	K	WARN!	NG ERROR	5		24 H	OUR FO	ORECAS ERRO			48 H	DUR F	ORECA!			72 HO		ORECA ERROR	
MO/DA/HR	POSIT WIND	POSIT	WIND	DST WI	ΗD	POS	IT	WIND	DST	WIND	P09	IT	MIND	DST	WIND	P09	TIE	WIND	DST	MIND
031406Z	7.1 153.0 15	0.0 0.0	9.	-0.	Ð.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.	9.9	0.0	0.	-0.	0.
0314122	7.4 151.5 20	0.0 0.6	0.	-0.	Ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-0.	0.	0.0	0.8	ø.	-0.	0.
0314182	7.7 150.1 25	0.0 0.0	0.	-8.	ð.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	9.0	ø.	-8.	0.
031500Z	7.8 149.0 25	0.0 0.0	0.	-0.	Ð.	0.0	6.0	Θ.	-8.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-8.	ø.
031506Z	7.7 148.3 30	0.0 0.0	0.	-0.	Ð.	0.0	0.0	ø.	-Ø.	ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	e.
0315122	7.6 147.8 35	0.0 0.6	0.	-0.	a.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-8.	ø.
0315182	7.5 147.2 40	9.0 9.6	0.	-0.	0.	0.0	0.0	0.	-8.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
0316002	7.3 146.4 45	0.0 0.6	ø.	-0.	a.	0.0	0.0	ø.	-0.	0.	9.0	0.0	ø.	-0.	ø.	0.0	8.0	ø.	-0.	ø.
031606Z	7.3 145.5 50	7.0 145.4	50.	19.	а.	5.8	141.8	65.	112.	10.	6.0	137.0	65.	154.	10.	8.0	133.6	65.	327.	5.
0316122	7.3 144.5 50	7.2 144.8	50.	19.	э.	7.2	141.2	65.	80.	10.	8.1	137.5	65.	214.	10.	10.7	134.2	65.	504.	10.
0316182	7.3 143.4 55	7.6 143.3			5.	7.9	139.3	65.	42.	10.		135.6	65.	231.	10.		132.6	65.	585.	20.
0317002	7.4 142.4 55	7.3 142.3	55.	В.	3.	8.2	138.2	60.	74.	5.	9.8	134.5	65.	278.	5.		131.4	65.	552.	25.
031706Z	7.6 141.3 55	7.4 141.2	55.	13.	3.	9.2	136.7	65.	97.	10.	10.3	132.5	70.	289.	10.	11.0	128.7	65.	446.	25.
0317122	7.8 140.0 55	7.9 140.6		6.	3.	9.9	135.6	60.	143.	5.	11.2	131.6	65.	371.	10.	11.6	127.8	60.	463.	25.
031718Z	7.9 138.6 55	8.8 138.3			ā.	11.1	132.8	60.	178.	5.	12.1	128.0	60.	316.	15.		124.0	50.	332.	15.
0318002	7.9 137.0 55	7.9 136.7	50.	18	5.	9.1	131.2	60.	85.	0.	9.6	126.3	55.	220.	15.	9.1	122.2	45.	202.	5.
031806Z	8.1 135.5 55	8.0 135.3			3.	9.4	130.0	60.	134.	ø.	9.6	125.3	50.	229.	10.		121.3	48.	194.	5.
0318122	8.2 133.9 55	8.3 134.6			3.		128.4	60.	154.	5.		124.5		241.	15.		120.4		187.	10.
031818Z	8.2 132.2 55	8.6 132.2			3.	9.5	127.3	50.	195.	5.	9.2	123.4	40.	214.	5.	8.7	119.3	45.	186.	10.
031900Z	8.2 130.1 60	8.1 129.9			5.		122.7	35.	48.	-5.		117.1		117.	-5.		113.1	40.	159.	5.
031906Z	8.2 128.1 60	8.1 127.7			5.		120.5	35.	68.	-5.		116.8		125.	5.		112.7		169.	10.
03 1912Z	8.4 126.0 55	8.2 126.7			ā.		122.B	35.	141.	ø.		117.2	40.	79.	5.		111.6		178.	15.
031918Z	8.4 124.2 45	8.2 124.8			5.		119.7	40.	36.	5.		114.9		115.	10.		110.8		191.	15.
Ø32000Z	8.4 122.8 40	8.5 122.2			3.		115.7	45.	184.	5.		110.1	50.	331.	15.		106.3	35.	394.	5.
032006Z	8.5 121.6 48	8.6 120.6			3.		114.7	45.	201.	10.		110.3	50.	273.	15.		106.7	45.	352.	15.
0320122	8.8 120.5 35	8.5 119.9			5.		115.2		132.	10.		110.4	45.	227.	15.		107.2	25.	282.	-5.
032018Z	9.0 119.8 35	8.5 118.8					114.7	25.	106.	-10.		111.8	25.	107.	-5.		110.2	20.	88.	-10.
032100Z	9.3 118.8 40	9.2 118.6					114.2	30.	90.	-5.		111.4	25.	95.	-5.		109.6	20.	116.	-5.
032106Z	9.5 118.1 35	9.5 118.3					115.2	30.	25.	-5.		112.7	25.	12.	-5.		110.8	20.	73.	-5.
0321122	9.8 117.4 35	10.0 117.0					113.9	25.	35.	-5.		111.4	25.	61.	-5.		109.5	20.	134.	-5.
	10.1 116.5 35	10.2 116.2					112.7	25.	58.	-5.		110.4	25.	96.	-5.	16.1	109.0	20.	238.	ě.
	10.3 115.7 35	10.7 115.2					112.0	25.	80.	-5.		110.2	28.	129.	-5.	8.9	8.0	8.	-0.	ø.
	10.5 114.9 35	10.5 114.6					112.2	25.	30.	-5.	8.0	0.0	а.	-0.	ø.	0.0	0.0	ø.	-0.	0.
	11.0 114.2 30	11.1 113.6					110.2	25.	147.	-5.	0.0	0.0	ø.	-A.	ø.	8.0	0.0	ø.	-ĕ.	ñ.
	11.3 113.6 30	11.3 113.2					110.9	25.	51.	-5.	0.0	0.0	ø.	~0.	ø.	0.0	8.0	a.	-0.	ø.
	11.6 113.0 30	11.7 113.2					111.8	20.	84.	-5.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
	11.8 112.5 30	11.7 112.1					109.3	25.	50.	ø.	0.0	0.0	ø.	-0.	ø.	8.8	0.0	ø.	-0.	ø.
	11.9 111.9 30	11.2 111.5					109.2	20.	54.	-5.	8.0	0.0	ø.	-0.	ø.	8.8	0.0	e.	-0.	a.
	12.1 111.2 30	12.0 111.3					108.8	25.	34.	5.	8.0	0.0	ø.	-0.	ø.	8.8	0.0	0.	-0.	9.
	12.1 110.7 25	12.2 110.8					108.2	15.	30.	5.	8.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	e.
	12.2 110.1 25	12.1 110.0			3.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	0.
	12.2 109.1 25	12.1 109.0			3.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	ø.	8.0	0.0	ø.	-0.	ø.
	12.2 109.1 23	12.1 108.2			3.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
	12.1 107.0 10	0.0 0.8			1.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-a.	В.	0.0	0.0	0.	-0.	0.
5323002	101.00 10	3.0 6.6		٥.	••	5.5	0.0	٥.	٥.		0.0	5.0	٥.	٥.	Ο.	0.0	5.0	٥.	٥.	٥.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	49-HR	72-HR
AVG FORECAST POSIT ERROR	25.	93.	188.	276.	Ø.	ø.	0.	0.
AVG RIGHT ANGLE ERROR	14.	48.	86.	115.	0.	ø.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	2.	5.	9.	11.	0.	ø.	0.	0.
AVG INTENSITY BIAS	-1.	1.	6.	8.	0.	0.	0.	0.
NUMBER OF FORECASTS	35	32	24	23	0	Ø	9	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2733. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TROPICAL STORM MAMIE
FIX POSITIONS FOR CYCLONE NO. 1

FIX NO.	TIME (Z)	PIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	140600 150000	6.9N 154.5E 7.8N 148.7E	PCN 5	T0.5/0.5 T0.5/0.5 /S0.0/18HRS	INIT OBS	PGTW PGTW
3 4 5	150300 151721 160000	8.1N 148.4E B.1N 147.0E 7.0N 146.1E	PCN 5 PCN 5 PCN 5	T1.0/1.0 /D0.5/24HRS	ULCC FIX	PGTW PGTW PGTW

7 8 9 10 11 12 13 14 15 16 17 18 20 21 223 24 25 26 27 28 33 1	160300 160424 160600 160900 161600 161600 162100 170300 1703504 1703504 171200 180000 180300 180300 190300 190300 191600 191600 191600 191600 192100	7.4N 145.9E 7.3N 145.7E 7.3N 145.6E 7.4N 145.1E 7.8N 144.3E 7.7N 143.7E 7.7N 143.7E 7.7N 142.2E 7.4N 140.9E 8.5N 140.7E 8.2N 139.5E 7.8N 136.3E 8.2N 131.8E 8.2N 131.8E 8.2N 131.8E 8.2N 131.8E 8.2N 131.8E 8.2N 128.6E	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	T3.0/3.0 / T3.5/3.5 / T4.0/4.0-/	D0.5/24HRS D0.5/27HRS		ULCC FIX			PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU		
33 4 5 6 6 7 8 9 9 4 1 2 3 4 4 5 6 7 4 4 9 9 5 5 5 5 5 5 5 5 5 5 9 6 6 6 2	220636 220900 221200 221600 221521 222100 230300 230525 230500 231909 231909 231910 240500 240500 241200	8.3M 121.6E 8.4M 121.1E 8.7M 120.6E 9.9M 120.4E 9.4M 119.6E 9.4M 119.6E 9.2M 118.7E 9.2M 118.7E 9.2M 118.6E 9.5M 118.6E 9.5M 116.6E 10.4M 115.6E 10.4M 115.6E 10.2M 115.2E 10.2M 114.6E 10.2M 113.8E 11.2M 114.6E 11.2M 114.6E 11.2M 114.6E 11.2M 113.8E 11.2M 113.8E 11.2M 113.9E 11.2M 113.9E 11.4M 113.7E 11.4M 113.7E	0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	T2.5/3.0+/ T3.8/3.0 / T2.8/2.0 T2.8/2.0 / T2.8/2.0 /	D8.5/24HRS U1.0/24HRS S0.0/24HRS		BASED ON C	CONTINUITY	NOT APPAREN TY CONTINUITY	PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
					AIRC	RAFT FIX	ES					
FIX ND.	TIME (Z)	FIX POSITION	FLT LVL	700MB OBS HGT MSLP					EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP OUT/ IN/ DP.	
1 2 3 4 5 6 7	160359 161921 162131 172217 180633 180847 182215	7.2N 145.8E 7.2N 143.1E 7.2N 142.8E 7.9N 137.2E 8.1N 135.3E 8.2N 134.3E 8.1H 130.4E	1500FT 700MB 700MB 700MB 700MB 700MB 700MB	998 3034 3034 994 3062 994 3086 3086 3087 991	45 300 10 50 340 10 45 350 20 65 330 10	120 4 120 5 050 3 080 5 120 4	5 200 10 15 050 40 5 360 18 6 310 60 3 320 60 8 350 8	10 4 10 5 10 3 3 10 8 2 9 1 7 4	CIRCULAR ELLIPTICAL ELLIPTICAL	15 10 040	+24 +25 +25 +12 +16 +10 +12 +15 +10 +12 +16 + 8 +11 +17 + 7 +12 +14	2 2 4 5
					RADA	R FIXES						
FIX NO.	TIME (Z)	FIX POSITION	RADAR A	EY CCRY SHA		RADOB-C ASWAR T		C	COMMENTS		RADAR POSITION	SITE UMO NO.
1 2 3	191800 192200 200000	8.5N 124.3E 8.5N 123.4E 8.7N 123.3E	LAND			20192 5 25551 5 22531 5	2818				10.3N 124.0E 10.3N 124.0E 10.3N 124.0E	98646 98646 98646

	BEST TRACK	WARN ING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR	POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	PUSIT WIND DST WIND
931896Z	3.8 160.7 25	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	9.9 9.9 99. 9.
0318122	4.5 158.8 25	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.9 0.0 00. 0.
0318182	4.9 157.1 30	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 8.0 00. 0.	0.0 0.0 00. 0.
031900Z	5.5 155.5 40	5.3 155.5 35. 125.	7.6 149.8 50. 42. 0.	8.2 144.8 60. 59. 10.	8.5 139.8 70. 21. 5.
031906Z	5.9 153.9 50	5.9 154.0 50. 6. 0.	8.5 149.0 60. 98. 10.	9.2 143.8 65. 91. 10.	9.0 138.2 75. 38. 15.
031912 Z	6.4 152.4 55	6.3 152.2 55. 13. 0.	8.4 146.6 60. 103. 10.	8.9 141.B 70. 89. 10.	8.6 136.1 75. 12. 15.
031 918Z	6.7 151. 0 5 5	7.0 150.4 55. 40. 0.	8.7 144.8 60. 131. 10.	8.8 140.0 70. 88. 5.	8.5 134.4 75. 38. 15.
032000Z	6.9 149.9 50	7.0 149.5 50. 25. 0.	B.6 143.9 55. 116. 5.	9.2 139.2 60. 575.	8.3 133.6 65. 48. 0.
032006Z	6.9 148.7 50	7.3 148.5 50. 27. 0. 7.0 147.6 50. 0. 0.	8.5 144.2 50. 445. 8.0 143.1 55. 135.	9.2 140.0 55, 1415. 8.7 138.8 50, 160, -10.	9.6 135.0 60. 15610. 8.7 133.7 50. 14120.
032012Z 032018Z	7.0 147.6 50 7.3 146.5 50	7.0 147.6 50. 0. 0. 7.2 146.2 50. 19. 0.	8.3 148.6 55. 4310.	8.8 135.3 50. 3210.	8.5 130.5 45. 6025.
032100Z	7.5 145.5 50	7.6 146.4 50. 54. 0.	8.5 141.2 60. 1025.	8.9 136.1 60. 155. ~5.	8.5 130.2 55. 8320.
032106Z	7.8 144.4 55	7.9 144.3 55. 8. 0.	8.8 139.8 65. 125. 5.	9.0 134.8 60. 14310.	8.7 129.0 60. 6720.
032112Z	7.9 142.9 60	7.9 143.4 55. 305.	9.0 139.0 60. 172. 0.	9.3 134.0 60. 15410.	9.2 128.3 55. 3630.
0321182	8.1 141.3 65	8.0 142.0 60. 425.	9.1 137.0 70. 130. 10.	9.8 131.4 65. 62. ~5.	10.4 126.2 55. 9435.
032200Z	8.3 139.5 65	8.2 139.9 65. 24. 0.	9.2 134.1 75. 36. 10.	10.8 128.6 70. 855.	11.7 123.8 55. 22240.
032206Z	8.5 137.7 60	8.5 138.1 65. 24. 5.	10.0 132.0 75. 54. 5.	11.6 126.0 70, 197, -10.	11.8 122.2 55. 28545.
032212Z	8.8 136.1 60	8.8 136.2 65. 6. 5.	10.8 130.6 75. 102. 5.	11.6 125.8 65. 17820.	11.6 121.8 50. 26755.
03221BZ	9.0 134.8 60	9.1 134.2 65. 36. 5.	10.8 128.7 65. 1275.	11.6 124.2 55. 23035.	11.5 120.0 45. 33155.
032300Z	9.1 133.5 65	9.2 133.5 80. 6. 15.	10.3 129.3 90. 38. 15.	10.9 125.2 65. 12730. 10.8 123.3 50. 20950.	10.9 121.1 50. 22145. 11.2 119.4 50. 27435.
032306Z	9.2 132.4 70	9.3 132.2 80. 13. 10.	10.3 127.3 90. 94. 10. 10.0 125.9 75. 13610.	10.8 123.3 50. 20950. 10.2 121.5 50. 27855.	11.2 117.4 55. 35925.
0323122	9.3 131.4 70 9.5 130.4 70	9.4 131.1 80. 19. 10. 9.5 129.9 75. 30. 5.	10.0 125.1 65. 15425.	10.7 120.8 50. 27850.	11.9 116.8 55. 35920.
032318Z 032400Z	9.5 130.4 70 9.7 129.5 75	9.5 129.5 70. 125.	9.9 126.2 65. 6030.	10.3 123.5 45. 7750.	11.5 119.2 50. 17715.
032406Z 032406Z	9.8 128.8 80	9.6 128.8 75. 125.	9.9 125.8 70. 6430.	10.1 123.0 50. 6435.	11.2 119.2 50. 12910.
0324122	9.8 128.2 85	9.6 128.2 90. 12. 5.	9.6 125.4 85. 7220.	9.7 122.7 60. 9120.	10.5 118.9 65. 122. 10.
0324182	9.9 127.7 90	9.7 127.4 100. 21. 10.	9.7 124.6 75. 6825.	9.9 121.0 60. 11615.	10.9 118.1 65. 106. 20.
032500Z	10.1 127.2 95	9.8 127.0 100. 22. 5.	10.2 124.5 70. 1925.	10.5 122.2 60. 725.	11.9 119.0 65. 42. 25.
032506Z		10.2 126.9 100. 8. 0.	11.0 125.6 90. 99. 5.	11.7 123.2 60. 112. 0.	12.3 121.0 55. 191. 10.
032512Z		10.6 126.2 100. 65.	11.7 123.9 60. 4820.	12.7 121.4 55. 76. 0.	13.0 118.6 55. 84. 5.
0325182		10.7 125.8 95. 255.	11.9 123.4 60. 3815. 11.7 122.0 65. 12. 0.	12.8 120.7 55. 85. 10. 12.6 118.8 65. 21. 25.	12.9 117.4 60. 67. 10. 13.5 115.0 60. 74. 15.
0326002		10.5 124.8 90. 125. 10.7 124.2 85. 17. 0.	11.7 122.0 65. 12. 0. 11.9 121.6 65. 19. 5.	12.6 118.8 65. 21. 25. 12.8 118.0 65. 13. 20.	13.7 114.2 60. 100. 15.
032606Z 032612Z		10.7 124.2 85. 17. 0. 10.8 123.0 65. 3215.	11.8 119.6 60. 47. 5.	12.9 115.6 65. 97. 15.	13.9 111.6 65. 222. 25.
032612Z		11.2 122.2 65. 4510.	11.8 119.2 55. 21. 10.	12.9 115.3 65. 90. 15.	14.0 111.4 60. 204. 20.
032700Z		11.5 121.3 55. 5410.	13.1 117.4 60. 77. 20.	14.0 112.7 70. 198. 25.	14.2 108.0 30. 3795.
0327062		11.5 120.0 60. 78. 0.	12.8 115.9 70. 111. 25.	13.8 112.0 75. 223. 30.	13.8 108.0 30. 361. 0.
032712Z	11.9 120.4 55	11.8 120.2 60. 13. 5.	13.0 117.2 70. 18. 20.	14.2 113.4 75. 116. 35.	14.4 109.2 60. 285. 30.
Ø32718Z	12.8 119.5 45	12.0 119.7 55. 12. 10.	13.2 116.9 65. 35. 15.	14.2 113.0 75. 111. 35.	14.4 108.8 50. 294. 20.
032800Z		12.3 118.6 45. 8. 5.	13.8 115.7 50. 29. 5.	15.2 112.7 50. 130. 15.	17.8 110.8 45. 336. 15.
032806Z		12.9 117.5 45. 18. 8.	15.0 113.7 45. 129. 0.	20.0 110.6 35. 425. 5.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
0328122		13.3 117.2 50. 0. 0.	15.7 113.8 50. 129. 10. 16.2 112.7 55. 183. 15.	19.6 110.2 40. 426. 10. 20.9 109.9 30. 511. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
032818Z 032900Z		14.0 116.4 55. 21. 5. 15.0 115.4 60. 68. 15.	16.2 112.7 55. 183. 15. 18.5 111.2 50. 335. 15.	23.2 110.9 25. 6375.	8.0 8.6 89. 0.
032906Z		14.7 115.7 55. 25. 10.	17.4 114.2 45. 216. 15.	21.4 113.7 35. 510. 5.	8.8 8.8 G0. G.
032912Z		15.1 115.3 50. 54. 10.	17.8 114.1 45. 258. 15.	22.2 113.8 30. 546. 0.	0.0 0.0 00. 0.
032918Z		13.8 114.9 40. 12. 0.	12.2 112.1 30. 111. 0.	11.1 107.5 20. 37210.	0.0 0.0 00. 0.
033000Z		13.7 114.6 35. 13. 0.	12.3 111.7 30. 117. 0.	0.0 0.8 00. 0.	0.0 0.0 00. 0.
033006Z		13.8 114.1 35. 6. 5.	13.6 112.2 30. 113. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0330122		13.7 113.7 30. 21. 0.	13.2 111.8 20. 12910.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
033018Z		13.1 113.7 30. 6. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
033100Z		12.4 113.8 20. 3210.	12.5 110.2 20. 1735.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
033106Z		12.9 113.2 30. 47. 0.	12.9 111,6 20. 605.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
0331122		12.4 113.8 25. 445. 12.4 113.8 20. 4610.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	9.9 9.9 B0. O.
033118Z 040100Z	13.1 113.5 30 13.1 113.1 25	12.4 113.8 20. 4610. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.	9.9 9.9 80. 0.
	13.1 112.6 25	0.0 0.0 00. 0.	8.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS .		ТҮРНО	ONS WHI	LE OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	24.	95.	160.	170.	23.	85.	122.	152.
AVG RIGHT ANGLE ERROR	13.	57.	114.	72.	13.	47.	50.	49.
AVG INTENSITY MAGNITUDE ERROR	5.	11.	17.	21.	5.	12.	19.	22.
AVG INTENSITY BIAS	1.	1.	-4.	-6.	1.	0.	-5.	-9.
NUMBER OF FORECASTS	53	49	44	37	45	41	37	33

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 3863. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

TYPHOON NELSON FIX POSITIONS FOR CYCLONE NO. 2

	TIME	FIX				
NO.	(2)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1 2	180400 180900	3.7N 160.9E 4.0N 160.1E	PCN 6 PCN 5	T1.5/1.5	SBD TINI	PGTW PGTW
3	181888	4.7N 157.7E	PCN 5			PGTW
4 5	190000 190348	5.3N 155.5E 5.8N 154.3E	PCN 3 PCN 4	T2.5/2.5 /D1.0/25HRS		PGTW PGTW
6	190600	5.8N 153.9E	PCN 5			PGT⊎
7	190900	6.0N 152.6E	PCN 5			PGTW
B 9	191633 192100	6.7N 150.7E 6.8N 150.0E	PCN 6 PCN 5			PGTW PGTW
10	200000	7.2N 149.6E	PCN 5	T3.0/3.0 /D0.5/24HRS		PG (W
11 12	200300 200518	7.2N 149.3E 7.5N 149.1E	PCN 5 PCN 5			PGTW PGTW
	201200	7.0N 147.4E	PCN 5.			PGTW
	201621	7.2N 146.1E	PCN 5			PGTW
	201800 202100	7.2N 146.0E 7.2N 145.7E	PCN 5 PCN 5			PGTW PGTW
17	210000	7.3N 145.2E	PCN 5	T3.5/3.5 /D0.5/24HRS		PGT₩
1B 19	210300 210506	7.5N 145.0E 8.2N 144.4E	PCN 5 PCN 5			FGTU PGTW
20	210600	8.5N 144.0E	PCN 5			PGTW
21 22	211200 211600	7.8N 143.0E 8.0N 141.9E	PCN 5 PCN 5			PGTW PGTW
	211751	8.0N 141.7E	PCN 6			PGTW
24	220000 220300	8.3N 139.3E 8.5N 139.0E	PCN 5 PCN 5	T4.0/4.0 /D0.5/24HRS		PGTW PGTW
25 26	220300	8.5N 138.1E	PCN 5			PGTW
27	220600	8.5N 138.0E	PCN 3			PGTW
28 29	221200 221600	8.6N 135.9E 8.3N 134.7E	PCN 5 PCN 5			PGTW PGTW
30	221740	9.0N 134.2E	PCN 5			₽GTW
31 32	230000 230600	8.8N 133.6E 9.3N 132.3E	PCN 5 PCN 5	T4.0/4.0 /S0.0/24HRS		PGTW PGTW
33	231200	9.4N 131.4E	PCN 5			PGTW
34	231728 231728	9.5N 130.1E	PCN 6 PCN 6		BASED ON EXTRAP	PGTW RODN
35 36	232100	9.3N 129.9E 9.6N 129.6E	PCN 5			PGTW
37	240000	9.5N 129.5E		T4.5/4.5-/D0.5/24HRS	FUE DIO FUM	PGTW
	240300 240613	9.6N 129.2E 9.8N 128.7E	PCN 1 PCN 1		EYE DIA 5MM EYE DIA 5MM	PGTW PGTW
49	241200	9.7N 128.2E	PCN I			PGTW
41 42	241600 241800	9.6N 127.8E 9.7N 127.6E	PCN 1 PCN 1			PGTW PGTW
43	242100	9.9N 127.4E	PCN 1			PSTW
44 45	250000 250300	10.0N 127.3E 10.1N 127.1E	PCH 1 PCH 1	T5.0/5.0-/D0.5/24HRS	EYE DIA 10NM	PGTW PGTW
46	250601	10.1N 127.1E	PCN 1			PGTW
47	250900	10.3N 126.7E	PCN 1			PGTW
48 49	251200 251200	11.1N 123.0E 10.3N 126.3E	PCN 5 PCN 1			PGTW PGTW
50	251800	10.4N 125.5E	PCN I			PGTW
51 52	252100 260000	10.4N 125.1E 10.3N 124.5E	PCH 1 PCH 3	T4.5/5.0 /W0.5/24HRS		PGTW PGTW
53	260300	10.4N 124.4E	PCN 1			PGT₩
54 55	260600 260900	10.4N 124.1E 10.7N 123.5E	PCN 5 PCN 5			PGT⊍ PGT⊍
56	261600	11.1N 122.7E	PCN 5			PGTW
57 58	261800 262100	11.1N 122.3E 11.4N 121.7E	PCN 5 PCN 5			PGTW PGTW
* 59	270000	11.3N 121.1E	PCN 5	T3.5/4.0 /W1.0/24HRS		PGTW
* 60	270300	11.0N 120.7E	PCN 5			PGTW PGTW
61 62	270600 270719	11.1N 120.6E 11.1N 120.8E	PCN 5 PCN 5			RPMK
63	270900	11.2N 120.5E	PCN 5			PGTW
	271200 271600	11.7N 120.3E 11.7N 119.5E	PCN 5 PCN 5			PGTW PGTW
66	271822	11.9N 119.3E	PCN 5		BASED ON EXTRAP	PGTW
	272100 280000	12.3N 118.9E 12.5N 118.3E	PCN 5 PCN 5			PGTW PGTW
69	280300	12.8N 117.9E	PCN 5	T2.5/3.0 /W1.0/27HRS		PGT₩
	280600 280706	12.8N 117.3E 13.0N 117.5E	PCN 5	T3.5/3.5	INIT OBS	PGTW RODN
72	200900	13.1N 117.3E	PCN 5	.0.0,010	1111 353	PGT₩
73	281200	13.5N 116.9E	PCN 5			PGTW PCTU
	201600 201800	13.8N 116.4E 14.1N 116.2E	PCN 5 PCN 5			PGTW PGTW
76	282100	14.7N 115.9E	PCN 5		11.00.534	PGT⊎
* 77 78	290000 290300	15.2N 115.8E 15.2N 116.1E	PCN 5 PCN 5	T2.5/2.5 /S0.0/24HRS	ULCC FIX	PGTW PGTW
79	290600	14.6N 116.0E	PCN 5			PGTW
80 81	290655 290900	14.2N 115.5E 14.3N 115.9E	PCN 3 PCN 5	T3.0/3.0	INIT OBS EXP LLCC	RPMK PGTW
82	291200	14.3N 115.4E	PCN 5			PGTW
83	291600	13.9N 115.1E	PCN 3		EXP LLCC	PGT₩

86 87	291940 292100	13.9N 115.0E 13.7N 114.8E	PCN 3 PCN 3			EXP 1.LCC EXP LLCC EXP LLCC		RPMK ROTH PGTW
89 89	300900 300300	14.1N 114.7E	PCN 3	T. 0.0 0 .	10 5 0 HIDD	(./#		PGTW
98	300500	14.0N 114.5E 13.9N 114.2E	PCN 3	T1.0/2.0 /	JØ.5/24HR5			PGTU PGTU
91 92	300643 300900	13.8N 114.0E 13.5N 113.9E	PCN 3 PCN 3	T2.0/3.0 /	J!.∂/24HRS			RPTIK PG NJ
93	301600	13.1N 113.8E	PCN 3			EXP LLCC		PGTW
94 95	301800 302100	13.2N 114.1E 13.1N 114.0E	PCN 3 PCN 3			EXP LLCC		PG FW PG FW
96 97	310000 310300	13.0N 113.6E 13.0N 113.4E	PCN 3 PCN 5					PGTU PGTU
98 99	310630 310631	12.8N 113.9E 12.7N 113.9E	PCN 3 PCN 3	T1.0/1.0 /3				PGTU
100	311600	12.7N 113.9E	PCN 5	11.6/2.6 /6	81.8724nK2	EXP LLCC		R! TIK PGTU
101 102	311800 311916	13.1N 113.7E 13.3N 113.3E	PCN 5					PGTM RODH
103	312100	13.3N 113.5E	PCN 5					PGTW
104 105	010000 010600	13.2N 113.1E 13.0N 112.6E	PCN 3 PCN 3					PGTW PGTW
					AIRCR	AFT FIXES		
FIX	TIME	FIX POSITION	FLT LVL	700MB 08S HGT MSLP	MAX-SEC-UND VEL/BRG/RNG	MAX-FLT-LVL-WND DIR/VEL/BRG/RNG	EYE SHAPE	EYE ORIEN-

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSL.P	MAX-SFE VEL/BRE			-FLT-L' ⁄VEL∕8I			CCRY V/MET	EYE SHAPE	DIANTATION	EYE TEMP (C) OUT/ IN/ 9P/SST	MSN NO.
1 2	190615 191902	5.9N 153.8E 6.8N 150.8E	700MB 700MB	3029 3031	996	50 070	20	210 080	66 11 47 9			3 5	CTROULAR	20	+12 +10 +10 + 9 +14 + 8	1 2
3	192224	6.8N 150.1E 6.8N 148.6E	700MB 700MB	3032 3052	992 994	35 130 40 030		240 060	35 13 46 33	36 1	1	5 4	CIRCULAR	15	+11 +14 + 9	2 3
5	200830 201917	6.9N 148.2E 7.2N 146.3E	700MB 700MB	3073 3084		30 150		250 060		40		1 10	CIRCULAR	5	+12 +15 +12	3
7 8	202145 210803	7.5N 145.9E 7.8N 144.1E	700MB 700MB	3020 3033	994	50 010 50 360	50 6	080 070		20 2	9 16		CIRCULAR	18	+11 +14 +19 +11 +14	4 5
9 10	212113 220631	8.1N 140.5E 8.4N 137.9E	700MB 700MB	2870 2970	973 986	65 360 55 060	30 30	140 080	60 30 45 3	10 3	0 5	2 5 5 4	CIRCULAR CIRCULAR	15 20	+15 +17 +10 +14 +14 + 8	6 7
11	220909 221918	0.7N 137.0E 9.0N 134.2E	700MB 700MB	2960 2979	986	40 180		220 080	51 11 81 0	10 1	0 10		C IRCULAR C IRCULAR	20 15	+11 +14 + 8	7 8
13 14 15	222211 230645 230835	9.0N 134.1E 9.2N 132.2E	700MB 700MB	2988 2964	985 984	80 360 70 360	10 30	160 080	63 3	49 3		' 5	C TRCULAR C TRCULAR	12 10	+11 +20 + 9 +13 +16 +11	8 9
16 17	232210 240635	9.1N 131.8E 9.5N 129.9E 9.8N 128.8E	700118 700MB 700MB	2966 2913 2696	979	80 220	5	200 040 310	55 13 63 36 70 24	00 i	0 5	6	C IRCULAR C IRCULAR	12 15	+18 +12 +12 +13 +14 +12	10
18 19	240830 250742	9.8N 128.5E 10.4N 126.8E	700MB	2630 2510	952 934	100 180	7	180	114 36	60	7 16	2	C IRCULAR C IRCULAR C IRCULAR	15 10 8	+14 +16 +13 +14 +15 +11 +11 +17 +11	11 11 13
28 21	250920 270934	10.3N 126.4E 11.8N 120.9E	700MB 700MB	2548 3052	938	50 100	28	100	113 35	50 1	1 4		CIRCULAR	7	+14 +14 +11 +15 + 6	13 16
22	272002 272259	12.2N 118.8E 12.3N 118.7E	700MB 700MB	3057 3073	998	00 700	20	150	45 02 35 31	20 3	5 3	4	C IRCULAR	15	+10 +14 + 6	17 17
24 25	280705 281003	12.8N 117.6E 13.2N 117.4E	70011B 700MB	3033 3005		50 270 50 360	25 15	210 240	41 15 60 15	50 1	3 5		CIRCULAR CIRCULAR	20 12	+12 +14 +18 +13 +14 +12	18 18

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB- ASWAR		CONMENTS	RADAR POSITION	SITE WMO NG.
1	242300	10.2N 126.8E	LAND				65502			10.3N 124.0E	
2	250200	10.3N 126.7E	LAND				50612			10.3N 124.0E	
3	250300	10.3N 126.7E	LAND				50642			10.3N 124.0E	
4	250600	10.3N 126.5E	LAND				50612	42910		10.3N 124.08	98646
5	251100	10.7N 12G.4E	LAND				10382	52910		10.3N 124.08	98646
6	251500	10.9N 125.8E	LAND				14492	52909		10.3N 124.0E	98646
7	251600	10.9N 125.7E	LAND				10322	52708		10.3N 124.0E	
8	251700	10.8N 125.6E	LAND				14322	52708		10.3N 124.06	
9	251800	10.7N 125.4E	LAND				14211	52608		10.3N 124.0E	
10	252000	10.5N 125.2E	LAND				14141			10.3N 124.09	
1 i	260000	10.3N 124.9E	LAND				5///1			10.3H 124.0E	

TYPHOON ODESSA BEST TRACK DATA

	BEST TR	RACK		WARN		RORS		24 H	OUR F	DRECA ERR			48 H	JUR F	ORECA ERRO			72 H		ORECAS ERRORS	
MO/DA/HR	POSIT WI	IND	POSIT	MIND	DST	WIND	P09	TI	MIND	DST	MIND	POS	TIE	MIND	DST	MIND	POS	IT	WIND	DST	MIND
032806Z	3.5 156.6	20	0.0 0.	0 0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
Ø32812Z	4.3 156.1	25	0.0 0.	0 0.	-8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-A.	9.	0.0	0.0	0.	-0.	8.
0328182	5.1 155.9	30	0.0 0.	0 0.	-0.	0.	0.0	0.0	ø.	-9.	0.	0.0	9.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
032900Z	6.0 155.0	30	0.0 0.	0 0.	-0.	8.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	9.0	ø.	-0.	ø.
032906Z	6.8 155.9	35	6.3 155.	6 35.	35.	0.	7.7	153.6	40.	324.	-10.	8.3	150.5	50.	760.	0.	8.6	147.3	60.	923.	10.
0329122	7,2 156.4	35	7.2 155.	2 35.	71.	0.	9.3	153.7	55.	381.	5.	18.6	150.8	60.	784.	10.	10.3	145.2	60.	962.	5.
032918Z	7.6 157.0	35	7.6 156.	0 40.	59.	5.	9.6	156.0	60.	313.	10.	11.2	154.3	65.	594.	15.	11.2	150.3	65.	696.	10.
033000Z	8.1 158.0	45	7.8 157.	8 40.	22.	-5.	6.5	159.4	60.	216.	10.	6.2	157.2	65.	448.	15.	8.0	154.8	65.	435.	5.
033006Z	8.5 159.0	50	8.4 158.	3 40.	42.	-10.	7.3	160.0	60.	218.	10.	7.4	157.6	65.	357.	15.	9.2	155.0	65.	369.	5.
033012Z	8.7 160.1	50	8.5 160.	1 50.	12.	0.	7.3	160.1	60.	261.	10.	8.8	155.7	65.	416.	10.	10.6	149.8	70.	624.	10.
033018Z	8.7 161.2	50	9.2 161.	2 50.	30.	0.	9.5	166.2	60.	116.	10.	9.2	170.0	65.	475.	10.	7.6	169.2	65.	650.	-5.
033100Z	8.8 162.2	50	9.6 162.	2 55.	48.	5.	10.2	167.0	60.	207.	10.	9.2	170.8	65.	560.	5.	7.2	168.7	65.	645.	-10.
033106 Z	8.9 163.3	50	9.0 163.	2 55.	8.	5.	8.9	165.8	60.	199.	10.	8.8	167.3	65.	417.	5.	8.8	168.3	65.	564.	8.
Ø33112Z	9.3 164.0	50	9.2 164.	2 50.	13.	0.	9.2	168.3	50.	353.	-5.	9.6	172.6	45.	740.	-15.	10.6	176.6	40.	1051.	-15.
033118Z	10.0 164.3	50	9.2 164.	8 50.	56.	0.	9.4	167.9	50.	351.	-5.	9.4	171.2	45.	696.	-25.	9.8	174.3	40.	1018.	-10.
040100Z	10.3 163.5	50	10.3 164.	5 55.	59.	5.	11.4	166.9	55.	319.	-5.	12.1	169.4	35.	572.	-20.	14.3	171.8	5 5.	92 9.	15.
040106Z	10.4 162.8	50	10.8 162.	4 58.	34.	ø.	9.8	162.3	50.	135.	-10.	11.4	164.6	50.	296.	-15.	12.6	168.0	45.	784.	15.
0481122		55	10.6 162.	1 50.	24.	-5.	9.8	161.2	50.	148.	-10.	10.6	163.3	50.	302.	-5.	0.0	0.0	0.	-0.	0.
040118Z	10.7 162.1	55	10.6 161.		19.	-5.		161.2	50.	190.	-20.		163.5	50.	399.	0.	0.0	8.6	0.	-0.	0.
040200Z	11.0 161.5	60	10.8 161.		21.	-5.	11.8	160.8	60.	111.	-15.		162.5	65.	387.	25.	0.0	0.0	0.	-0.	ø.
040206Z		60	11.6 161.		13.	5.		161.4	75.	65.	10.	15.6	165.3	70.	640.	40.	0.0	0.0	Θ.	-0.	0.
0402122	12.1 160.3	60	12.2 160.		8.	5.		161.3	75.	173.	20.	0.0	0.0	0.	~0.	0.	0.0	0.0	0.	-0.	0.
040218Z		70	12.6 159.		13.	-5.		160.1	75.	213.	25.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
040300Z		75	13.3 159.		6.	0.		160.8	75.	328.	35.	0.0	0.0	e.	-8.	0.	0.0	0.0	0.	-0.	0.
040306Z		65	13.3 159.		59.	-5.		157.2	35.	177.	5.	9.9	0.0	0.	-0.	9.	0.0	0.0	0.	-0.	0.
040312Z		55	13.0 158.		13.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
040318Z		50	12.8 157.		21.	-5.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
040400Z		40	13.0 156.		24.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
040406Z	13.1 154.6	30	13.2 154.	6 30.	6.	0.	0.0	9.0	0.	-0.	9.	0.0	8.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPH0	DNS UHII	LE OVER	35 KTS
	LIRNG	24-HR	48-HR	72-HR	wirng	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	29.	228.	520.	742.	30.	231.	513.	739.
AVG RIGHT ANGLE ERROR	16.	113.	226.	385.	17.	115.	221.	392.
AVG INTENSITY MAGNITUDE ERROR	3.	12.	14.	9.	4.	12.	12.	₽.
AVG INTENSITY BIAS	-1.	4.	4.	3.	-1.	4.	2.	2.
NUMBER OF FORECASTS	25	21	17	13	24	20	16	12

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1528. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

TYPHOON UDESSA FIX POSITIONS FOR CYCLONE NO. 3

SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DYORAK CODE	CONENTS	SITE	
1	280300	3.4N 156.8E	PCN 5	T1.0/1.0	INIT OBS ULCC FIX BRKS CONTINUITY BASED OH EXTRAP BASED OH EXTRAP ULAC FIX POSSIBLE EYE	PG Da	
3	290000 290300	6.0N 155.8E 6.2N 155.7E	PCN 5 PCN 5	T2.0/2.0 /D1.0/24HRS	ULCC FIX	<u> </u>	
_	290900 291200 291615	6.7N 155.5E	PCN 5		BRKS CONTINUITY	PG IIJ PG IIJ PG IIJ	
8 9	291800 300000	7.6N 157.5E 7.9N 158.0E	PCN 5 PCN 5	T3.0/3.0-/D1.0/24HRS	BASED ON EXTRAP	PGTU PGTU PGTU	
10 11	300300 300600	8.4N 158.4E 8.4N 158.6E	PCN 5	T3.0/3.0-/D1.0/24HRS		ԲGTN ԲG TW ԲGTW	
13 14	301600 301603	9.0N 160.7E 9.1N 160.5E	PCH 5 PCH 6		ULAC FIX	PGTW KCMC	
15 16 17	301800 302053 302053	9.3N 161.0E 9.1N 161.3E 8.9N 161.3E	PCN 5 PCN 6 PCN 5	T3.5/3.5 /D1.5/21HRS	PRSSTRIF FYF	PGTW KGWC PKWA	
18 19	302100 310000	9.5N 161.7E 9.3N 162.4E	PCN 5 PCN 5	T3.0/3.0 /S0.0/21HRS		PGTW PGTW	
20 21 22	311200 311551	9.1N 162.4E 9.2N 164.3E 10.0N 164.0E	PCN 6 PCN 5 PCN 6	T3.5/3.5 /D1.5/21HRS T3.0/3.0 /S0.0/21HRS		KGWC PGTW KGWC	
24	711000	19 IN 164 CE	DCN 5			PG TW PG TW	
27	итивии	10.5N 164.7F	PCN 5	T4.0/4.0 /D0.5/24HRS		KGWC PKWO PGTW	
28 29 38	010300 010600 010900	10.5N 163.2E 10.7N 162.4E	PCN 5 PCN 5	T4.0/4.0 /D1.0/27HRS		PGTW PG TW PGTW	
31 32	011540 011600	10.9N 162.1E 10.8N 162.1E	PCN 6 PCN 5			PGTW PGTU	
33 34 35	011800 012100 020000	10.7N 161.8E 10.6N 161.8E 11.1N 161.6E	PCN 5 PCN 5 PCN 1		EYE DIA 10NM	PGTW PGTW PGTW	
36 37	020300 020425	11.4N 161.2E 11.6N 161.1E	PCN 1 PCN 3	T4.0/4.0 /S0.0/24HRS	EYE DIA 5NM	PG (N PGTN PG (N	
39 48	020900 021200	12.0H 160.4E 12.2H 160.3E	PCN 5	T4.0/4.0 /D1.0/27HRS T4.0/4.0 /S0.0/24HRS	EYE DIA 18NM EYE DIA 5NM	PGTW PGTW	
41 42 43	021600 021600 022100	12.2N 160.3E 12.4N 159.9E 12.4N 160.1E 12.9N 159.9E	PCN 5 PCN 5 PCN 5	T3.0/4.0-/W1.0/24HRS		PGTW PGTW PGTW	
44 45	030000 030300	13.4N 159.5E 13.7N 159.5E	PCN 5 PCN 5	T3.0/4.0-/W1.0/24HRS	BASED ON EXTRAP	คราบ พราย พราย พราย	
47 48	030600 030900	14.1N 160.1E 14.1N 160.0E	PCN 5 PCN 5			PGTW	
49 50 51	031200 031600 031800	13.2N 158.8E 13.2N 157.4E 13.3N 157.8E	PCN 5 PCN 5 PCN 5	T0 5 0 0 4D 5 0 4UDC	EXP LLCC	PGTW PGTW PGTW	
52 53	040000 040300	13.2N 155.9E 13.2N 155.2E	PCN 3 PCN 3	T0.5/2.0 /W2.5/24HRS	EXP LLCC	PGTW PGTU	
55	040600	13.2N 154.6E	PEN 3		EXP LLCC	PGTW PGTW	
				AIRCR	AFT FIXES		
	TIME (Z)	F1X POSITION	FLT LVL	700MB OBS MAX-SFC-UND HGT MSLP VEL/BRG/RNG	MAX-FLT-LVL-UND ACCRY DIR/VEL/BRG/RNG NAV/MET	EYE EYE ORIEN- SHAPE DIAM/TATION	EYE TEMP (C) MSN OUT/ IN/ DP/SST NO.
1 2	290328 292217	6.2N 155.8E 7.8N 157.6E	1500FT 700MB	994 35 240 15 3030 35 180 10	270 35 210 45 5 I 070 31 350 25 7 5	CIRCULAR 10	+25 +26 +24 28 1 +14 + 9 2
3 4 5	301140 310213 310630	8.6N 160.0E 8.9N 162.5E 8.9N 163.2E	700MB 700MB 700MB	2947 985 2990 989 45 250 18 2999 40 060 10	060 52 340 15 8 2 350 43 280 48 15 3 030 42 320 30 10 5		+16 +16 +10 3 +13 +17 + 9 4 5
7	310844 312017	9.2N 163.5E 10.1N 164.0E	700MB 700MB	3015 989 2973 985 60 090 15	340 51 240 28 10 5 170 47 030 8 5 5	CIRCULAR 8 ELLIPTICAL 25 18 020	+12 +19 + 8 5 +15 +23 +14 6 +12 +19 + 9 7
9 10	010837 012126 020600	10.5N 162.7E 10.8N 161.9E 11.5N 160.8E	700MB 700MB 700MB	2951 986 50 180 11 2897 65 090 6	250 55 180 11 4 4 180 72 090 6 5 5		+13 +14 +12 8
11 12 13	020837 022019 030800	11.8N 160.4E 12.9N 160.8E 13.3N 159.5E	700MB 700MB 700MB	2906 964 80 050 4	239 68 160 15 10 5 180 79 020 12 5 2 110 27 010 60 10 2	CIRCULAR 10 ELLIPTICAL 15 10 090	+15 +19 + 8 9 +13 +21 + 7 10 +18 +19 + 4 11
14 15		13.1N 156.5E 13.0N 156.3E	700MB 700MB	3115 25 040 35	270 23 210 30 10 8 100 23 320 60 10 6		+14 +14 + 5 12 12

TYPHOON PAT BEST TRACK DATA

	BEST TR	ACK		WARN 1				24 H	OUR FO	ORECO!			48 HC	OUR FI				72 HO		DRECAS	
****	20017					RORS				ERRO					ERRO					RRORS	
MO/DA/HR	POSIT WI		POSIT	MIND		MIND	P09		WIND		MIND	POS		MIND	DST	MIND	P09		MIND		WIND
Ø51618Z			a.a a.a	0.	-0.	ø.	0.0	0.0	Ø.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.8	0.0	9.	-0.	0.
051700Z			a.a e.e	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-Ø.	0.	0.0	0.0	0.	-0.	0.
051706Z			1.4 133.2	30.	6.	0.	12.5	129.1	40.	102.	0.	13.0	124.9	50.	144.	-15.	13.4	121.0	50.	375.	-50.
0517122	11.6 131.6	30 13	2.0 132.2	30.	43.	0.	13.2	128.0	45.	71.	5.	13.5	124.2	50.	162.	-20.	13.7	120.5	45.	431.	-60.
0517182	11.3 130.0	35 1	1.9 130.4	35.	43.	0.	12.8	125.9	55.	69.	5.	12.7	122.4	.50.	289.	-35.	12.6	118.8	45.	599.	-60.
951800Z	11.2 128.6	35 16	3.8 128.2	35.	34.	0.	10.9	123.2	25.	266.	-30.	10.5	118.4	30.	557.	-65.	11.0	113.8	45.	941.	-55.
051806Z	11.5 127.7	49 16	3.8 126.8	40.	68.	ø.	10.6	122.1	25.	334.	-40.	10.6	117.4	35.	636.	-65.	10.8	112.8	45.	1060.	-45.
Ø51812Z	12.4 127.1	48 12	2.2 126.4	45.	43.	5.	12.5	121.5	35.	279.	-35.	12.7	117.4	40.	599.	-65.	13.5	113.3	45.	040.	-40.
051816Z	13.8 126.5 !	50 13	3.8 125.8	45.	41.	-5.	15.8	121.7	55.	167.	~30.	16.5	117.7	45.	513.	-60.	16.9	113.7	50.	029.	-25.
051900Z	14.6 125.7	55 15	5.2 125.6	45.	36.	-10.	20.9	125.2	50.	189.	-45.	25.5	130.0	50.	359.	-50.	28.3	137.2	45.	363.	-25.
051906Z	15.4 125.0	65 15	5.6 124.5	55.	31.	-10.	19.3	122.4	65.	132.	-35.	24.5	125.9	65.	243.	-25.	28.2	133.2	45.		-20.
0519122	16.2 124.4	70 16	5.4 124.1	65.	21.	-5,	21.1	124.2	76.	122.	-35.	25.0	129.0	65.	193.	-20.		137.2	55.	171.	ø.
051918Z	17.2 124.2	B5 17	7.3 123.8	65.	24.	-20.	21.8	124.2	70.	157.	-35.	25.5	129.5	60.	209.	-15.		137.9	50.	145.	ø.
052000Z	17.9 124.2	95 17	7.8 124.0	95.	13.	0.	21.5	125.5	108.	115.	ø.	26.2	132.7	65.	163.	-5.	0.0	0.0	ø.	-ø.	ø.
052806Z	18.6 124.6 1	00 18	3.9 124,6	100.	18.	0.	23.0	128.2	90.	127.	Ð.	27.3	138.2	60.	222.	-5.	0.0	0.0	ø.	-0.	Đ.
052012Z	19.3 125.2 1	05 19	3.3 125.1	100.	б.	-5.	23.0	128.2	85.	94.	ø.	27.1	137.2	55.	107.	ē.	0.0	0.0	Ñ.	-ø.	ø.
052018Z	19.8 126.0 10	0 5 20	0.0 125.6	105.	26.	ø.	23.8	129.4	80.	126.	5.	27.8	139.2	50.	95.	ø.	0.0	0.0	ø.	-0.	ø.
052100Z	20.2 127.0 11	99 26	3.3 126.8	100.	13.	0.	24.3	132.9	70.	49.	ø.	9.9	0.0	0.	-0.	ø.	9.6	0.0	ø.	-0.	ø.
052106Z	20.9 127.9 9	90 21	.0 128.0	95.	8.	5.	25.8	134.8	65.	87.	e.	0.8	0.0	ø.	-0.	ø.	0.0	0.0	9.	-0.	ē.
0521122	21.8 129.3	85 21	1.8 129.1	90.	11.	5.	27.8	137.2	60.	148.	5.	0.0	8.0	ø.	-0.	Ø.	0.0	0.0	Ø.	-0.	ø.
052118Z	22.3 131.0 7	75 22	2.8 130.7	75.	34.	0.	29.8	141.2	50.	205.	ø.	0.0	8.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	ø.
052200Z	23.5 133.1	70 23	3.7 133.0	70.	13.	0.	0.0	0.0	0.	-0.	0.	0.0	6.0	0.	-0.	8.	0.0	0.0	ø.	-0.	ē.
052206Z	24.5 135.5 6	55 25	5.2 135.7	65.	43.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	e.	0.0	0.0	в.	-0.	ē.
0522122		55 25	.8 137.7	55.	25.	ø.	0.0	0.0	0.	-8.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ð.	-0.	e.
052218 <i>2</i>	26.5 140.2	50 27	.2 140.7	50.	50.	0.	0.0	0.0	0.	-0.	ø.	0.0	6.0	Ю.	-0.	ø.	0.0	0.0	Ð.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	ONS WHI	LE OVER	35 KTS
	WRNG	24-HR	48~HR	72-HR	LIRNG	24-HF	48-HR	72-HR
AVG FORECAST POSIT ERROR	28.	149.	299.	583.	29.	149.	299.	583.
AVG RIGHT ANGLE ERROR	24.	134.	237.	394.	24.	134.	237.	394.
AVG INTENSITY MAGNITUDE ERROR	3.	16.	30.	35.	3.	16.	30.	35.
AVG INTENSITY BIAS	-2.	-14.	-30.	-35.	-2.	-14.	-30.	-35.
NUMBER OF FORECASTS	23	19	15	11	21	19	15	11

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1994. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

14. KNOTS

TYPHOON PAT FIX POSITIONS FOR CYCLONE NO. 4

FIX	TIME	FIX				
NO.	(Z)	POS1T10N	ACCRY	DVORAK CODE	COMMENTS	SITE
	1.44000	10 50 14 55				
* 1	141800 160547	12.6N 141.2E 9.3N 137.3E	PCH 5	T1 8 41 8	ULAC FIX	PGTW
3	161200		PCN 5	T1.0/1.0	INIT OBS	PGTW
	161600	9.7N 136.4E 9.9N 135.5E			ULCC FIX	PGTW
4 5	161832	10.7N 135.3E	PCN 5		ULCC FIX	PGT₩
6	170300	11.4N 133.8E	PCN 5 PCN 3		ULCC FIX	PGTW PGTW
7	178535	11.6N 133.4E	PCN 5	T1.5/1.5 /D0.5/24HRS		
,	170900	11.8N 132.6E	PCN 5	11.3/1.3 /DB.3/24RKS	ULCC FIX	PGTW PGTW
9	171200	12.0N 132.1E	PCN 5		OLCC FIX	PGTW
10	171600	11.5N 130.3E	PCN 5			PGTW
11	171800	11.5N 129.6E	PCN 5			PGTW
12	172100	11.2N 128.2E	PCN 5			PGTW
13	189900	11.1N 128.4E	PCN 5			PG'TW
14	180523	11.2N 127.6E	PCN 3	T3.0/3.0-/D1.5/24HRS		PGTW
15	180900	11.6N 127.4E	PCN 5	13.0/3.0-/U1.3/24HK3		PGTW
16	181200	12.2N 127.1E	PCN 5			PGTW
17	181600	13.6N 126.5E	PCN 5			PGTW
18	181800	14.1N 126.3E	PCN 5			PGTU
19	181808	13.9N 126.1E	PCN 5			PGTW
20	182100	14.5N 125.6E	PCN 5		ULCC FIX	PGTW
21	190000	14.7N 125.6E	PCH 5		dece i ix	PGTW
22	190300	15.1N 124.6E	PCN 3			PGTW
23	198688	15.4N 124.5E	PCN 3	T3.5/3.5 /D0.5/25HRS		PGTW
24	190900	15.9N 124.8E	PCN 3	1010, 010 - 2010, E0110		PGTW
25	191200	16.2N 124.3E	PCN 5			PGTW
26	191600	16.5N 123.BE	PCN 5			PGTW
27	191756	17.0N 124.1E	PCN 3			PGTW
28	191800	17.0N 123.9E	PCN 3		EYE FORMING	PGTW
29	192100	17.4H 124.0E	PCN 1			PGTW
30	200000	17.7N 124.3E	PCN L		BANDING EYE	PGTW
31	200600	18.5N 124.5E	PCN L	T5.5/5.5 /D2.0/24HRS		PGTW
32	200641	18.4N 124.7E	PCN 1	T5.0/5.0	INIT OBS	RODH
33	200900	19.0N 124.9E	PCN 1			PGTW

35 36 37 38 39 41 42 43 44 45 46 47 48 49 50	201600 201926 201926 202100 210000 210300 210629 210920 211200 211200 211800 212100 220000 220300 220435	19.3N 125.1E 19.6N 125.3E 19.7N 125.7E 19.8N 125.9E 19.9N 126.3E 20.3N 127.0E 20.7N 127.3E 21.0N 128.2E 21.0N 128.3E 21.4N 129.0E 21.9N 129.4E 22.2H 130.6E 22.5N 131.4E 23.3H 132.2E 24.0N 133.1E 24.4N 133.4E 24.4N 133.4E 24.4N 133.59E 24.5N 135.9E	PCN 1 PCN 1 PCN 1 PCN 1 PCN 1 PCN 1 PCN 1 PCN 1 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5 PCN 5	T5.5/	5.5 /9	00.5/21HRS 10.0/24HRS			ULCC ULCC ULCC ULCC	FIX FIX FIX FIX	ONM		PGTU PGTU RFITM PGTU PGTU PGTU RODN PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU			
						A	IRCR	AFT F	IXES							
	TIME (2)	FIX POSITION	FLT LVL	700MB HGT		MAX-SFC- VEL/BRG/							EYE ORIEN- DIAM/TATION	EYE TEMP OUT/ IN/ DP		MSN NO.
2 3 4 5 6 7 8 9 10 11 12 13 14 15	172231 180940 190755 191009 192233 200200 200823 201003 202027 202307 210700 210913 212001 220926	11.3N 133.0E 10.9N 120.0E 12.1N 127.4E 15.3N 124.9E 16.2N 124.1E 18.5N 124.1E 18.5N 124.5E 18.5N 124.0E 18.7N 124.9E 20.1N 126.3E 20.1N 126.3E 20.2N 126.7E 21.1N 120.1E 21.4N 120.5E 23.0N 131.7E 25.8N 137.0E 25.1N 136.8E	760MB 760MB 760MB 760MB 760MB 760MB 760MB 760MB	2993 2854 2842 2664 2623 2594 2600 2631 2634 2625 2656 2769 2928	1004 999 990 970 949 944 943 947 952 968 988	25 330 35 340 40 250 50 210 80 140 65 120 65 120 65 120 65 130 100 270 80 180 80 180 65 220 65 320	30 10 20 45 10 50 45 60 10 30 50 50 51 60 51 51 51 51 51 51 51 51 51 51 51 51 51	030	39 990 37 300 50 150 75 320 80 100 94 100 99 200 90 200 100 260 90 200 103 180 37 170 75 160	20 15 14 62 15 8 30 15 37 9 30 60 30	3 3 5 1	CIRCULAR CIRCULAR CIRCULAR CIRCULAR ELLIPTICAL	15 20 15 28 38 23 Ø58	+12 +12 +11 +11 +13 +13 +15 +14 +13 +13 +19 + 8 +15 +19 + 6 +12 +18 +14 +11 +16 +14 +11 +21 +16 +14 +19 +15 +11 +16 + 9		3 4 5 6 6 7 7 8 8 9 9 10 11 12 12
						R	ADAR	FIXE	S							
	TIME (Z)	FIX POSITION	RADAR A	CCRY	EYE SHAP				R-CODE TDDFF		C	OMMENTS		RADAR POSITION	SITE WMO NO	
2 3 4 5	182000 182100 182200 182300 190100 200200	14.2N 126.0E 14.5N 125.0E 14.6N 125.6E 14.6N 125.4E 15.2N 125.1E 18.4N 123.8E	LAND LAND LAND LAND LAND LAND	2; 2; 2; 2; 30					53214 53316 53114 43218 53210 53603					14.0N 124.3E 14.0N 124.3E 14.0N 124.3E 14.0N 124.3E 14.0N 124.3E 14.0N 124.3E	98447 98447 98447 98447 98447 98447	
						SYN	OPTI	C FIX	ŒS							
	TIME (2)	F1X POSITION	INTENSI ESTIMAT		AREST TA (NM)		c	OMMENTS							

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

* 1 221800 27.0N 142.5E 040 090

	BEST TRAC	K	WAR		2000		24 H0	OUR FO	DRECA			48 HO	OUR F	ORECA:			72 HC		ORECA:	
MOZDAZHR POS					RORS				ERRI					ERRO					ERROR:	5
061806Z 9.3					MIND	POS		MIND	DST	MIND	P09		MIND			POS		MIND		MIND
			0.0 0.	-8.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0618122 9.3			0.0 0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.8	0.	-0.	0.	0.8	0.0	0.	-0.	ø.
061818Z 9.3			0.0 0.	-0.	0.	0.0	0.0	0.	-0.	ø.	8.8	0.0	0.	Θ.	0.	0.0	0.0	0.	-0.	0.
061900Z 9.2			0.0 0.	-e.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-8.	0.	0.0	9.0	0.	-0.	0.
061906Z 9.2			0.0 0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	8.	0.0	8.0	e.	-0.	0.
061912Z 9.1			0.0 0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-9.	8.	0.0	0.0	0.	-0.	ø.
061918Z 9.1			0.0 0.	-8.	0.	0.0	0.0	0.	-0.	в.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.
062090Z 9.0			a.o o.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.
062006Z 9.0			0.0 0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	~მ.	0.	0.0	0.0	0.	-0.	ø.
062012Z 9.0			0.0 0.	-0.	Ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ē.
062018Z 9.2			0.0 0.	-0.	ø.	0.0	0.0	0.	-Ø.	0.	0.0	0.0	ø.	-0.	9.	0.0	0.0	ø.	-0.	8.
062100Z 9.6			9.2 35.	6.	5.	10.3	137.0	50.	312.	15.	11.6	134.2	65.	565.	25.	13.4	130.6	80.	703.	25.
062106Z 9.5			8.9 35.	48.	0.	10.3	137.3	45.	347.	10.	11.3	134.7	60.	567.	15.	12.7	131.9	75.	651.	15.
0621127 9.6		9.5 13	9.9 35.	36.	0.	10.0	139.5	50.	290.	15.	11.0	138.2	60.	427.	15.	11.7	135.8	70.	543.	5.
062118Z 16.2			9.8 40.	94.	5.	11.4	138.2	55.	334.	15.	12.4	136.5	65.	432.	15.	13.4	134.2	75.	549.	10.
062200Z 11.3				8.	10.	14.8	143.3	60.	0.	20.	17.9	142.9	75.	57.	20.		145.7	70.	319.	Й.
062206Z 12.4		11.9 14	2.8 45.	30.	10.	15.5	143.2	60.	13.	15.	19.4	143.5	70.	130.	10.	22.4	147.8	65.	466.	-5.
062212Z 13.3	143.1 35	13.6 14	3.2 45.	19.	10.	17.2	141.7	55.	97.	10.	21.1	140.2	55.	133.	-10.	24.8	143.6	50.	240.	-25.
D62218Z 14.1	143.2 48	14.6 14	3.2 45.	30.	5.	18.2	141.5	55.	99.	5.	21.3	139.6	50.	87.	-15.		141.8	40.	139.	-35.
062300Z 14.8	143.3 48	15.4 14	3.1 50.	38.	10.	18.2	141.1	60.	66.	5.	21.4	139.3	60.	39.	-10.		141.9	50.	183.	-25.
062306Z 15.7	143.3 45	15.4 14	3.2 60.	19.	15.	18.0	143.3	70.	98.	10.	20.9	143.8	75.	266.	5.		146.7	65.	486.	-5.
0623127 16.3	143.1 45	16.4 14	3.5 60.	24.	15.	19.6	143.1	70.	112.	5.	22.8	143.2	75.	226.	0.	26.1	144.6	65.	397.	ø.
062318Z 16.8	142.4 50	17.2 14	2.8 60.	33.	10.	20.4	141.9	70.	74.	5.	23.5	141.8	75.	178.	0.	0.0	0.0	ø.	-0.	ø.
062400Z 17.5	142.0 59	17.6 14	1.8 60.	13.	5.	19.8	139.2	70.	106.	0.	22.4	136.2	70.	348.	-5.	9.0	0.0	В.	-0.	ø.
062406Z 18.2	141.6 69	18.7 14	1.4 55.	32.	-5.	21.5	138.7	50.	77.	-20.	25.0	136.8	45.	334.	-25.	0.0	0.0	ø.	-8.	ø.
062412Z 19.1	141.2 65	19.9 14	0.9 60.	51.	-5.	23.8	138.2	50.	62.	-25.	27.1	138.2	45.	343.	-20.	0.0	0.0	ø.	-8.	ø.
062418Z 20.2	140.6 65	28.2 14	0.7 60.	6.	-5.	23.5	138.3	70.	126.	~5.	0.0	0.0	0.	-0.	0.	0.0	0.0	в.	-0.	ø.
0625002 21.4	140.0 70	21.2 14	0.0 65.	12.	-5.	25.7	137.9	70.	136.	-5.	0.0	9.9	в.	-0.	ø.	0.0	9.0	e.	-0.	ø.
062506Z 22.6	139.4 70	22.2 13	9.2 65.	26.	-5.	27.0	138.2	75.	193.	5.	0.0	9.0	0.	-8.	ø.	0.0	0.0	ø,	-0.	ø.
062512Z 24.0	139.3 75	23.6 13	9.2 70.	25.	-5.	29.2	140.2	70.	185.	5.	0.0	0.0	ø.	-0.	e.	0.0	0.0	ā.	-0.	ø.
0625182 25.4	139.3 75	24.8 13	9.2 75.	36.	0.	0.0	0.0	0.	~8.	0.	0.0	0.0	e.	-0.	ø.	0.0	9.0	ē.	-0.	ø.
062600Z 27.2	139.8 75	27.1 139	9.8 75.	6.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	Ñ.	9.0	0.0	e.	-0.	0.
062606Z 29.5	140.5 70	29.6 14	0.6 70.	8.	0.	0.0	0.8	ø.	-0.	ø.	9.0	0.0	ø.	-0.	ě.	0.0	8.8	ø.	-0.	ø.
0626122 32.1	141.4 65	32.2 14	1.1 65.	16.	ø.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-0.	ě.	8.0	0.0	ø.	-0.	Й.
															٠.		0	٠.	٠.	٠.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	27.	144.	275.	425.	28.	144.	275.	425.			
AVG RIGHT ANGLE ERROR	12.	64.	143.	326.	12.	64.	143.	326.			
AVG INTENSITY MAGNITUDE ERROR	6.	10.	13.	14.	6.	10.	13.	14.			
AVG INTENSITY BIAS	3.	4.	1.	-4.	3.	4.	1.	-4.			
NUMBER OF FORECASTS	23	19	15	11	22	19	15	11			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2173. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON RUBY FIX POSITIONS FOR CYCLONE NO. 5

FIX	TIME	FIX					
NO.	(Z)	POSITION	ACCRY	DVORAK	CODE	COMMENTS	SITE
1	192100	8.9N 141.1E	PCN 5				PGTW
ź	200000	9.2N 140.7E	PCN 5				PGTU
3	200300	9.2N 140.1E	PCN 5	T1.0/1.6	1	INIT OBS	PGTW
4	200600	9.3N 139.5E	PCN 5	11.0, 1.0		INTI ODS	
5	200900	9.4N 139.5E	PCN 5				PGTU
6	201200	9.3N 139.4E	PCN 5				PGTW
7	201600	9.2N 139.0E	PCN 5				PGTW
В	201800	9.2N 138.4E	PCN 5				PGTW
9	202100	9.4N 138.1E	PCN 5				PGTW
10	210000	9.5N 138.8E	PCN 5				PGTU
11	210300	9.2N 139.1E	PCN 5	T1 0/1 0	/S0.0/24HRS		PGTW
12	210600	9.3N 139.5E	PCN 5	11.0/1.0	, , 20.0, 54UK3		PGTW
13	210000	9.2N 140.1E	PCN 5				PGTW
14	211200	9.6N 139.5E	PCN 5				PGTW
* 15	211600	10.5N 140.0E	PCN 5				PGTW
* 16	211800	10.7N 139.9E	PCN 5				PGTW
* 17	212100	10.8N 139.3E	PCN 5				PGTW
18	220000	11.2N 142.4E	PCN 5			BACER ON EVENAR	PGTW
19	220300	11.5N 142.4E	PCN 6	70 5 6 6		BASED ON EXTRAP	PGTW
20	220509	12.0N 142.8E	PCN 5	12.3/2.3	/D1.5/24HRS		PGTW
	220309						PGTW
21		12.6N 142.7E	PCN 6				PGTW
22	221200	13.5N 143.3E	PCN 6				PGTW

23 24	221600 221800	13.8N 143.3E 14.4N 143.2E	PCN 6 PCN 6			PG IW PGTW
25	222100	14.7N 143.2E	PCN 6			PGTW
26	230000	14.8N 143.1E	PCN 4			PGTW
27	230300	15.0N 143.4E	PCN 4	T4.0/4.0 /D1.5/24HRS		PGTW
28	230457	15.4N 143.7E	PCN 4			PG TW
29	239699	15.7N 143.5E	PCN 4			PGT₩
30	230900	16.1N 143.3E	PCH 4			PGTW
31	231200	16.6N 143.2E	PCN 6			PGTW
32	231600	17.0N 142.4E	PEN 6			PGT₩
* 33	231800	17.5N 141.9E	PCN 4			PGTW
34	232100	17.1N 141.8E	PCN 6			PGT₩
35	240000	17.0N 142.3E	PCN 6			PGT₩
36	240300	17.6N 142.2E	PCN 6	T4.0/4.0 /S0.0/24HRS		PGT₩
* 37	248445	19.3N 142.0E	PCN 6		ULCC 17.8N 142.1E	PGTW
* 38	240600	19.4H 141.6E	PCN 6		ULCC 10.0N 141.8E	PGT₩
39	240900	18.4N 141.3E	PCN 6		ULCC FIX	PGT₩
40	241200	18.7N 140.8E	PCN 6		ULCC FIX	PGTW
41	241500	19.5N 140.3E	PCN 6		ULCC FIX	PGT⊍
42	241730	20.2N 140.8E	PCN 6		ULCC FIX	PGTW
43	242032	21.1N 140.7E	PCN 6		NFCC Ł1X	PGTW
44	242100	21.0N 140.4E	PCN 6			PGTW
45	250000	21.6N 140.1E	PCH 4			PGT₩
46	250300	21.9N 139.7E	PCN 4	T4.5/4.5-/D0.5/24HRS		PGTW
47	250600	23.0N 139.9E	PCN 2			PGTW
48	250900	23.2N 139.7E	PCN 2			PGTW
49	251200	24.0N 139.0E	PCH 4			PGTW
50	251600	24.6N 139.6E	PCH 4			PGTW
51	251718	25.3N 139.5E	PCN 4			PGTW
52	251800	25.3N 139.6E	PCN 4			PGTW
53	252100	26.7N 140.0E	PCN 4		ULCC FIX	PGTU
54	260000	27.6N 140.2E	PCN 6			PGTW
55	260300	28.8N 140.7E	PCN 6	T3.5/4.5 /W1.0/24HRS		PGTW
* 56	260421	29.4N 141.1E	PCN 5			PGTW
57	269699	30.1N 141.4E	PCN 6			PGTU
5B	260900	31.4N 142.2E	PCN 6		ULCC FIX	PGTW PGTW
59	261200	32.4N 142.7E	PCN 6		OLLE PIX	PGTW
69	261600	33.3N 143.0E	PCN 6			PGTW
61	270000	36.0N 143.7E	PCN 6			PGTW
62 63	270300 270600	37.0N 143.8E	PCN 6			PGTW
63	21 0000	37.9N 144.7E	PCN 6			raiw

AIRCRAFT FIXES

	TIME	FIX	FLT	700MB			-SFC-								EYE	EYE ORIEN-	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
NO.	(2)	POSITION	LVL	HGT	MSLP	VEL	/BRG/	KNG	DIR/	VEL.	BKG	KNG	NH V	THE I	SHAPE	DININ IN LON	0017 IN7 DF7551	NU.
1	202339	9.6N 139.2E	700MB	3097	995	60	180	15	070	33	040	15	3	2			+12 +13 + 9	1
2	210838	9.3N 139.9E	799MB	3862	995	45	979	18	349	26	260	15	3	10			+11 +16 + 8	2
3	220633	12.5N 142.8E	700MB	3076		48	150	30	220	26	150	30						4
4	220838	13.0N 143.0E	700MB	3979	1003		160	40	230	41	120	120	2	10			+10 +13 + 9	4
5	231959	16.9N 142.0E	700MB	3000					130	42	040	120						5
6	232044	17.0N 142.0E	700MB	2993	989	69	130	95	210	49	130	98	5	10	ELLIPTICAL	30 10 360	+10 +13 +10	5
7	240809	18.5N 141.4E	788MB	2989	989	65	150	70	180	60	969	90	10	10			+12 +13 + 9	6
8	250630	22.9N 139.3E	780MB	2905		45	260	90	330	52	260	98						8
9	250911	22.7N 139.2E	700MB	2841	977	65	240	15	210	95	100	70	5	15			+12 +16	8
10	251914	25.8N 139.4E	700MB	2887					230	78	170	95						8 9
11	252157	26.2N 139.7E	700MB	2912	980	40	0 90	8	290	62	220	60	10	10			+12 +14 +13	9
12	260602	29.6N 140.5E	700MB	2823		55	160	50	210	94	990	68						10
13	260812	30.3N 140.7E	700MB	2825	972	50	270	60	350	56	270	60	5	8			+14 +13	18
14	261929	35.0N 142.2E	700MB	2847					190	72	090	120						11
15	262149	35.5N 142.7E	700MB	2837		65	260	69	090	71	350	78	5	4			+9+9+9	11

TROPICAL STORM TESS BEST TRACK DATA

	BEST T	RACK		WARNI		DRS		24 H	OUR FO	ORECAS ERRO			48 H	OUR F	ORECA!			72 H		ORECAS ERRORS	
MO/DA/HR	POSIT W	IND	POSIT	MIND		MIND	POS		MIND	DST	ผเทบ	POS		WIND			-				
062800Z	17.2 113.7	30	0.0 0.0	0.	-0.	Ø.	8.0	0.0		-0.					DST	MIND	P09		MIND		MIND
062806Z	17.5 113.3	30	0.0 0.0	ø.	-0.				ø.		0.	0.0	0.0	9.	-0.	0.	0.0	0.0	0.	-0.	0.
062B12Z						ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	0.
		30	0.0 0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	Θ.	0.0	0.0	8.	-0.	0.	0.0	0.8	0.	-0.	0.
0628182	1B.2 112.9	30	0.0 0.0	0.	-8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
062900Z	18.5 112.7	30	18:0 113.0	30.	35.	0.	19.0	114.3	40.	113.	18.	19.8	115.2	45.	116.	15.	21.3	115.7	50.	144.	25.
062906Z	18.8 112.4	30	18.9 112.4	30.	6.	0.	20.4	111.4	30.	96.	0.	22.2	111.0	25.	240.	-5.	0.0	9.8	9.	-0.	ø.
0629122	19.2 112.4	30	19.2 112.2	30.	11.	0.	20.8	111.2	30.	135.	-5.	22.3	110.8	20.	295.	-10.	0.0	0.0	ø.	-0.	ø.
Ø62918Z	19.6 112.4	30	19.5 112.0	30.	23.	0.	20.9	111.0	30.	175.	-5.	0.0	0.0	8.	-0.	ø.	9.6	0.0	ด	-0.	a.
063000Z	20.0 112.6	30	20.1 112.3	30.	18.	e.	21.7	112.6	30.	123.	ø.	9.8	0.0	Ř.	-0.	8.	8.9	0.0	Й.	-0.	ø.
863886Z	20.5 113.1	30	20.5 112.8	30.	17.	ø.			30.	91.	ø.	8.8	0.0	e.	-0.	ø.	8.8	0.0	Й.	-0.	0.
	20.9 113.6	35	21.8 113.7	30.	8.	-5.		114.3	20.	108.	-10.	0.0	0.0	ä.		8.	8.8				
	21.2 114.1	35	21.4 114.1	30.	12.	-5.		114.9	20.	123.	-5.			٥.	-0.			0.0	6.	-0.	0.
												0.0	0.0	٥.	-0.	ø.	0.6	0.0	в.	-0.	0.
	21.7 114.8	30	21.6 114.5		18.	5.		116.8	.0	58.	-25.	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.
	21.9 115.3	30	22.2 115.5	35.	21.	5.		118.2	35.	45.	15.	0.0	0.0	ø.	-0.	Ø .	3.6	0.0	0.	-0.	0.
0701122	22.1 116.1	30	22.4 116.2	35.	19.	5.	0.0	0.8	0.	-0.	0.	0.0	0.0	9.	-e.	0.	0.0	0.0	0.	-0.	0.
070118Z	22.3 116.9	25	22.3 116.7	30.	11.	5.	0.0	0.0	0.	-0.	0.	0.0	0.8	0.	-0.	0.	0.0	0.0	в.	-0.	0.
070200Z	22.7 117.8	25	22.8 117.8	25.	6.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-8.	0.	0.0	0.0	ø.	-0.	ø.
070206Z	23.2 118.5	20	23.2 118.5	20.	0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-8.	ø.	0.0	0.0	Ñ.	-ø.	ø.
	,													٠.	٠.	٠.		5.0	σ.	٥.	٠.

	ALL	FORECAS	TS		TYPHO	35 KTS		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	15.	107.	217.	144.	9.	ø.	0.	0.
AVG RIGHT ANGLE ERROR	9.	73.	142.	41.	8.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	2.	е.	10.	25.	0.	0.	0.	0.
AVG INTENSITY BIAS	1.	-3.	0.	25.	0.	0.	0.	6.
NUMBER OF FORECASTS	14	10	3	1	9	8	9	6

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 585. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 6. KNOTS

TROPICAL STORM TESS
FIX POSITIONS FOR CYCLONE NO. 6

FI		IME	FIX						
NO	. (Z)	POSITION	ACCRY	DVORAK	CODE		COMMENTS	SITE
*	i 2	72100	17.6N 111.3E	PCN 6					PGTW
* :	2 2	80300	16.6N 110.7E	PCN 6			ULCC	FIX	PGTW
* :	3 2	80721	18.1N 112.5E	PCN 5	T1.5/1.5	5	INIT	OBS	RPMK
* .	4 2	80721	17.5N 112.0E	PCN 5					RODN
	5 2	80900	17.4N 111.4E	PCN 6			ULCC	FIX	PGT⊎
* (6 2	81200	16.7N 111.3E	PCN 6			ULCC	FIX	PGTW
* 1	7 2	81600	16.5N 109.7E	PEN 6			ULCC	FIX BRKS CONTINUITY	PGTW
* (8 21	81800	16.2N 109.2E	PCN 6			ULCC	FIX	PGTW
* :	9 2	82006	18.0N 114.1E	PCN 6					RPMK
* 10	2 2	82100	16.0N 109.0E	PCN 6			ULCC	FIX	PGTU
* 1	1 2	82223	17.4N 116.9E	PCN 6	T1.8/1.6	3	INIT	OBS	RODN
* 13	2 2	90300	18.5N 113.2E	PCN 6			1515	INIT OBS	PGTW
13	3 2:	90600	18.6N 113.0E	PCN 6					PGTW
1.	4 2:	90708	19.3N 112.2E	PCH 6					RODH
1	5 2:	90709	19.2N 113.3E	PCN 5	T1.5/1.5	5 /S0.0/24HRS			RPMK
1	5 2	90900	19.2N 111.9E	PCN 6			ULCC	FIX	PGTW
* 1	7 2:	91200	18.2N 111.5E	PCN 6					PGTW
* 1	B 2:	91600	18.3N 111.2E	PCN 6					PGTW
* 15	9 2:	91 800	18.8N 110.7E	PCN 6					PGTW
* 2	8 2	91953	19.8N 111.8E	PCN 5					RPMK
2	1 2:	91953	20.2N 112.1E	PCN 6					RODH
* 2	2 2	92100	20.2N 111.3E	PCN 6					PGTW
2	3 3	00000	20.0N 113.5E	PCN 6			ULCC	20.3N 111.5E	PGTW
2	4 3	00300	20.2N 112.9E	PCN 4	T1.5/1.5	5-/S0.0/24HRS			PGT₩
2	5 3	00600	20.4N 113.7E	PCH 4					PGTW

* 26 300656 21.8N 114.1E PCN 3 T1.5/1.5-/50.0/24HRS EXP LLCC 27 300900 21.4N 112.7E PCN 6 ULCC F1X	RPMK PGTIJ
27 300900 21.4N 112.7E PCN 6 ULCC FIX	
* 28 301200 21.4N 112.3E PCN 6 ULCC FIX	PGTIJ
* 29 301600 21.5N 111.7E PCN 6 ULCC FIX	₽GTW
* 30 301800 21.9N 111.5E PCN 6 ULCC FIX	PGT⊎
31 301941 22.5N 113.5E PCN 5	RPMK
* 32 010000 22.5N 113.2E PCN 6 ULCC FIX	PGT⊎
* 33 010300 22.5N 114.1E PCN 6 T2.5/2.5 /D1.0/24HRS	PGTW
34 010600 21.9N 114.8E PCN 6	PGTW
35 010644 22.6N 115.3E PCN 5 T1.5/1.5-/S0.0/24HRS	RPMK
36 010900 22.0N 115.6E PCN 6	₽GTW
37 011200 21.9N 116.1E PCN 6 ULCC FIX	PGT⊎
38 011600 22.0N 116.1E PCN 6	PGT₩
39 011800 22.0N 116.5E PCN 6	PGT₩
40 020000 22.0N 117.5E PCN 6	PGTW

SYNOPTIC FIXES

-	1X 0.	TIME (Z)	F1X POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	COMMENTS
* * *	1 2 3 4 5	281200 292100 300300 300900 301600	19.3N 114.8E 21.2N 113.0E 21.3N 114.0E 21.6N 114.0E 21.5N 113.7E	30 30 30 30 30	210 110 75 50 60	
*	6	302100 010300 010900	21.8N 114.5E 21.5N 115.0E 21.8N 116.3E	35 35 35	48 60 90	

TROPICAL STORM SKIP BEST TRACK DATA

BEST TRACK	: WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST EPRORS
MO/DA/HR PDSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST JIND
062906Z 21.7 131.7 35	0.0 0.0 00. 0.	0.0 0.9 06. 0.	0.8 6.6 9, -6. 0.	0.0 0.0 S0. O.
0629122 22.2 133.5 40	0.0 0.0 00. 0.	0.0 0.0 08. 0.	0.0 0.6 00. 0.	0.0 0.0 90. 0.
062918Z 22.9 135.4 40	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 8.8 90. 0.	0.0 0.0 00. 0.
0 63000Z 24.1 137.2 40	24.2 137.3 45. 8. 5.	27.6 146.2 35. 3915.	0.0 8.0 90. 0.	0.0 0.0 00. 0.
06 3006Z 25.1 138.9 40	25.2 139.1 45. 12. 5.	27.8 147.4 35. 13110.	0.0 8.8 0 0. 0.	0.0 0.0 ก0. 0.
0630122 26.0 141.1 45	26.0 141.0 45. 5. 0.	30.0 149.3 30. 11415.	0.0 0.0 Q0. Q.	0.0 0.0 00. 0.
0630182 26.8 143.7 45	26.8 143.2 48. 275.	8.0 6.0 08. 6.	0.0 8.0 00. 0.	0.0 0.0 00. 0.
0701002 28.2 146.5 50	28.2 146.7 48, 11, -10,	8.0 0.0 0, -0. 0.	0.0 0.0 00. 0.	0.0 0.8 00. 0.
0701062 29.4 149.1 45	29.6 149.3 48. 165,	g.a g.o oa. c.	9.0 0. 0 6 , -0. 0.	0.0 0.0 00. 0.
070112Z 30.8 151.3 45	31.0 151.9 40. 335.	8.0 0.0 06. 0.	0.0 8.8 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHO	TYPHOONS WHILE OVER 35			
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	16.	95.	0.	0.	0.	0.	0.	0.	
AVG RIGHT ANGLE ERROR	15.	32.	0.	0.	0.	0.	0.	0.	
AVG INTENSITY MAGNITUDE ERROR	5.	13.	0.	0.	0.	0.	0.	0.	
AVG INTENSITY BIAS	-2.	-13.	0.	0.	0.	0.	0.	0.	
NUMBER OF FORECASTS	7	3	8	0	0	0	8	9	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1197. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 22. KNOTS

TROPICAL STORM SKIP
FIX:POSITIONS FOR CYCLONE NO. 7

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	290526	22.7N 132.8E	PCN 6	T1.0/1.0	INIT OBS	PGTU
2	290900	21.8N 132.4E	PCN 6		ULCC FIX	PGTW
3	291200	21.8N 132.8E	PCN 6			PGTW
4	291600	22.1N 134.2E	PCN 6			PGTW
5	291811	22.5N 135.8E	PCN 5			PGTW
6	291811	22.8N 135.7E	PCN 5			RPMK
7	292100	23.7N 136.6E	PCN 6			PGTW
8	300000	24.2N 137.0E	PCN 4			PGTW
.9	300300	24.5N 137.4E	PCN 4	T2.5/2.5 /D1.5/22HRS		PGTW
10	300514	24.9N 138.8E	PCN 3			PGTW
11	300600	25.0N 139.1E	PCN 4			PGTW
12	300900	25.7N 140.7E	PCN 6		ULCC FIX	PGTU
13	301200	25.9N 142.1E	PCN 6			PGTW
14	301600	26.3N 144.BE	PCN 6			PGTW
* 15	301000	26.5N 145.0E	PCN 6			PGTW
* 16	302100	27.1N 146.6E	PCN 6			PGTW
17	010000	28.5N 147.4E	PCN 6		BRKS CONTINUITY	PGTW
18	010300	28.9N 147.8E	PCN 6	T3.0/3.0-/D0.5/24HRS		PGT⊎
19	010600	29.4N 148.8E	PCN 6			PGTW
* 20	010900	30.1N 152.0E	PCN 6		BRKS CONTINUITY	PGTW
21	011200	31.0N 152.2E	PCN 6			PGTW
22	011600	31.3N 152.5E	PCN 4		EXP LLCC	PGT₩
23	911860	31.6N 153.6E	PCN 4		EXP LTCC	PGTW
24	012100	32.0N 154.9E	PCH 4		exp llcc	PGTW

AIRCRAFT FIXES

	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT		MAX-SFC-UND VEL/BRG/RNG						EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
2	300933	24.3N 137.6E 25.6N 140.0E 28.1N 144.9E	700MB	3016 3024	991	48 210 70 48 148 38 58 288 98	278	53	150	68				+24 +23 +18 29 +13 +16 + 6	1 2 3
* 4	302156	28.9N 144.7E 30.7N 150.7E	700MB	3058	995	45 150 120 45 190 120	288	46	150	120				+ 9 + 9 + 4 +11 +13 +12	3

SYNOPTIC FIXES

FIX TIME FIX INTENSITY NEAREST ND. (Z) POSITION ESTIMATE DATA (NM) COMMENTS

1 301600 26.5N 142.5E 40 40 UMO 47981

TROPICAL STORM VAL BEST TRACK DATA

BEST TRACK	WARN ING ERRORS	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
MO 400 410 DOCES		ERRORS	ERRORS	ERRORS
MO/DA/HR POSIT WIND	DAIN TSD DAIN TIROP	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
070200Z 24.3 123.3 35	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0702062 24.3 123.9 35	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0702122 24.3 124.3 40	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
070218Z 24.3 125.6 45	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
070300Z 24.8 127.8 55	24.8 127.8 45. 010.	26.9 132.0 55. 363. 20.	0.0 0.0 00. 0.	0.0 9.0 00. 0.
070306Z 26.2 129.9 50	26.2 129.9 50. 0. 0.	9.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
070312Z 27.7 132.3 45	27.5 131.9 50. 24. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	8.0 8.0 99. 9.
070316Z 28.9 135.1 45	28.9 134.5 50. 32. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0.0-005 75.1 190.1 30	30.8 136.9 50. 91. 15.	0.0 0.0 0D. O.	0.0 0.0 00. 0.	0.0 0.0 DO. O.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	29.	363.	ø.	0.	в.	0.	0.	ø.		
AVG RIGHT ANGLE ERROR	22.	33.	ø.	0.	8.	0.	0.	ø.		
AVG INTENSITY MAGNITUDE ERROR	7.	20.	0.	0.	0.	0.	Ø.	ē.		
AVG INTENSITY BIAS	3.	20.	0.	0.	6.	0.	0.	8.		
NUMBER OF FORECASTS	5	1	9	0	8	Ø	ø	8		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 876. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

18. KNOTS

TROPICAL STORM VAL FIX POSITIONS FOR CYCLONE NO. 8

SATELLITE FIXES

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1 * 2 * 3 4 5 6 7 8 9 10 11	828888 828888 828888 921888 921888 938889 938888 938888 938888 9388 9388 9388 93888 93888 93888 9388	24,9N 125,1E 25,4H 125,5E 25,3N 126,1E 23,7N 125,6E 23,7N 125,7E 24,8N 127,8E 26,6N 128,9E 26,2H 129,9E 27,2N 131,0E 27,6N 132,3E 28,0N 134,5E 28,1N 135,4E		T8.5/8.5	INIT OBS ULCC FIX ULCC FIX ULCC FIX BASED ON EXTRAP INIT OBS BASED ON EXTRAP BASED ON EXTRAP BASED ON EXTRAP ULCC FIX	PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW
13 14	040000	29.2N 137.5E 29.4N 138.2E	PCN 6		ULCC 29.6N 139.7E	PGT⊍ PGTW

AIRCRAFT FIXES

	TIME (Z)	FIX POSITION	FLT LVL		08S MSLP	MAX-FLT-LVL-UND DIR/VEL/BRG/RNG	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) DUT/ IN/ DP/SST	MSN NO.
* 1		25.1N 124.2E 24.7N 127.8E		2830		3 0 312 2 0 809 250 56 030 20			24+ 26+ 242 9 +25 +26 29	1 2

SYNOPTIC FIXES

FIX NO.	TIME (2)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)	COMMENTS
1	920000	24.5N 123.4E	35	30	UMO 47912 47918
2	021200	24.3N 124.2E	35	28	UMO 47918
3	021800	24.4N 125.5E	35	20	WMO 47927
4	030900	26.4N 130.2E	35	60	LMO 47945

TROPICAL STORM WINDHA BEST TRACK DATA

	BEST TRACK	WARNI		24 HOUR I		48 HOUR FORECA		72 HOUR FORECAST	
			ERRORS		ERRORS	ERRO		ECRORS	
MO/DA/HR		POSIT WIND	DST WIND	POSIT WINI	DST WIND	POSIT WIND DST	MIND	POSIT WIND PST WIND	
071212Z	11.8 132.6 25	11.8 132.1 30.	29. 5.	13.4 127.1 45	. 119. 15.	14.9 123.2 55. 76.	5.	16.5 119.2 35. 46. 0.	
Ø71218Z	12.2 131.5 25	12.1 130.9 30.	36. 5.	13.7 126.2 45	. 105. 10.	15.2 122.2 55. 70.	5.	16.2 118.2 35. 445.	
071300Z	12.8 130.8 25	12.3 130.5 30.	35. 5.	14.0 125.4 45.	. 70. 5.	15.5 121.6 50. 40.	ø.	17.6 117.9 35. 6415.	
0713062	13.5 130.2 30	13.2 129.6 30.	39. 0.	15.0 125.3 45.	. 385.	15.8 121.3 50. 6.	5.	17.9 117.8 35. 16820.	
0713122	13.8 129.1 30	14.0 129.4 30.	21. 0.	15.0 125.5 45.	615.	15.8 121.6 50. 99.	15.	18.3 118.5 35. 28120.	
0713182	13.8 128.0 35	14.1 127.6 30.	295.	15.4 123.0 50	. 29. 0.	17.6 119.1 35. 58.		20.5 116.3 30. 21915.	
0714002	14.1 126.6 40	13.7 126.8 40.	27. Ø.	15.1 122.1 55.	. 27. 5.	17.8 116.7 30. 109.		21.6 117.2 30. 3395.	
071406Z	14.4 125.5 50	14.4 125.6 45.	65.	15.8 120.8 40	295.	19.0 118.0 35. 171.	-20. 3	23.0 116.8 30. 390. 0.	
071412Z	14.7 124.5 50	14.8 124.5 50.	6. 0.	16.5 120.2 40.	. 13. 5.	19.7 117.8 30, 226.	-25. 2	23.8 117.2 30. 468. 5.	
0 714182	15.1 123.4 50	15.1 123.2 50.	12. 0.	17.0 119.6 40.	. 69. 0.	28.4 117.4 38. 281.	-15.	8.0 6.0 00. 0.	
071500Z	15.5 122.3 50	15.3 122.2 50.	13. 0.	18.1 118.5 30.	9926.	22.5 117.2 30. 350.	-5.	0.0 0.0 00. 0.	
0715062	15.9 121.3 45	15.8 121.2 48.	85.	18.8 118.1 30.	17625.	23.0 117.3 30. 416.	ø.	0.0 0.0 00. 0.	
0715122	16.4 120.0 35	16.1 120.5 35.	34. 0.	17.8 117.8 30.	25725.	21.3 115.9 30. 375.	5.	0.0 0.0 00. 0.	
071518Z	16.9 118.4 49	16.5 119.2 45.	52. 5.	19.0 115.6 50.	. 199. 5.	0.0 0.0 00.	ø.	0.0 8.0 00. 0.	
071600Z	17.8 116.8 50	17.6 117.0 45.	175.	20.2 112.7 60.	92. 25.	0.0 0.0 00.	ø.	8.0 0.0 00. 0.	
071606Z	18.8 115.0 55	18.8 115.2 55.	11. 0.	24.6 109.5 20.	21318.	0.0 6.0 00.	ø.	0.0 0.0 00. 0.	
071612Z	19.8 113.8 55	20.0 113.5 55.	21. 0.	0.0 0.0 0.	0. 0.	0.0 0.0 B0.	ø.	0.0 0.0 00. 0.	
071618Z	20.4 112.4 45	20.7 112.1 45.	25. ส.	0.0 0.0 0.	0. 8.	0.0 0.0 00.	Ø.	0.0 0.0 00. 0:	
071700Z	20.8 111.2 35	20.8 110.8 35.	22. 0.	0.0 0.0 0.	0. 0.	0.0 0.0 00.	0.	0.0 0.0 00. 0.	
971796Z	21.1 110.1 30	20.8 110.2 30.	19. 0.	0.6 0.8 0.	-8. 8.	9.8 6.8 89.	ø.	0.0 0.0 00. 0.	
071712Z	21.3 109.2 25	21.3 109.1 30.	6. 5.	0.0 0.0 0.		8.0 0.0 60.	ø.	0.0 0.0 00. 0.	

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	₩RNG	24-HR	48-HR	72-HR	WPNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	22.	100.	175.	224.	0.	0.	0.	0.		
AVG RIGHT ANGLE ERROR	13.	42.	93.	121.	8.	0.	0.	0.		
AVG INTENSITY MAGNITUDE ERROR	2.	10.	10.	9.	0.	8.	0.	0.		
AVG INTENSITY BIAS	0.	-2.	-4.	-8.	0.	ø.	0.	0.		
NUMBER OF FORECASTS	21	16	13	9 .	. 6	0	6	0		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1486. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

12. KN01

TROPICAL STORM WINDNA FIX POSITIONS FOR CYCLONE NO. 9

SATELLITE FIXES

FIX TIME NO. (Z) FIX POSITION ACCRY DVORAK CODE COMMENTS SITE 092100 7.7N 145.1E PCN 6 INIT OBS MID LVL MID LVL ULCC FIX ULCC FIX INIT OBS 100000 8.0N 143.4E 7.2N 142.8E PCN 6 PCN 6 T1.0/1.0 PGTW PGTW PGTW PGTW PGTW PGTW ULCC FIX 7.1N 142.2E 7.0N 143.2E PCN 5 100456 ULCC FIX 100600 PCN 6 7.9N 139.4E 11.4N 140.0E 11.3N 138.7E 11.2N 130.0E 101600 110000 T1.8/1.8 PGTW PGTW PGTW PGTW PGTW 110300 110600 11.4N 137.9E 11.4N 137.1E ULAC FIX 111600 11.5N 136.7E 11.5N 136.3E 11.5N 136.3E 11.6N 135.7E 11.4N 135.1E 11.7N 134.0E 12.0N 133.4E 12.1N 133.7E 12.0N 132.0E 12.0N 132.0E 11.9N 131.1E 12.0N 130.4E 12.6N 131.1E PGTW PGTW PGTW 112100 PCN 6 6 5 5 6 6 6 6 4 4 5 5 6 6 6 5 5 6 7 7 PCN 6 6 6 6 5 6 7 4 PCN 6 6 6 6 5 6 7 PCN 6 PCN BASED ON EXTRAP T2.0/2.0 /D1.0/24HRS 120000 120300 120613 BRKS CONTINUITY PGTW RPMK 120614 120900 T2.0/2.0 INIT OBS PGTW PGTW 121200 121800 PGTW PGTW 122100 130000 130300 130601 PGTW PGTW PGTW RPMK T2.5/2.5 /D0.5/24HRS 12.6N 131.7E 13.2N 131.1E 14.0N 130.4E 13.9N 129.8E 13.3N 127.7E 13.6N 126.9E 13.2N 126.9E 12.9N 127.4E 12.8N 127.0E 130601 131200 T2.5/2.5 /D0.5/24HRS PGTW PGTW BRKS CONTINUITY 131600 131600 131600 131646 132100 BRKS CONTINUITY PGTW PGTW PGTW PGTW 13.8N 127.1E 14.6N 126.1E 14.9N 125.4E 14.9N 125.5E 14.8N 124.4E 14.9N 123.8E T3.0/3.0-/D0.5/24HRS 140000 PGTW PGTW 140300 148549 148549 RPMK PGTW T3.0/3.0-/D0.5/24HRS BASED ON EXTRAP 141200 BASED ON EXTRAP 141600

38	141800	15.1N 123.2E	PCN 6		BASED ON EXTRAP	PGTW
39	141834	15.2N 123.1E	PCN 5		BASED ON EXTRAP	PGT⊎
48	141834	14.8N 123.1E	PCN 5		BASED ON EXTRAP	RPMK
41	142100	15.1N 122.8E	PCN 6		BASED ON EXTRAP	PGTW
42	150000	15.3N 123.2E	PCN 6	T4.0/4.0-/D1.0/24HRS	-	PGTW
43	150300	15.1N 122.4E	PCN 6			PGT₩
44	150537	15.3N 121.8E	PCN 5	T4.0/4.0-/D1.0/24HRS		RPMK
45	150600	15.5N 121.8E	PCN 6		ULCC FIX	PGTW
46	150719	15.2N 121.6E	PCN 5			RPMK
47	150900	15.4N 121.2E	PCN 6		ULCC FIX	PGTW
48	151200	16.1N 120.4E	PCN 6		3233 / 1	PGTW
49	151600	16.5N 119.4E	PCN 6		BASED ON EXTRAP	PGTW
50	151800	16.5N 11B.7E	PCN 6			PGTW
51	151822	16.6N 118.4E	PCN 5			PGTW
52	151822	17.1N 118.1E	PCN 5			RPMK
53	152004	16.7N 117.6E	PCN 5			RPNK
54	152100	17.0N 117.4E	PCN 6		BASED ON EXTRAP	PGTW
55	160000	18.0N 116.7E	PCN 4	T2.5/3.0 /U1.5/24HRS	with the second	PGTW
56	160300	18.8N 115.8E	PCN 4		EXP LLCC	PGTW
57	160600	19.1N 115.0E	PCN 4		EXP LLCC	PGTW
5B	160707	18.9N 114.6E	PCN 3	T2.5/3.0-/D1.5/25HRS	E/W ELGG	RPMK
59	160707	18.8N 114.2E	PCN 3	T3.0/3.0 /S0.0/26HRS		RODH
60	160900	19.4N 114.0E	PCN 6	1010101010101010101		PGTW
61	161200	20.0N 114.1E	PCN 6			PGTW
62	161600	20.1N 112.4E	PCN 6			PGTW
63	161952	20.4N 111.6E	PCN 6			RODN
64	162100	20.4N 111.1E	PCN 6			PGTW
65	170000	20.3N 111.8E	PCN 4	T1.0/1.5 /W1.5/24HRS	EXP LLCC	PGTW
66	170300	20.3N 110.9E	PCN 6	1110-110-1010-1	2200	PGTW
67	170600	20.8N 110.5E	PCH 4		EXP LLCC	PGTU
6B	170655	21.1N 109.9E	PCN 3	T1.5/2.0-/W1.0/24HRS	EXP LLCC	RPMK
69	170900	21.3N 109.8E	PCN 6	71157 216 7 WITG 2-41KS	LA LLOO	PGTW
70	171200	21.9N 109.4E	PCN 6			PGTW
71	171600	21.3N 107.9E	PCN 6			PGTW
72	171948	21.1N 108.8E	PCN 5			RPMK
		E 100.0L				Nr 1 IIV

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC-LIN VEL/BRG/RN			FLT-L VEL/8					EYE SHAPE	EYE ORIEN- DIAM'TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1	120508	11.5N 133.7E	700MB	3110	1000		94	40	30 3	30	60	5	48			+10 + 9 + 9	3
2	130036	12.6N 130.7E	700MB	3071	1001	25 100 6	0 16	60	27 1	20	40	10	10			+10 +10	4
3	130702	13.8N 130.2E	700MB	3071	1000	25 240 11	0 07	70	38 2	70	120						5
4	130850	13.4N 129.9E	1500F1		1000	25 260 9	0 32	20	29 2	60	90	10	30			+24 +23 +21 29	5
5	132106	13.8N 127.4E	1500FT		994	25 120 2	0 12	20	49 0	130	69	6	4			- ·	6
6	132233	13.8N 127.1E	1500FT		991	35 020 9	0 34	40	50 2	70	120	3	4			+24 +26 29	ě.
7	140654	14.6N 125.3E	700MB	2986		65 280 3	0 09	99	68 3	38	30	5	10				7
8	140815	14.5N 125.0E	700MB	2978	986	70 230 1	5 82	20	53 2	69	58	8	8			+12 +17 +10	7
9	152249	17.6N 116.9E	700MB	2988	988	48 898 6	0 16	80	48 1	00	90	4	2			+12 +14 +10	ė
10	160110	18.1N 116.6E	700MB	2991		50 180	6 15	50	52 1	80	6	4	2			· · · •	9
11	160639	18.8N 114.8E	700MB	2972	985	55 140 3	5 28	00	31 1	30	65	10	10			+13 +15 +12	19

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	DIAM	RADOB-CODE ASWAR TODEF	COMPENTS	RADAR POSITION	SITE UMO NO.
1 2 3 4 5 6 7 8 9 10 11	142300 142340 150100 150230 150600 150730 150800 150830 150900 150910 150935 151035	15. IN 122.6E 15. IN 122.9E 15. IN 122.8E 15. IN 122.8E 15.6N 121.5E 15.5N 121.5E 15.5N 121.2E 15.5N 121.8E 15.5N 120.9E 15.7N 120.8E 15.7N 120.8E	LAND LAND LAND LAND	GOOD FAIR FAIR POOR	CIRCULAR ELL IPTICAL ELL IPTICAL CIRCULAR	10 10 10	1888/ 42984 119/3 42786 188// 43812 188// 42812 188// 42712 188// 42722	20 DEG SPRL OVRLY STNRY EYE 100 PCT CI DIA 50 KMS EYE 100 PCT CI DIA 50 KMS EYE 100 PCT CI DIA 50 KMS EYE 100 PCT CI DPEN N DIA 35 KMS EYE 70 PCT CI DPEN S DIA 35 KMS EYE 100 PCT CI DIA 20 KMS EYE 60 PCT CI DIA 25 KMS EYE 60 PCT CI DIA 25 KMS	16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 16.3N 128.6E 15.2N 128.6E 15.2N 128.6E 15.2N 128.6E 15.2N 128.6E 15.2N 128.6E	98321 98321 98321 98321 98321 98321 98327 98327 98327 98327 98327
13 14	151200 152300	16.1N 120.2E 17.8N 116.3E					118// 43210 10/// 7///	EYE 100 PCT EL AXIS 35/15 KMS	16.3N 120.6E 16.3N 120.6E	98321 98321

TYPHOON ANDY BEST TRACK DATA

	BEST TRACK	WARNING ERRORS	24 HOUR FORE	CAST RRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
M0/0A/HF	DOCTT TIME					
072112Z	POSIT WIND	POSIT WIND DST WIN		IST WIND ∙0. 0. (
0721122	11.1 147.0 25	0.0 0.0 00. 0 0.0 0.0 00. 0			0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
072200Z					0.0 0.0 0c. c. 0.0 0.0 0c. c.	8.8 0.8 88. 8.
072206Z	11.4 145.6 35 11.7 144.9 35				4.6 139.6 65. 183. 0.	15.7 135.7 75. 24715.
						14.9 133.4 75, 352, -15.
072212Z 072218Z	12.2 144.9 40 11.8 145.1 40	12.5 144.3 50. 40. 10 12.8 143.8 50. 97. 10			4.7 137.5 65. 256. 0. 4.8 136.4 65. 2855.	14.9 132.3 75. 32115.
0723002	11.8 145.1 46	12.8 143.8 50. 97. 18			4.8 135.4 65. 2855. 4.8 139.3 60. 14228.	14.9 135.1 75. 20415.
072306Z	12.1 144.1 55	12.0 144.0 50. 85			4.2 138.1 65. 20225.	15.0 133.3 75. 20420.
072312Z					3.0 139.6 65. 30625.	13.3 135.4 75. 36325.
072318Z	12.8 143.4 60	11.8 143.3 55. 605				
072400Z	13.2 143.1 65	13.1 142.9 65. 13. 0			5.7 136.5 85. 1815. 5.8 135.7 85. 20810.	16.2 132.3 90. 25310. 16.3 131.6 90. 28510.
0724062	13.7 142.6 65	13.7 142.5 65. 6. 0			6.5 134.7 85. 19215.	
0724122	14.4 141.9 65	14.2 141.9 65. 12. 0				
0724182	15.2 141.3 70	15.0 141.0 70. 21. 0			6.9 132.8 90. 17815.	17.5 128.2 95. 22925.
072500Z	16.0 140.6 80	15.9 140.7 80. 8. 0			8.8 132.9 95. 2065.	20.1 128.3 109. 21220.
072506Z	17.2 139.7 90	16.4 148.4 85. 635			9.3 133.3 110. 295. 10.	19.8 129.1 105. 32215.
0725122	18.0 13B.6 90	18.2 139.3 90. 42. 0			2.2 129.3 110. 1805.	24.3 123.8 115. 164. 0.
072518Z	10.2 136.7 90	18.8 137.7 90. 67. 0			2.7 128.2 110. 19210.	24.5 123.6 115. 164. 10.
072600Z	10.3 134.9 90	18.2 135.2 90. 18. 0			0.0 124.4 105. 4915.	22.9 120.0 90. 395.
972696Z	18.4 133.3 95	18.8 133.1 95. 27. 0			1.8 123.2 110. 3710.	24.5 119.8 70. 7315.
0726122	18.4 132.0 100	18.8 131.3 100. 46. 0			1.2 121.1 110. 915.	23.2 117.3 80. 127. 10.
072618 Z	18.8 130.4 105	18.8 130.7 105. 17. 0			1.6 120.3 95. 91 10.	23.8 116.4 58. 1425.
0727 0 02	19.3 129.3 100	19.2 128.8 100. 29. 0			3.6 119.3 85. 8510.	0.0 8.0 00. 0.
0727062	19.7 128.1 100	19.6 128.2 100. 8. 0			3.6 119.4 85. 30. 0.	0.0 0.0 00. 0.
0727122	20.2 126.9 115	20.3 126.9 115. 6. 0			4.9 118.2 50. 6220.	0.0 0.0 00. 0.
0727182	20.5 125.7 120	20.8 125.8 120. 19. 0			4.9 117.0 35. 8320.	0.0 0.0 00. 0.
072809Z	20.8 124.6 120	21.0 124.5 120. 13. 0			0.6 0.6 00. 0.	0.0 0.0 00. 0.
072806Z	21.3 123.6 120	21.4 123.4 120. 13. 0			9.9	3.0 0.0 00. 0.
Ø72812Z	21.8 122.6 115	21.8 122.6 115. 0. 0	23.5 119.5 70. 5	i6. Ø. (8.0 6.8 GG. A.	0.0 0.0 00. 0.
072818Z	22.4 121.7 105	22.2 121.9 105. 16. 0	24.0 119.1 70. 7	9. 15. (0.8 0.9 00. 0 .	6.0 6.0 OO. O.
072900Z	23.0 120.7 95	23.0 121.0 95. 17. 0	25.7 118.0 30. 5	0. - 5. 6	0.0 0.0 00. 0.	0. 0
072906Z	23.8 119.9 85	23.8 120.0 85. 5. 0	0.0 0.0 0	0. 0. 9	9.8 0.8 00. 0.	0.0 0.0 00. 0.
0729122	24.4 119.2 70	24.4 119.2 70. 0. 0	0.0 0.0 0	0. 0. 6	0.0 0.0 00. 0.	8.0 0.0 00. 0.
072918Z	25.2 118.5 55	25.2 118.6 55. 5. 0	0.0 0.0 0	0. 0. 6	0.0 0.0 00. 0.	0.0 0.0 00. O.
0730002	26.4 117.5 35	26.8 117.1 35. 32. 0	8.0 8.8 8	0. 0. 6	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	URNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	24.	99.	168.	231.	24.	99.	168.	231.		
AVG RIGHT ANGLE ERROR	14.	50.	106.	144.	14.	50.	106.	144.		
AVG INTENSITY MAGNITUDE ERROR	1.	6.	12.	15.	1.	6.	12.	15.		
AVG INTENSITY BIAS	0.	-5.	-11.	-13.	Θ.	-5.	-11.	-13.		
NUMBER OF FORECASTS	32	28	23	19	32	28	23	19		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2072. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

10. KNOTS

TYPHOON ANDY FIX POSITIONS FOR CYCLONE NO. 10

FIX	TIME	FIX POSITION				
NO.	(2)	POSITION	ACCRY	DVORAK CODE	ULCC FIX ULAC FIX INIT OBS ULCC FIX	SITE
1	211600	12.2N 144.7E	PCN 6		HICC EIV	PGTU
3	212100	10.8N 145.7E	PCN 6		ULAC FIX	PGTW
* 4 5	220000 220413	12.6N 145.9E	PCN 6	T2.5/2.5	INIT OBS	PGTW PGTW
* 6	220600	12.7N 144.3E	PCN 6		III CC CTM	PGTW
Ť b	221200	12.1N 144.3E	PCN 6		ULCC FIX	PGTW
* 9 * 19	221600 221658	11.8N 143.9E	PCN 6		ULCC FIX	PGTW PGTM
* 11	221800	11.5N 142.9E	PCN 6		ULCC FIX	PGTW
* 12	230000	11.1N 142.9E 11.9N 144.6E	PCN 6		ULLL FIX	PGTW
14 15	230300	11.6N 145.0E	PCN 6	T3.5/3.5 /01.0/25HRS		PGTU PGTU
16	230543	12.1N 144.8E	PCN 5	T4.0/4.0	INIT OBS	RPMK
18	230900 231200	12.8N 144.0E 12.8N 143.5E	PCN 6		ULCC FIX	PGTW
19 28	231600	11.7N 143.4E	PCN 6		ULCC FIX	PGTW PGTU
21	231800	11.7N 143.7E	PCN 5		ULCC FIX	PGTW
23	240000	12.9N 143.BE	PCN 6		ULAC FIX	PGTW
24 25	240300 240530	13.5N 142.8E	PCN 6	T4.0/4.0 /D0.5/24HRS	ULCC FIX	PGTW PGTU
26	240600	13.BN 142.1E	PCN 6			PGTW
28	241288	14.1N 141.8E	PCN 6		ULCC FIX	PGTW
29 30	241600 241800	14.6N 140.9E 14.7N 140.2E	PCN 6		ULCC FIX	PGTW PGTW
31	242100	15.2N 140.2E	PCN 6		ULCC FIX	PGTW
33	250300	16.3N 148.3E	PCN 6		ULCC FIX	PGTW
34 35	250518 250600	17.1N 139.9E 17.2N 139.BE	PCN 5 PCN 6	T4.5/4.5 /DØ.5/24HRS	ULCC FIX ULCC FIX	PGTW PGTW
36	250900	17.8N 139.3E	PCN 6		ULCC FIX	PGTW
38	251200	18.1N 137.1E	PCN 6		ULCC FIX	PGTW
39 40	251000 252100	18.3N 136.4E 18.4N 135.6E	PCN 6 PCN 6			PGT⊍ PGT⊍
41	260000	18.5N 135.0E	PCN 6		ULCC FIX	PGTW
43	260506	18.6N 133.3E	PCN 5	T5.0/5.0-/D0.5/24HRS	ULCC FIX	PGTU
44 45	260506 260600	18.5N 132.9E 18.5N 133.2E	PCN 5	T5.5/5.5	INIT OBS	RPMK PGTW
46	260900	18.6N 132.2E	PCN 6		ULCC FIX	PGTU
48	261600	19.0N 131.0E	PCN 2			PGTW
49 50	261888 262188	18.9N 130.1E 19.3N 128.9E	PCN 2 PCN 6			PGTW PGTW
51	270000	19.4N 129.3E	PCN 6			PGTW
53	270600	19.6N 128.0E	PCN 2	T6.0/6.0-/D1.0/25HRS T6.0/6.0 /D0.5/25HRS		PGTW
54 55	270636 270900	19.6N 127.8E 20.0N 127.7E	PCN I PCN 2	T6.0/6.0 /D0.5/25HRS	EYE DIA 18NM	RPMK PGTW
56 52	271600	20.4N 125.9E	PCN 2			PGTW PGTW
58	271921	20.1N 125.4E	PCN 5			RPMK PGTW
			10110			PGTW
	280300 280624	21.4N 123.6E 21.5N 123.6E	PCN 6	T6.0/6.0-/S0.0/24HRS		PGTW PGTW
63		21.5N 123.8E	PCN 3 PCN 6	T6.0/6.0-/S0.0/24HRS		RPMK PGTW
64 65	281200	21.5N 122.5E 21.7N 122.8E	PCN 6			PGTW
66 67	281600 281800	22.4N 122.1E 22.6N 121.8E	PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
68 69	281989 282188	22.6N 121.5E 22.8N 121.3E	PCN 3 PCN 6		ULCC FIX	RPMK PGTW
70	290000	22.6N 120.9E	PCN 6		UL.CC FIX	PGTW
71 72	290300 290611	23.4N 120.1E 23.5N 119.4E	PCN 6 PCN 5	T4.5/4.5-/J1.5/25HRS	ULCC FIX	PGTW PGTW
73 74	290612 290900	23.9N 119.5E 23.6N 119.4E	PCN 5 PCN 6	T4.5/4.5 /W1.5/24HRS		RPMK PGTW
75	291200	24.5N 119.1E	PCN 6			PGTW
76 77	291600 291800	24.9N 118.6E 25.3N 118.4E	PCN 6 PCN 6			PGTW PGTW
78 79	291857 292100	25.7N 118.4E 25.9N 117.7E	PCN 5 PCN 6			PGTW PGTW
88	300000	26.0N 117.4E	PCN 4			PGTW
81 82	300300 300600	25.2N 117.0E 26.3N 116.8E	PCN 6			PGTW PGTW

					AIRC	RAFT FIXES					
FIX NO.	TIME (Z)	FIX POSITION	FLT LVL		ix-sfc-und L/BRG/RNG			EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP OUT/ IN/ DP	
1 2 3 4 5 6 7 8 9 10 11 12 13 14 15 16	220538 221901 222150 230700 230943 232002 232218 240835 240835 242256 252138 260023 261216 270011	11.5N 145.2E 11.7N 144.9E 11.8N 145.0E 11.9N 144.7E 12.0N 143.9E 12.5N 143.2E 13.1N 143.2E 13.6N 142.6E 13.9N 142.4E 15.0N 142.6E 13.9N 142.4E 16.4N 134.0E 18.4N 134.0E 19.3N 129.3E	709M8 700M8 700M8 700M8 700M8 700M8 700M8 700M8 700M8 700M8 700M8 700M8	3846 S S S S S S S S S S S S S S S S S S S	60 050 30 60 150 15 60 360 15 55 120 20 75 150 60 80 050 50 80 050 50	968 40 298 25 109 48 358 38 230 33 320 21 359 33 220 120 220 45 159 110 239 62 120 40 110 64 344 60 120 58 95e 42 220 56 128 50 192 80 668 40 160 81 996 115 860 77 838 112 169 118 899 48 108 96 358 68	5 6 6 5 4 6 8 5 5 3 3 5 5 2 3 8 3 1 1 2 3 3 1 2 3 1 1	C IRCULAR	15 10 040 10 7 7	+15 + 7 +15 +16 + 8 +15 +17 +11 +12 +14 +11 +14 +18 +12 +16 + 8 +12 +16 +10 +15 +11 +12 +14 +12 +15 +11 +11 +16 +12 +15 +16 +14 +19 +15	8 9
					RADAR	R FIXES	,				
FIX NO.	TIME (Z)	FIX POSITION	RADAR AC	EYE CRY SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	t	COMPENTS		RADAR POSITION	SITE WMO NO.
16 17 19 20 21 22 23 24 25 26 27 29 30 31 32 33 34 35 36 37	280408 280408 280508 280508 280508 280508 280508 280508 280508 280508 281008 281308 281308 281308 281408 281408 281408 281408 281508 281608 281708 281708 281708 281808	11.9H 143.2E 13.5H 142.7E 13.6H 142.7E 13.6H 142.6E 13.8H 142.6E 21.2H 124.2E 21.3H 124.2E 21.3H 123.6E 21.2H 123.7E 21.4H 123.5E 21.7H 123.7E 21.7H 123.3E 21.9H 122.3E 21.9H 122.5E 21.1H 121.1E 22.2H 122.6E 21.9H 122.6E 21.9H 122.6E 21.9H 122.6E 21.9H 122.6E 22.1H 122.1E 22.2H 122.6E 22.1H 122.1E 22.2H 122.6E 22.3H 121.9E 22.3H 121.9E 22.3H 121.9E 22.3H 121.9E 22.3H 121.6E 22.5H 121.8E 22.5H 121.8E 22.5H 121.8E 22.5H 121.8E 22.7H 121.4E		OOR AIR AIR AIR AIR		6///5 73112	EN NW E ELLIPTI	ICAL OPEN N		13.6N 144.9E 13.6N 144.9E 13.6N 144.9E 13.6N 144.9E 13.6N 144.9E 13.6N 144.9E 14.3N 124.2E 15.1N 121.6E 14.3N 124.2E 16.3N 124.2E	
FIX	TIME	FIX		Y NEAREST	SYNOPTI	IC FIXES					
	(Z) 282288	P051T10N		DATA (NM)	UMO 467	COMMENTS					

FIX NO.	TIME (Z)	F1X POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)			CONTENTS
1	282200	22.8N 121.2E	095	010	UMO	46760	
2	290100	23.7N 120.6E	085	030	UMD	46751	
3	290600	23.8N 119.8E	085	010			
4	290900	24.2N 119.5E	070	025			
5	291500	24.8N 119.0E	865	030			
6	291800	25.8N 118.5E	939	030			
7	292100	26.3N 117.3E	030	030			

SUPER TYPHOON BESS BEST TRACK DATA

	BEST TRACK	WARN ING	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
MO 476 416		ERRORS	ERRORS	ERRORS	ERRORS
MO/DA/HR		WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
0722002	11.1 163.8 25 0.0 0.		8.9 0.0 00. 0.	0.8 0.0 00. 6.	0.0 0.0 00. 0.
072206Z		0 00. 0.	0.0 0.0 00. 0.	0.8 0.0 00. 0.	0.0 0.0 00. 8.
0 72212Z	12.2 162.3 25 0.0 0.	0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
072218Z	12.8 161.6 30 12.7 160.	1 30. 88. 0.	14.2 156.6 40. 93. 0.	15.3 152.5 50. 16215.	16.0 148.2 60. 23325.
072300Z	13.2 160.8 30 12.8 160.	8 30. 24. 0.	14.8 157.1 45. 54. 0.	16.2 153.2 60. 6710.	17.2 150.2 70. 12020.
072306Z	13.8 159.9 30 13.6 159.	8 30. 13. 0.	15.3 156.2 50. 36. 8.	16.8 152.4 65. 5310.	18.0 148.4 89. 23615.
072312Z	14.4 159.0 35 14.4 158.	7 30. 175.	16.3 154.6 50. 58. ~10.	18.0 150.3 65. 15515.	18.8 145.8 80. 37215.
0723182	15.1 157.9 40 14.9 157.	8 35. 135.	16.8 153.8 50. 6315.	18.2 149.3 65. 19220.	18.9 144.9 80. 41415.
072400Z	15.7 157.0 45 15.8 157.	1 45, 8, 9,	18.3 153.2 55. 9915.	20.0 148.2 65. 31525.	20.2 143.3 70. 53925.
072406Z	15.9 156.3 50 16.5 156.	0 50. 40. 0.	19.0 151.5 60. 15815.	20.3 146.2 65. 41830.	20.0 140.4 65. 64030.
0724122	16.3 155.6 60 16.6 155.		18.4 152.6 70. 9610.	20.2 147.6 75. 35220.	20.2 142.8 75. 51120.
0724182	16.7 154.9 65 16.8 154.		18.0 151.6 75. 9110.	19.5 146.4 75. 36120.	19.3 141.8 80. 51615.
072500Z	16.9 154.1 70 16.9 154.		18.3 150.5 80. 15310.	19.2 145.4 90. 4865.	19.1 141.0 95. 510. 0.
072506Z	17.0 153.3 75 17.1 153.		18.1 149.5 85. 19110.	19.0 144.6 95. 409. 0.	
072512Z	16.8 152.7 80 16.9 152.		18.2 149.9 90. 1815.	20.1 147.8 95. 314. 6.	
072518Z	16.6 152.2 85 16.9 152.		18.5 150.3 90. 1785.		21.1 144.9 95. 17410.
072600Z	16.2 152.0 90 16.4 151.		16.0 149.5 95. 107. 0.		21.0 145.3 95. 7325.
072606Z	15.8 151.8 95 16.2 151.		16.0 149.3 100. 86. 5.	16.0 146.4 100. 190. 5. 16.0 146.2 105. 195. 5.	16.1 143.0 110. 28525.
072612Z	15.5 151.3 95 15.8 151.				16.2 143.8 110. 30630.
072618Z	15.7 151.3 95 15.8 151.		15.8 149.5 105. 47. 10.	15.8 146.2 115. 190. 10.	16.1 142.8 125. 36615.
872700Z			15.8 149.5 105. 29. 18.	15.8 146.2 115. 2435.	16.1 142.8 125. 405. ~10.
072706Z			15.5 149.5 105. 78. 10.	15.4 146.6 115. 33220.	15.7 143.2 125. 4865.
	15.3 150.6 95 15.5 150.		15.4 147.3 105. 186. 5.	15.6 144.1 115. 34325.	15.B 140.3 125. 490. 5.
0727122	15.4 150.2 95 15.3 150.		15.4 147.3 105. 211. 0.	15.6 144.1 115. 40425.	15.8 140.3 125. 539. 10.
072718Z	15.7 150.0 95 15.9 150.		15.2 149.4 105. 35515.	15.3 147.4 115. 56320.	15.7 144.2 125. 665. 15.
072800Z	16.8 149.6 95 16.2 150.		15.7 148.1 110. 35525.	15.7 146.1 115. 56515.	16.0 142.8 125. 643. 20.
072006Z	18.2 148.7 100 17.8 148.		19.8 143.8 115. 9025.	21.2 138.8 120. 164. 0.	21.5 133.6 125. 364. 25.
0728122	18.9 146.9 105 19.2 147.		21.4 141.2 105. 9635.	21.6 136.0 115. 249. 0.	27.3 131.2 125. 331. 30.
072818Z	19.8 145.5 120 19.7 145.		21.0 139.2 130. 1555.	22.4 134.1 130. 276. 20.	25.2 130.7 120. 377. 30.
072900Z	20.6 144.6 135 20.3 144.		22.4 139.9 155. 56. 25.	23.8 134.1 130. 236. 25.	25.5 128.9 115. 480. 30.
072906Z	21.3 143.7 140 21.2 143.		24.2 139.9 145. 42. 25.	26.2 136.2 120. 86. 20.	27.6 133.3 105. 265. 25.
072912Z	22.2 142.7 140 22.3 142.		25.0 138.8 140. 21. 25.	26.6 135.4 120. 111. 25.	28.3 132.4 100. 364. 30.
0729 I 8Z	22.7 141.3 135 22.8 141.		25.1 137.7 135. 23. 25.	26.7 134.4 115. 158. 25.	28.7 131.9 100. 526. 50.
073000Z	23.3 140.2 130 23.3 140.	2 130. 0. 0.	26.0 137.2 110. 42. 5.	28.9 135.5 100. 76. 15.	34.3 135.8 80. 265. 30.
073006Z	23.9 139.2 120 24.0 139.	4 125. 13. 5.	26.7 136.7 110. 66. 10.	30.0 135.0 95. 107. 15.	35.8 138.0 70. 278. 30.
073012Z	24.7 139.0 115 24.8 138.	9 120. 8. 5.	27.3 136.2 105. 65. 10.	31.3 134.9 90. 144. 20.	0.6 0.6 00. 0.
073018Z	25.2 138.1 110 25.2 137.	9 110. 11. 0.	28.1 135.9 100. 66. 10.	32.5 135.1 85. 249. 35.	0.0 0.0 00. 0.
073100Z	25.7 137.9 105 25.5 137.	B 105. 13. 0.	27.4 136.2 105. 114. 20.	30.8 135.0 90, 478, 40,	8.0 0.0 00. 0.
0731062	26.2 137.8 100 26.1 137.	4 105. 22. 5.	28.3 136.2 100, 149, 20,	31.8 134.9 85. 493. 45.	9.6 9.9 90. 9.
073112Z	27.1 137.4 95 27.1 137.		30.7 135.5 90. 153. 20.	0.0 0.0 00. 0.	8.0 0.0 00. 0.
073 118Z	27.8 137.1 90 27.8 137.	1 95. 0. 5.	31.5 135.3 85. 302. 35.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
080100Z	29.2 136.9 85 29.0 136.		35.8 137.5 65. 185. 15.	0.0 0.0 00. 0.	6.6 6.6 60. 6.
080106Z	30.7 136.9 80 31.0 136.		39.8 139.8 60. 198. 20.	0.0 0.0 00. 0.	8.8 6.6 60. 6.
0801122	32.9 137.0 70 32.8 136.		8.0 0.0 00. 0.	0.0 0.0 00. 0.	6.6 6.6 60. 6.
000110Z	36.3 137.1 50 36.1 137.		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
080200Z	38.7 136.2 50 38.8 136.		0.0 0.0 00. 8.	0.0 0.0 00. 0.	6.6 6.8 60. 6.
080206Z	40.0 135.5 40 39.9 135.		8.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
	100.0 -0 03.0 100.	· u. u.	J. J. J. J. J.	0.0 0.0 0D. 0 .	0.0 0.0 0n. 0 .

	ALL FORECASTS				TYPHOONS WHILE OVER 35 KT				
	LIRNG	24-HR	48~HR	72-HR	WRHG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	18.	121.	267.	396.	16.	121.	267.	396.	
AVG RIGHT ANGLE ERROR	13.	64.	122.	198.	12.	64.	122.	198.	
AVG INTENSITY MAGNITUDE ERROR	2.	13.	17.	20.	2.	13.	17.	20.	
AVG INTENSITY BIAS	-0.	2.	1.	1.	-0.	2.	1.	1.	
NUMBER OF FORECASTS	43	39	35	31	49	39	35	31	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2811. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 18. KNOTS

SUPER TYPHOON BESS FIX POSITIONS FOR CYCLONE NO. 11

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
						Born
		10.5N 164.8E 10.9N 164.8E			ULCC FIX	PGTW PGTW
3	212100	10.5N 164.1E	PCN 6			PGTU
		11.1N 163.7E 11.8N 162.7E		T1.5/1.5	INIT OBS	PSTW PSTW
6	220600	12.2N 162.3E	PCN 6	1110, 110		PSTW
		12.9N 160.8E 12.7N 160.6E			ULCC FIX	PGTW PGTW
	221600	11.6N 160.9E	PCN 6		ULCC FIX	PGTU
		12.2N 160.2E	PCN 5		ULCC FIX ULCC FIX	PG TW PG TW
		12.0N 160.3E 11.8N 160.4E			ULCC FIX	FGTU
13	230000	13.4N 160.2E	PCN 6	TO 5 10 5 40 40 40 40 40 40 40 40 40 40 40 40 40		PGTU PGTW
15	230401 230900	14.3N 159.8E	PCN 5	T2.5/2.5+/D1.8/24HRS		PGT₩
16	231600	15.1N 158.2E 15.1N 157.9E 15.1N 157.6E	PCN 6		ULCC FIX	PGTW
17 18	231645 231888	15.1N 157.9E	PCN 5			PGTW PGTW
19	232100	15.3N 157.3E	PCN 6		ULCC FIX	PGTW
20	240000	15.6N 157.2E	PCN 6	T3.5/3.5 /D1.9/24HRS	ULCC FIX	PGTW PGTW
22	240600	16.7N 156.9E	PCN 6	T3.5/3.5 /D1.0/24HRS		PGT₩
23	240900	16.2N 156.2E 16.7N 155.4E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
		16.7N 155.1E	PCN 2		EYE DIA 30NM	PGTW
26	241800	16.8N 154.8E	PEN 4			PGTW PGTW
28	250000	16.9N 154.5E 16.9N 154.1E	PCN 4 PCN 2			PGTW
29	250300	16.9N 153.4E	PCN 2	T4 E /4 E /01 0 /04UPC		PGTW PGTW
30	250336 250600	16.9N 153.1E 17.0N 153.1E	PCN 2	T4.5/4.5 /D1.0/24HRS		PGTW
32	250900	16.9N 152.BE	PCN 2			PGTW PGTW
34	251688	17.0N 152.7E 16.9N 152.3E	PCN 2			PGTW
35	251800	16.8N 152.2E 16.6N 152.0E	PCN 2			PGTW FGTW
36 37	252100 260000	16.6N 152.0E	PCN 2			PGTW
38	260300	16.4N 151.9E 16.3N 151.8E	PCN 2			PGTU
	260506 260506	16.0N 151.7E	PCN 1	T5.5/5.5 /D1.0/25HRS T6.0/6.0	INIT OBS	PGTW RPMK
41	269699	15.9N 151.7E	PCN 2	70.00		PGTW
	260900	15.7N 151.7E 15.7N 151.4E	PCN 2			PGTW PGTW
44	261600	15.7N 151.6E	PCN 2			PGTW
45 46	261800	15.8N 151.5E 15.7N 151.4E	PCN 2 PCN 2			PGTW PGTW
47	270000	15.6N 151.0E 15.4N 150.6E	PCN 2 PCN 2			PGTW
48	270300	15.4N 150.6E 15.4N 150.6E	PCN 2	T6.5/6.5-/D1.0/25HRS		PGTW PGTW
	270900	15.4N 150.5E		10.3/6.3-/D1.0/23/R3		PGTIJ
51	271200	15.4N 150.3E	PCN 2 PCN 2			PGTW PGTW
53	271739	15.7N 150.2E 15.8N 150.4E	PCN 2			PGTW
54	271800	16.0N 150.2E	PCN 2 PCN 2			PGTW PGTW
5 6	288888	16.5N 150.0E 17.1N 149.7E	PCN 2			PGTW
	280442	18.2N 149.3E	PCN 2	T6.0/6.0-/W0.5/23HRS		PGTW PGTW
	280600 280900	18.2N 149.3E 18.3N 148.4E 19.0N 147.8E	PCN 2			PGT₩
69	281200	19.0N 146.9E	PCN 2			PGTW PGTW
61 62	201600 201727	19.3N 146.0E 19.6N 145.6E	PCN 2 PCN 1			PGTW
63	281800	19.6N 145.6E	PCN 2			PGTW PGTW
64 65	282100 290000	19.8N 145.1E 20.4N 144.7E	PCN 2 PCN 2			PGTW
66	290300	21.0N 144.0E	PCN 2	TC E (C E / MO E / MINO		FGTW PGTW
67 68	298429 298600	21.2N 143.6E 21.5N 143.4E	PCN 1 PCN 2	T6.5/6.5 /D0.5/24HRS		PGTW
69	290900	21.9N 143.0E	PCN 2	1		PGTW PGTW
70 71	291200 291600	22.3N 142.2E 22.5N 141.5E	PCN 2 PCN 2			PGTW
72	291715	22.5N 141.2E	PCN 1			PGTW
73 74	291800 292100	22.5N 141.2E 23.1N 140.8E	PCN 2 PCN 2			PGTW PGTW
75		23.3N 140.2E	PCN 2			PGTW

91 92 93 94 95 96	300308 300407 300608 301200 301200 301600 301600 310500 310500 310500 311500 311600 311600 311200 010500 010500 020504 020524	23.7N 139.96 23.9N 139.66 24.3N 139.33 24.8N 139.33 24.8N 138.96 25.1N 138.16 25.1N 138.16 25.1N 138.16 25.5N 138.86 25.5N 138.86 26.1N 137.76 26.8N 137.76 27.3N 137.56 27.3N 136.96 29.9N 136.96 39.1N 136.96 39.1N 136.96 39.1N 136.96 39.2N 136.66 39.2N 136.66	PCN 1 T6. PCN 2 PCN 2 PCN 2 PCN 1 PCN 2 PCN 1 PCN 2 PCN 6 PC	0/3 . 0	.5∕25HRS	IMIT OBS INIT OBS			PGTU PGTU PGTU PGTU PGTU PGTU PGTU PGTU		
					AIRCR	AFT FIXES					
FIX NO.	TIME (Z)	FIX POSITION	FLT 700 LVL HG			MAX-FLT-LVL-WND D1R/VEL/BRG/RNG		EYE SHAPE	EYE ORIEN- DIAM/TOTION	EYE TEMP (
123445678991111314415671892112234425627829930	262043 270600 270842 280232 281201 281431 281909 282202 290634 290854 292219 301234 302116 310645 310912	13.0N 161.2E 14.2H 159.0E 15.4H 157.4E 15.7N 156.8E 16.7N 154.7E 17.0N 153.1E 16.4H 152.0E 15.7N 151.7E 15.7N 151.3E 15.7N 151.3E 15.7N 151.3E 15.7N 151.3E 15.7N 151.4E 15.7N 151.4E 15.7N 154.3E 15.9N 150.4E 15.7N 154.3E 15.3N 150.4E 15.3N 150.4E 15.3N 150.4E 15.3N 150.3E 26.3N 137.8E 26.8N 137.8E 26.8N 137.8E 28.1N 137.0E 28.7N 136.8E 31.7N 136.8E 31.7N 136.8E 31.7N 136.8E	700HB 307. 700HB 297. 700HB 297. 700HB 297. 700HB 276. 700HB 276. 700HB 276. 700HB 266. 700HB 267. 700HB 267. 700HB 268. 700HB 253. 700HB 253. 700HB 255. 700HB 255. 700HB 255. 700HB 256. 700HB 267. 700HB 268. 700HB 272. 700HB 272. 700HB 272. 700HB 272. 700HB 272. 700HB 272.	4 998 4 985 4 985 4 978 8 961 9 954 8 949 8 948 8 927 9 948 9 948 1	25 366 15 50 100 08 70 320 30 80 040 30 70 300 45 50 100 55 80 360 38 55 130 69 45 030 185 80 250 40 55 090 90 90 360 35 90 360 35 125 190 10 45 290 25 80 290 15 80 290 15 80 290 110 45 160 120	148 10 170 20 618 40 280 52 220 57 180 80 220 57 180 80 220 57 180 80 220 57 180 30 120 67 040 30 120 67 040 30 120 67 040 30 120 67 040 30 230 86 340 30 610 81 270 20 180 87 360 10 230 83 140 30 020 180 320 20 330 86 4250 48 260 113 140 150 260 104 360 12 170 111 020 20 310 53 180 30 130 101 050 40 170 79 070 60 170 80 240 20 110 65 350 90 240 80 130 120 156 72 070 60 166 69 960 66 080 90 350 90	10 10 3 5 5 10 10 10 10 10 10 10 10 10 10 10 10 10	CIRCULAR CIRCULAR ELLIPTICAL CIRCULAR CIRCULAR CIRCULAR CONCENTRIC CIRCULAR	30 30 20 25 40 20 18	+12 + 8 +12 +14 +15 +14 +10 +11 +13 + 8 +12 +17 +10 +13 +19 +10 +14 +20 +15 +15 +17 +14 +12 +17 +14 +14 +16 +15 + 9 +16 +10 +11 +21 +12 +11 +23 +11 +13 +28 +6 +12 +27 +12 +14 +15 +15 +14 +16 +16 +13 +17 +16 +13 +17 +16 +13 +17 +16	1 2 3 3 4 5 5 6 7 7 7 8 8 8 9 9 10 11 11 12 12 13 14 15 16 17 17 18 19 19 19 19 19 19 19 19 19 19 19 19 19
					RADAR	FIXES					
	TIME (Z)	FIX POSITION	RADAR ACCRY	EYE SHAPE		RADOB-CODE ASWAR TDDFF	С	OMMENTS		RADAR POSITIUN	SITE UMO NO.
2 3	011300 011300	31.6N 136.6E 33.6N 136.9E 33.6N 137.0E 33.6N 136.7E	LAND LAND			5//// ///// 55/// ///// 5//// 51522 6//// 5////				35.3N 138.7E 35.2N 137.0E 35.3N 138.7E 34.6N 135.7E	47639 47636 47639 47773
					SYNOPTI	C FIXES					
FIX NO.	TIME (Z)	FIX POSITION	INTENSITY N ESTIMATE I	EAREST ATA (NM)		COMMENTS					
2 3	011630 011800	34.4N 137.1E 35.1N 137.1E 36.3N 137.1E 37.8N 136.9E	060 060	040 020 040 025	UMO 4766 UMO 4763 UMO 4766 UMO 4766	35 05					

BEST TRACK	WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
			POSIT WIND DST WIND	POSIT WIND DST WIND
	POSIT WIND DST WIND	POSIT WIND DST WIND		
0804122 19.0 130.9 20 0.0		0.0 0.0 aa. c.	0.0 0.0 00. 0.	
080418Z 20.0 127.8 20 0.0		0.0 0.0 00. 0.	0.0 0.0 00. 0.	
080500Z 20.3 127.0 20 0.0		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 0.
080506Z 20.6 126.4 25 20.0		23.8 123.8 40. 2265.	27.0 121.3 50. 38920.	8.0 0.0 00. 0.
0805122 20.7 125.8 25 20.8		22.7 123.8 40. 14810.	24.4 122.1 49. 21850.	26.5 120.7 25. 28795.
989518Z 21.0 125.2 30 21.3	2 125.2 30. 12. 0.	23.0 123.3 45. 15810.	24.9 121.8 35. 24575.	26.9 120.3 25. 296100.
880600Z 20.7 124.8 35 21.3	7 124.6 35. 61. 0.	23.7 122.4 50. 20115.	26.1 120.9 30. 31485.	28.6 119.7 20. 363100.
080606Z 20.1 124.6 45 20.	1 124.6 45. 0. 0.	21.4 122.9 55. 5415.	22.6 120.2 45. 18175.	23.1 117.2 39. 37380.
	6 124.8 50. 29. 0.	22.0 123.2 60. 6230.	22.9 120.8 50. 14770.	23.5 118.4 30. 299. ~75.
	5 124.3 55. 6. 0.	21.3 123.0 65. 2545.	22.3 120.8 60. 15465.	23.2 118.8 35. 29165.
	9 123.9 65. 13. D.	21.5 122.8 75. 3440.	22.5 120.5 55. 19B. ··65.	23,5 118.1 35. 31160.
	Ø 123.7 70. 6. 0.	21.6 122.5 85. 4535.	22.7 120.2 55. 22855.	23.5 117.7 35. 35455.
	9 123,8 90, 18. 0.	22.0 123.2 100. 2620.	24.1 121.9 105. 113. 0.	26.2 120.8 60. 14725.
	0 123.4 95. 615.	22.0 122.4 100. 8125.	23.7 121.2 105. 170. 5.	25.9 120.3 55. 18920.
		22.8 122.2 115, 1075.	24.8 121.9 100, 105. 5.	26.2 122.4 80. 108. 10.
		23.5 122.5 120. 97. 10.	25.5 122.3 105. 89. 15.	27.1 122.9 85. 63. 20.
		24.5 123.1 115. 53. 10.	26.5 122.8 100. 50. 15.	28.6 123.0 80. 49. 20.
	2 123.4 120. 12. 0.			29.2 122.9 80. 60. 25.
	9 123.4 120. 65.	25.2 122.9 110. 42. 10.		
	9 123.9 120. 8. 0.	28.1 126.2 100. 207. 5.		
	8 123.7 115. 13. 5.	28.6 125.0 100. 148. 10.	32.6 122.1 80. 285. 15.	35.5 117.6 59. 448. 0.
	3 123.8 10516. 0.	27.8 123.6 90. 39. 5.	30.0 124.7 75. 105. 15.	31.8 126.3 65. 120. 15.
	8 123.2 95. 55.	28.2 122.2 75. 80. 0.	30.2 123.3 60. 86. 5.	32.2 125.2 45. 61. 0.
081000Z 26.3 122.9 95 26.4	4 122.8 90. 85.	28.6 122.3 75. 83. 5.	30.5 123.4 60. 68. 10.	32.1 125.3 45. 124. 0.
081006Z 26.8 123.1 90 26.5	.8 122.8 85. 165.	29.2 122.8 65. 81. 0.	31.3 124.2 50. 61. 0.	32.7 126.3 40. 2045.
0810122 27.2 123.3 85 27.3	3 123.3 90. 65.	29.2 124.4 60. 55. 0.	31.1 125.3 45. 625.	33.4 124.6 30. 15915.
081016Z 27.4 123.4 75 27.	7 123.4 75. 18. 0.	29.4 124.6 60. 43. 5.	31.3 125.2 40. 785.	33.6 124.5 30. 19310.
	8 123.3 70. 12. 0.	29.9 124.3 55. 29. 5.	31.8 124.2 40. 1085.	33.8 123.5 25. 21115.
	Ø 123.2 65. 16. Ø.	29.5 123.8 50. 49. 0.	31.4 124.0 35. 20410.	0.0 0.0 00. 0.
	3 123.8 60. 8. 0.	29.9 124.8 45. 815.	31.4 124.7 30. 26915.	0.0 0.0 0. -0. 0.
081118Z 28.9 124.0 55 28.		30.2 125.0 40. 1255.	31.7 124.5 35. 3005.	0.0 0.0 00. 0.
	8 124.0 50. 18. 0.	32.1 123.7 35. 8510.	32.8 122.9 25. 27015.	6.0 9.0 EO. O.
	2 124.0 50. 6. 0.	32.6 124.1 35. 13710.	34.8 125.2 25. 20215.	0.0 0.0 0O. O.
	.0 124.1 50. 6. 0.	33.2 124.2 35, 160, -10.	35.5 124.9 25. 17610.	0.0 0.0 00. 0.
	.2 124.2 45. 12. 0.	37.7 127.0 30. 21310.	0.6 0.0 06. 0.	0.0 0.0 08. 0.
	.2 123.8 40. 235.	38.8 126.7 30. 19710.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	.2 123.8 40. 235. .8 123.1 40. 85.	40.0 126.6 29. 20311.	0.0 0.0 00. 0.	8.0 8.0 0. ·0. 0.
	.8 123.1 46. 65. .8 122.8 35. 1210.	0.0 0.0 00. 0.	8.0 0.0 00. 0.	0.0 0.0 00. 0.
		0.0 0.0 00. 0.	8.8 8.6 80. 8.	0.0 0.0 0. ·0. 0.
			0.0 0.0 00. 0.	8.8 9.0 0. ·0. 0.
	.2 122.7 49. 16. 8.		0.0 0.0 00. 0.	0.0 0.0 00. 0.
081406Z 37.8 123.3 40 38.		0.0 0.0 00. 0.		9.0 9.8 90. 0.
	.5 124.0 35. 15. 0.	0.0 0.0 00. 0.	0.0 0.0	
081418Z 38.9 125.6 30 38.	.9 125.4 30. 9. 0.	0.0 6.0 60. 6.	0.0 0.8 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	wrng	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	14.	102.	172.	219.	14.	102.	172.	219.		
AVG RIGHT ANGLE ERROR	9.	41.	75.	141.	9.	41.	75.	141.		
AVG INTENSITY MAGNITUDE ERROR	2.	12.	25.	36.	2.	12.	25.	36.		
AVG INTENSITY BIAS	-2.	-8.	-18.	-27.	-2.	-8.	-18.	-27.		
NUMBER OF FORECASTS	39	33	30	23	35	33	30	23		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1665. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

TYPHOON CECIL FIX POSITIONS FOR CYCLONE NO. 12

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
		19.6N 128.7E	PCN 5			PGTU
	042125	20.0N 127.6E	PCN 6			PGTW
	050000 050600		PCN 4	T1.5/1.5	INIT ORS	PGTW PGTW
	050900		PCN 6	11.3/1.3	1111 1103	PGTW
	051200	21.0N 125.9E	PCN 6			PGTW
	051600		PCN 6			PGT₩
	051800		PCN 6		III.CC ETV	FGTW
	052100 060000		PCN 6 PCN 4		ULCC FIX	PGTW PGTW
11	060300	20.7H 123.8E	PCN 4			PGTW
	060600	20.2N 124.4E		T3.0/3.0+/D1.5/24HRS		PGTW
	060617		PCN 1	T3.5/3.5	INIT OBS	RPMK
	060900 061200	20.3N 124.5E 20.3N 124.4E	PCN 4 PCN 1			PGTW PGTW
	061600	20.3N 124.3E	PCN 4			PGTW
17	061800	20.6N 124.2E	PCN 2			PGTW
	061902		PCN 3			PGTW PGTW
	062100 070000		PCN 4 PCN 4			PGTW
	070300		PCN 6			PGTW
	070605		PCN 1	T4.5/4.5 /D1.5/24HRS		PGTW
	970605		PCN 1	T5.0/5.0+/D1.5/24HRS		RPIK PGTW
	070900 071200		PCN 2 PCN 2			PGTU
26	8 71600	20.9N 123.5E	PCN 2			PGTW
	071800		PCN 2			PGTW
	071850 072100		PCN 2 PCN 2			PG TW PG TW
		21.3N 123.5E	PCN 2		er e	PGTW
31	080300	21.6N 123.3E	PCN 2			FGTW
	080553	21.5N 123.5E		T5.5/5.5-/D1.8/24HRS		PGTU
	080900 081200	22.2N 123.5E 22.3N 123.5E	PCN 2 PCN 2			PG TW PG TW
		22.7N 123.5E	PCN 2			PGTW
36	001000	22.9N 123.6E	PCN 2			PGTW
	001030		PCN 1			PGTW PGTW
		23.3N 123.8E 23.8N 123.8E	PCN 2 PCN 2			PGTW
48	090300	24.4N 123.6E	PCH 2			PGTW
	090541	24.7N 123.5E		T6.0/6.0-/D0.5/24HRS		PGTW
	090900	25.2N 123.7E 25.5N 123.5E	PCN 2 PCN 2			PGTW PGTW
		25.8N 123.1E	PCN 2			PGTW
	091800		PCN 2			PGTW
	092100 100000	26.2N 123.0E 26.3N 123.1E	PCN 2 PCN 2			PGTW
		26.5N 123.1E	PCN 2		EYE DIA 18NM	PGTW PGTW
49	100528	26.7N 123.5E	PCN 1	T5.0/5.0 T4.5/4.5 /41.5/23HRS	INIT OBS	RODN
	100529			T4.5/4.5 /W1.5/23HRS		PGTW
		27.0N 123.3E 27.3N 123.2E	PCN 4 PCN 4			PGTW PGTW
		27.3N 123.2E	PCN 4			PGTW
		27.4N 123.4E	PCN 4			PGTW
55 56		27.6N 123.2E 27.7N 123.4E	PCN 4 PCN 4			PGTU PGTU
	110300		PCN 4		ULCC FIX	PGTW
58	110517	27.8N 123.5E		T3.5/4.0 /J1.0/24HRS		PGT₩
	110900 111200		PCN 2 PCN 4			PGTW PGTW
		28.6N 124.2E	PCN 4			PGTU
62	111800	28.9N 124.1E	PCN 6			PGTW
		29.7N 123.7E	PCN 6		ULCC FIX	PGTU
64 65	120300 120600	29.8N 124.0E 30.1N 124.0E	PCN 6 PCN 2	T3.5/3.5~/S0.0/25HRS	ULCC FIX	PGTW PGTW
66	120900	30.7N 124.1E	PCN 2	7010-010-0010-0010-		PGTU
		31.5N 124.0E	PCN 4			PGTW
	121600	31.9N 124.2E 32.1N 123.8E	PCN 4 PCN 6			PGTW PGTW
	122100		PCN 4			PGTW
71	122100	29.6N 123.7E	PCN 6			PGTW
		33.5N 123.4E	PCN 4			PGTW
		33.9N 123.0E 34.6N 122.9E	PCN 4 PCN 6	T2.5/3.8 /W1.8/24HRS		PGTW PGTW
	130900		PCN 6	12.070.0 /WI.0/24NK3		PGTW
76	131200	35.6N 122.8E	PCN 6			PGTW
	131600		PCN 6			PGTU
	131800 132100	36.4N 122.8E 36.7N 122.9E	PCN 6 PCN 6			PGTW PGTW
80	140000	37.3N 123.5E	PCN 6			PGTW
81	140300	37.4N 124.2E	PCN 6		ULCC FIX	PGTW
		37.7N 123.7E	PCN 6 PCN 6	T2.0/2.5 /W0.5/24HRS	ULCC 37.5N 124.5E	PGTW PG FW
		37.9N 124.0E 38.4N 125.4E	PCN 6		ULCC 37.7N 127.1E	PGTW
85	141600	38.5N 125.7E	PCN 6			PGTW
86	141800	38.7N 126.1E	PCN 6			PGTW

65	090930	25.1N 123.7E	LAND	10811 40507	24.0H 121.6E	46695
66	091000	25.1N 123.6E	LAND	11812 53508	24.8N 125.3E	47.97.
67	091000	25.2N 123.7E	LAND	11813 73509	24.3N 124.2E	47918
68	091000	25.2N 123.7E	LAND	10932 43511	24.0N J21.6E	46699
69	091000	25.2N 123.5E	LAND	6//// 53509	24.0H 121.6E	46763
70	091030	25.2N 123.6E	LAND	10822 43116	24.0N 121.6E	46699
71	091100	25.3N 123.6E	LAND	11813 73407	24.3H 124.2E	47918
72	091100	25.2N 123.5E	LAND	11013 53211	24.BN 125.3E	47927
73	091200	25.3N 123.3E	LAND	6//// 53008	25.1N 121.6E	46696
74	091200	25.5N 123.5E	LAND	10823 43111	24.9H 121.6E	46699
75	091200	25.4N 123.5E	LAND	11834 73307	24.3H 124.2E	47918
76	091200	25.3N 123.5E	LAND	11813 53306	24.8H 125.3E	47927
77	091300	25.5N 123.5E	LAND	11814 73308	24.3N 124.2E	47918
78	091408	25.6N 123.4E	LAND	10823 43605	24.0N 121.6E	46693
79	091400	25.6N 123.4E	L'AND	21844 73307	24.3H 124.2E	47918
80	091400	25.5N 123.3E	LAND	11813 53211	24.8H 125.3E	47927
81	091500	25.6N 123.4E	LAND	21813 73305	24.3N 124.2E	47918
82	091500	25.6N 123.3E	LAND	10813 53505	24.50 125.3E	47927
83	091600	25.7N 123.3E	LAND	5//43 73104	24.31 124.25	47019
84	091600	25.6N 123.1E	LAND	21863 52911	24.8N 125.3E	47927
- 85	091630	25.9N 123.1E	LAND	10913 43309	24.0N 121.6E	46699
86	091700	25.9N 123.2E	LAND	6//// 5330G	25.1N 121.6E	46696
87	091700	25.9N 123.1E	LAND	10923 40000	24.0N 121.6E	46699
88	091700	25.8N 123.1E	LAND	6///3 73207	24.3N 124.2E	47918
69	091700	25.7N 123.1E	LAND	20844 53611	24.8H 125.3E	47927
90	091700	25.9N 123.1E	LAND	10923 40000	24.0N 121.6E	45763
91	091800	25.9N 123.1E	LAND	6///3 73207	24.3N 124.2E	47918
92	091800	25.9N 123.1E	LAND	10873 53311	24.8N 125.3E	47927

SYNOPTIC FIXES

FIX	TIME	FIX	INTENSITY	NEAREST	COMMENTS
NO.	(Z)	POSITION	ESTIMATE	DATA (NM)	
1 2 3	060000 140000 141800	20.8N 124.1E 37.5N 123.0E 38.9N 125.2E	035 035 030	040 020 040	SHIP OBSERVATION WMO 54775

	BEST TRAC	<	WARN				24 H	OUR FO				48 H	OUR F	ORECA			72 H		ORECAS	
				ERR					ERR					ERRO					ERRORS	
MO/DA/HR	POSIT WIND	POSIT	MIND	DST		POS		MIND		MIND	POS		MIND			POS		MIND		MIND
080800Z	7.7 153.9 20	9.0 0.		-0.	Θ.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.
080806Z	8.1 152.4 25	0.0 0.	00.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
0808122	8.7 151.4 25	0.0 0.	0 0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	U.0	0.	-0.	ø.
080818Z	9.7 149.6 30	0.0 0.	0 0.	-0.	8.	0.0	8.0	ø.	-0.	0.	0.0	6.0	0.	-0.	0.	0.0	9.0	9.	-0.	0.
080900Z	10.4 148.8 38	10.1 149.	9 30.	67.	ø.	11.8	146.1	40.	306.	-5.	13.8	141.4	65.	351.	0.	15.0	136.7	90.	293.	15.
080906Z	10.9 147.4 35	11.2 147.	5 35.	19.	0.	13.0	143.2	50.	228.	0.	14.7	138.7	70.	256.	-10.	15.8	133.8	90.	201.	35.
0809122	10.8 144.5 48	10.8 144.	8 40.	18.	0.	12.2	138.7	55.	48.	Ø.	13.8	134.0	75.	50.	-5.	15.8	129.5	95.	99.	50.
080918Z	11.6 142.5 45	11.4 142.	3 45.	17.	0.	12.8	136.4	65.	12.	5.	14.6	131.8	80.	55.	5.	17.0	127.4	100.	116.	50.
981999Z	12.0 140.9 45	12.0 140.	7 45.	12.	ø.	13.3	135.8	70.	23.	5.	13.9	130.7	BØ.	128.	5.	15.4	126.0	100.	248.	50.
981896Z	12.2 139.4 50	12.0 139.	0 50.	26.	Θ.	13.1	133.9	65.	51.	-15.	13.8	129.0	80.	203.	25.	15.9	124.8	95.	277.	40.
081012Z	12.6 138.0 55	12.3 138.	3 55.	25.	0.	13.1	133.5	70.	78.	-10.	13.8	128.7	85.	227.	40.	16.2	124.2	100.	279.	40.
081018Z	13.0 136.4 60	12.4 136.	9 55.	46.	-5.	13.8	132.2	75.	81.	Ø.	15.0	128.8	85.	198.	35.	15.4	125.1	100.	336.	40.
081100Z	13.3 135.4 65	13.2 135.	0 65.	24.	0.	15.2	130.3	85.	89.	10.	16.4	126.4	95.	184.	45.	16.8	122.8	105.	273.	45.
081106Z	13.8 134.4 80	13.3 134.	2 80.	32.	0.	15.3	130.7	100.	84.	45.	16.8	126.9	110.	198.	5 5.	17.1	123.2	115.	270.	55.
081112Z	14.4 133.4 80	14.2 133.	6 80.	17.	0.	16.6	130.3	100.	53.	55.	18.1	127.0	105.	165.	45.	19.2	123.7	110.	180.	50.
981118Z	15.1 132.6 75	14.5 132.	6 85.	36.	10.	16.5	129.2	105.	109.	55.	17.6	126.2	110.	219.	50.	18.6	123.4	119.	244.	50.
981209Z	15.8 131.7 75	15.8 131.	0 75.	40.	0.	18.2	127.0	85.	72.	35.	20.8	123.8	90.	26.	30.	24.8	121.2	100.	125.	60.
081206Z	16.7 130.8 55	16.0 130.	5 75.	45.	20.	18.7	127.2	85.	87.	30.	21.7	124.7	90.	84.	30.	25.2	123.1	100.	263.	65.
ØB1212Z	17.4 129.9 45	17.6 130.	9 45.	13.	0.	21.2	127.2	60.	86.	ø.	24.2	126.2	70.	256.	10.	27.3	126.1	75.	473.	45.
0 81218Z	18.3 128.9 50	18.5 129.	2 50.	21.	Ø.	21.8	126.9	60.	127.	ø.	24.9	126.1	70.	305.	10.	28.2	126.2	75.	520.	55.
081300Z	19.2 127.7 50	19.2 127.	8 50.	6.	ø.	23.2	125.2	65.	137.	5.	27.2	124.7	75.	363.	35.	0.0	9.0	Ø.	-0.	ø.
0B1306Z	20.1 126.8 55	20.2 126.	8 55.	6.	0.	24.8	124.8	65.	211.	5.	29.3	124.7	75.	464.	48.	0.0	9.0	ø.	-0.	0.
ØB1312Z	20.6 125.8 60	21.0 125.	8 60.	24.	0.	24.8	123.5	79.	186.	10.	28.2	122.8	75.	344.	45.	0.0	0.0	0.	-0.	0.
081318Z	21.0 124.8 60	21.7 125.	1 60.	45.	0.	24.8	122.B	75.	174.	15.	27.8	121.6	70.	288.	50.	0.0	0.0	8.	-0.	ø.
981499Z	21.2 124.0 60	21.2 124.	0 60.	0.	0.	22.8	120.8	65.	80.	25.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
081406Z	21.6 123.2 60	21.5 123.	2 60.	6.	0.	23.2	119.7	50.	78.	15.	0.0	9.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
081412Z	21.9 122.3 60	21.8 122.	5 60.	13.	ø.	23.3	119.1	40.	98.	10.	0.0	0.0	ø.	0.	0.	0.0	0.0	0.	-0.	0.
0B1418Z	22.2 121.4 60	22.0 121.	6 60.	16.	0.	24.0	117.8	40.	81.	20.	0.0	8.9	0.	-0.	0.	0.0	9.0	ø.	-0.	0.
0B1500Z	23.4 119.5 48	23.4 119.	6 40.	6.	Ø.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
081506Z	23.9 118.5 35	23.8 118.	6 35.	Θ.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	Ø.	-0.	0.
Ø81512Z	24.5 117.9 30	24.4 117.	7 30.	12.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
Ø81518Z	25.2 117.1 20	0.0 0.	0 0.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	Θ.	-0.	0.	0.0	0.0	ø.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	35 KTS		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	22.	100.	218.	262.	21.	109.	207.	229.
AVG RIGHT ANGLE ERROR	17.	68.	172.	208.	17.	73.	157.	180.
AVG INTENSITY MAGNITUDE ERROR	1.	16.	29.	47.	1.	16.	26.	46.
AVG INTENSITY BIAS	1.	13.	27.	47.	1.	13.	25.	46.
NUMBER OF FORECASTS	27	24	20	16	25	22	18.	14

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2435. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

13. KNOTS

TYPHOON DOT FIX POSITIONS FOR CYCLONE NO. 13

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	071800	7.7N 156.7E	PCN 6			PGTW
2	072100	6.8N 153.5E	PCN 6			PGTW
3	000000	8.0N 153.2E	PCN 4	T1.0/1.0	INIT OBS	PGTW
4	080411	7.8N 152.6E	PCN 3	11.0-1.0	1111 003	PGTW
5	080600	8.5N 152.0E	PCN 6		ULCC FIX	PGTW
6	080900	8.8N 151.7E	PCN 6		ULCC FIX	PGTW
* 7	081800	9.1N 148.4E	PCN 6		OLCC I IX	PGTW
* 8	082100	10.0N 147.6E	PCN 6			PGTW
9	090000	10.3N 149.9E	PCN 4	T2.0/2.0 /D1.0/24HRS		PGTW
10	090300	10.9N 149.3E	PCN 6	1210, 210 12110, 2-4110		PGTW
11	090600	11.4H 147.7E	PCN 6		BASED ON EXTRAP	PGTW
12	090900	11.4H 146.1E	PCN 6		ULCC FIX	PG'TW
13	091200	11.9N 144.9E	PCH 6			PGTW
14	09.1600	11.6N 142.7E	PCN 6			PGTW
15	091644	11.5N 142.9E	PCN 6			PG'TW
16	091800	11.6N 142.4E	PEN 6			PGTW
17	092100	11.7N 141.5E	PCN 6			PGTW
18	100000	11.4N 140.7E	PCN 6	T2.5/2.5 /D0.5/24HRS		PGTU
19	100300	11.6N 140.0E	PCN 6		ULCC FIX /	PGTW
28	100529	12.0N 139.4E	PCN 5			PGTW
21	100900	12.2N 138.9E	PCH 6			PGTW
22	101200	12.4N 138.0E	PCN 6			PGTW
23	101600	12.5N 136.6E	PCN 6			PGTW
24	101800	12.7N 135.8E	PCN 6			PGTW

25	101813	13.0N 136.3E	PCN 5		PSTU
26	102100	13.1N 135.8E	PCN 6		PGTU
27	110000	13.3N 135.6E	PCN 6	T3.5/3.5 /D1.0/24HRS	PGTU
28	110308	13.5N 135.2E	PCN 6		LCLM
29	110517	13.8N 134.5E	PCN 1		PGTW
30	110900	14.1N 133.7E	PCN 4		POTA
31	111200	14.2N 133.3E	PCN 6		PGTU
32	111600	14.4N 132.6E	PCN 6		PGTW
* 33	111800	14.1N 132.1E	PCN 6		PGTM
34	112100	14.9N 131.2E	PCN 6		PGTU
35	120000	15.2N 131.1E	PCN 6	T4.5/4.5-/D1.0/24HRS	PGTU
36	120300	15.9N 131.2E	PCN 6		PGTVI
37	120600	16.7N 131.2E	PCN 6		PGTW
* 38	120647	16.3N 129.6E	PCN 5		RPLK
39	120900	16.8N 131.3E	РСН 6		PGTM
40	121200	17.2N 129.8E	РСН Б		PGTO
41	121600	17.6N 129.4E	PCN 6		PGTM
42	121750	18.8N 128.9E	PCN 5		POTU
43	122100	18.9N 128.5E	РСН Б		PS FM
44	130000	19.0N 127.7E	PCN 6		PGTU
45	130300	19.6N 127.5E	PCN 6	T3.0/3.5 /W1.5/27HRS	PGTW
46	130600	20.4N 126.8E	PCN 6		PGTW
47	130900	21.0N 126.5E	PCN 6		PSTW
48	131200	21.3N 126.3E	PCN 6		PGTU
49	131600	21.7N 125.5E	PCN 6		PSTU
50	131800	21.BN 125.1E	FCN 6		PGTU
51	132100	21.7N 124.3E	PCN 6		PGTW
52	140000	21.0N 124.0E	PCN 6		PS IW
53	140300	20.9N 123.5E	PCN 6		PGTW
54	140622	21.3N 123.0E	PCH 5	T2.0/3.0 /W1.0/27HR5	PGTW
55	140900	21.2N 122.6E	PCN 6		PGTW
56	141200	21.6N 122.6E	PCN 4		PG TW
57	141600	22.0N 121.7E	PCN 4		PGTW
58	141800	22.1N 121.4E	PCN 4		PGTW
59	141907	22.2N 121.1E	PCN 4		PGTW
60	142100	22.5N 120.4E	PCH 4		PGTU
61	150000	23.1N 119.7E	PCN 6		PG IW
62	150300	24.0N 118.5E	PCN 6		PGTU
63	150610	23.4N 119.1E	PCN 5	T1.0/2.0 /J1.0/24HRS	PGTW
64	150900	24.3N 118.6E	PCN 6		FGTU
65	151200	24.4N 117.7E	PCN 6		PGTW
€6	151600	25.0N 116.6E	PCN 6		PGTW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC VEL/BRG			FLT-L VEL/B			ACC NAV		EYE SHAPE		OR IEN- FAT ION			EMP (C) / DP/SST	MSN NO.
* 1	080210	8.4N 153.2E	1500FT		1005	15 020	95	060	38 3	100	143	5	10				+23	+23	+2B	
2	<i>0</i> 90118	10.8N 148.5E	1500FT		1003	40 080	50	120	41 1	00	100	3	8					121		,
3	090322	10.9N 148.1E	700MB	3084	1003	30 330	56	130	52 0	30	10	3	4					+13		5
4	090715	10.0N 145.9E	700MB	3087		45 040	88	100	44 B	130	120	6	8						• •	3
5	091022	9.9N 144.8E	700MB	3099	1006			120	41 3	60	120	10	25				+11	+ 8		3
6	092209	11.9N 141.5E	700MB	3054	998	30 320	30	100	44 3	20	30	10	28				+12		+ 9	4
7	100653	12.6N 139.3E	700MB	2982	989	60 360	10	210	64 9	160	55	5	8					+16		5
8	100831	12.5N 138.8E	700MB	2982	987	55 330	15					5	8					+13		5
9	101911	13.1N 136.3E	700MB	2908				330	33 2	30	10	7	3					+15		6
10	102151	13.0N 135.9E	700MB	2925	979	78 879	15	170	72 Ø	190	42	7	2	CIRCULAR	40			+16		6
11	110607	13.7N 134.5E	700MB	2847		90 060	14	090	72 3	49	27	2	2							7
12	110052	13.9N 134.0E	700MB	2844	971	55 280	11	330	61 2	80	11	3	2	ELLIPTICAL	10 08	020	F12	+16	+10	7
13	111926	14.8N 131.1E	786MB	2959				178	75 0	170	25	10	5							8
14	112219	15.5N 132.0E	790MB	2990	986	50 340	60	129	55 3	60	20	В	10				+13	+17		8
15	120901	17.2N 130.5E	700MB	3025		49 340	60	010	45 2	80	60	5	10					+15	+ 9	10
16	122019	18.6N 128.2E	700MB	3002		40 100	60	010	44 2	60	30	10	10						-	11
17	122202	18.8N 127.BE	700MB	2978		30 020	120	150	48 0	30	90	5	В				+18	+16	+11	11
18	130950	20.4H 126.1E	700MB	2977	986	75 100	40	120	81 6	30	45	5	В				+13	+18		12
19	131128	20.5N 125.8E	700MB	2984				689	70 3	40	40	10	10							12
20	131904	21.2N 124.7E	700MB	2962				119	75 3	40	20	₿	8							13
21	132150	21.2N 124.4E	700MB	2980	986	50 350	20	110	55 3	50	98	5	8				+14	+18	+ 6	13
22	140710	21.6N 123.0E	700MB	2992		50 000	30	170	46 0	80	60	5	3							14
23	141010	21.6N 122.8E	700MB	2977		65 010	30	110	48 Ø	10	75	5	5				+16	+17	+ 8	14

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	DIAM	RADOB-CODE ASWAR TDDFF	COMMENTS	RADAR POSTTION	SITE WMO NO.
1 2 3	090935	11.6N 145.9E 11.7N 145.2E 12.5N 143.8E	LAND	FAIR POOR POOR					13.6N 144.9E 13.6N 144.9E 13.6N 144.9E	91218 91218 91218

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE			COM	ENTS
		22.8N 120.2E 23.4N 119.6E	040 040	010 015	46745. 46730,		

TYPHOON ELLIS BEST TRACK DATA

	BEST TRACK	. WARNI	NG ERRORS	24 HOUR F	ORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST
MO/DA/HR	POSIT WIND	POSIT WIND	DST WIND	POSIT WIND			ERRORS
081706Z	8.2 154.2 20						POSIT WIND DST WIND
0817122				0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.0 9.0 00. 0.
		0.0 0.0 0.	-0. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.9 9.6 90. 0.
Ø81718Z	B.1 152.1 20	0.0 0.0 0.	-0. 0.	0.0 0.0 0.	-0. 0.	0.3 0.0 00. D.	8.9 8.0 80. 8.
081800Z	8.0 151.1 25	0.0 0.0 0.	-0. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.6 9.9 80. 8.
001806Z	8.1 150.0 25	0.0 0.0 0.	-0. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	9.0 9.0 % -0. 0.
001812Z	8.2 148.8 25	8.0 9.0 0.	-0. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.0 0.0 U0. O.
081818Z	8.5 147.4 30	8.8 148.2 25.	515.	9.6 146.2 40.	2065.	10.8 144.3 50. 30620.	12.0 141.5 79. 32625.
081900Z	8.8 146.1 30	9.1 146.1 30.	18. 0.	10.8 143.5 50.	985.	12.2 140.3 60. 12215.	12.8 136.7 70. 19830.
0B1906Z	9.4 145.0 30	9.7 144.5 30.	35. 0.	11.2 141.1 50.	5410.	11.9 137.7 65. 15015.	11.9 134.0 75. 31330.
	10.2 143.9 35	10.2 144.2 35.	18. 0.	11.9 140.9 50.	5515.	13.4 137.4 65. 19229.	14.2 133.9 80, 22135.
	10.9 142.9 45	10.8 143.2 35.	1910.	12.5 139.8 55.	4215.	13.7 135.8 70. 14325.	14.0 131.7 85. 29535.
	11.5 142.0 55	11.6 142.0 50.	65.	13.2 138.1 60.	6415.	14.5 134.2 75. 17425.	15.8 138.2 85. 33840.
	12.1 141.0 60	12.2 141.2 55.	135.	14.5 137.4 70.	5910.	15.4 133.0 85. 19520.	16.2 128.5 100. 40825.
	12.6 140.3 65	12.7 140.4 60.	85.	14.7 136.8 75.	7210.	15.9 133.B 90. 14625.	17.4 131.2 INU. 27415.
082018Z	13.2 139.7 70	13.3 139.4 60.	1910.	15.4 136.2 75.	6520.	16.9 133.2 90. 14730.	18.2 130.6 105, 282, -10.
082100Z	13.8 139.0 75	13.8 139.0 65.	010.	15.2 136.5 75.	5525.	16.4 134.3 90. 171. ··35.	17.7 132.5 101. 34310.
082106Z	14.3 138.4 80	14.1 130.3 70.	1310.	15.5 136.1 00.	7225.	16.7 133.9 95. 21130.	17.5 132.1 105. 3725.
082112Z	15.0 138.0 85	14.9 137.7 70.	1815.	17.0 135.2 90.	4225.	18.2 133.0 100. 18720.	19.8 139.8 119. 291. 5.
0821182	15.6 137.3 95	15.8 137.3 75.	1220.	17.8 134.8 95.	4125.	19.8 132.4 105. 14910.	21.8 139.3 113. 226. 15.
082200Z	16.1 136.7 190	15.8 136.8 95.	195.	17.2 135:1 125.	121. 6.	18.8 133.3 130. 247. 15.	20.7 131.2 135, 324, 35,
082206Z	16.7 136.1 105	16.8 136.1 110.	6. 5.	18.9 134.1 135.	79. 10.	20.6 132.2 140. 186. 30.	22.7 131.0 135, 240, 40,
	17.4 135.8 115	17.4 135.8 120.	0. 5.	20.1 134.2 135.	68. 15.	21.9 132.5 140. 158. 35.	24.1 131.3 130. 203. 40.
	18.3 135.3 120	18.2 135.4 125.	8. 5.	20.9 134.1 140.	82. 25.	22.8 132.7 135, 158, 35,	25.2 132.0 130, 190, 40,
	19.2 134.9 125	19.2 135.1 125.	11. 0.	21.7 133.6 135.	82. 20.	23.8 132.2 130, 148, 30,	25.9 131.1 120. 176. 35.
	20.2 134.3 125	20.2 134.4 125.	6. 0.	22.7 132.8 130.	64. 20.	25.2 131.5 125. 98. 30.	27.5 130.6 115. 132. 35.
	21.2 133.9 120	21.2 134.1 120.	11. 0.	24.5 132.2 120.	5. 15.	27.0 130.9 120. 32. 30.	29.2 130.1 120. 107. 45.
	22.1 133.4 115	22.1 133.4 120.	0. 5.	25.3 131.8 120.	0. 20.	27.9 130.6 120. 12. 30.	30.2 (29.5 128, 156, 55,
	22.9 132.9 115	23.0 132.9 120.	6. 5.	26.7 131.0 109.	38. 0.	32.4 130.0 75. 21810.	39.8 133.6 49, 379, -20.
	23.7 132.4 118	23.7 132.4 115.	0. 5.	27.3 130.4 95.	42. 8.	34.1 138.8 65. 26415.	0.0 0.0 00. 0.
	24.5 132.1 105	24.4 132.1 105.	6. 0.	28.1 130.4 95.	42. 5.	34.4 130.8 65. 22310.	0.0 9.9 00. 9.
	25.3 131.8 100	25.4 131.7 100.	8. 0.	29.2 130.2 90.	69. B.	35.5 131.2 55. 21810.	8.8 6.8 8B. 8.
	26.1 131.2 100	26.2 130.9 95.	175.	31.2 129.4 65.	15720.	38.2 132.3 40. 27620.	
	26.7 130.8 95	27.0 130.8 90.	185.	32.0 129.6 65.	15115.		
	27.4 130.5 90						9.8 ค.ย กอ. อ.
		27.3 130.4 85.		31.5 129.7 60.	9115.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	28.1 130.6 90	28.2 130.4 80.	1210.	31.4 129.8 55.	10610.	8.8 6. 0 00. 0.	0.0 0.0 00. 0.
	28.8 130.6 85	28.9 130.5 80.	85.	33.2 130.4 50.	8810.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	29.7 130.8 80	29.8 130.6 75.	125.	35.1 130.2 45.	95. 0.	0.0 0.0 d0. 0.	0.9 0.0 n0. o.
	30.7 131.2 75	30.7 131.1 70.	55.	36.3 131.0 45.	139. 5.	0.0 0.0 00. 0.	8.6 0.0 00. 9.
	31.9 131.8 65	31.8 131.8 65.	6. Ø.	0.0 0.0 0.	-0. 0.	8.0 8.0 8. ~8. 8.	0.0 0.0 00. 0.
	33.6 132.1 60	32.7 132.0 60.	54. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	35.7 132.0 45	35.1 132.0 50.	36. 5.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0827122	38.5 131.9 40	38.7 131.8 40.	13. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0 00. 0.	0.0 0. 0 00. 0 .

	ALL	FORECAS	TS		TYPHO	ONS WHIL	35 KTS	
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72~HR
AVG FORECAST POSIT ERROR	14.	76.	171.	263.	12.	76.	171.	263.
AVG RIGHT ANGLE ERROR	8.	42.	81.	153.	8.	42.	81.	153.
AVG INTENSITY MAGNITUDE ERROR	5.	13.	23.	28.	5.	13.	23.	28.
AVG INTENSITY BIAS	-3.	-4.	-5.	3.	-3.	-4.	-5.	3.
NUMBER OF FORECASTS	36	32	26	22	33	32	26	22

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2640. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON ELLIS FIX POSITIONS FOR CYCLONE NO. 14

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DYORAK CODE	CONTENTS	SITE
		100111011	HOURT	DYONAN COLC	CUITERIS	2115
1	170404	0 10 154.05	DO: -	T		
2	171688	9.1N 154.8E 7.7N 152.8E	PCN 5	T1.0/1.0		PGTW
3	171649	7.5N 152.7E	PCN 5			PGTW
4	172100	7.1N 151.7E	PCN 6			PGTW PGTW
5	180000	7.5N 151.6E	PCN 6	*	BASED ON EXTRAP	PGTW
6	180300	8.0N 150.9E	PCN 6	T1.5/1.5 /D0.5/23HRS	BASED ON EXTRAP	PGTW
7	180600	8.1N 150.2E	PCN 6		white dir Erring	PGTW
8	180900	8.1N 149.5E	PCN 6		ULCC FIX	PGTW
9	181200	8.6N 148.4E	PCN 6			PGTW
10	181600	8.3N 148.1E	PCN 6			PGTW
11	181637	8.2N 148.1E	PCN 5			PGTU
	181800	8.2N 148.0E	PCN 6			PGTW
13	182100	8.2N 147.6E	PCN 6			PGTW
14	190000	9.4N 145.4E	PCN 6			PGTW
15	190300 190522	9.4N 144.9E	PCN 6	T2.0/2.0 /D0.5/24HRS		PGTW
16 17	190522	9.5N 144.4E 9.5N 144.3E	PCN 5 PCN 6			PGTW
18	190900	10.0N 144.2E	PCN 6			PGTW
19	191200	10.5N 144.1E	PCN 6			PGTW PGTW
20	191600	10.6N 143.1E	PCN 6			PGTU
21	191888	10.6N 142.7E	PCN 6			PGTIJ
22	192100	11.6N 142.2E	PCN 6			PGTW
23	200000	11.5N 142.4E	PCN 6			PGTW
24	200300	11.9N 141.7E	PCN 6	T3.5/3.5 /D1.5/24HRS		PGT₩
25	200510	12.2N 141.1E	PCN 5			PGTW
26	200600	12.3N 140.9E	PCN 2			PGTW
27	200900	12.5N 140.7E	PCN 6			PGTW
	201200	12.8N 140.2E	PCN 6			PGTW
29 30	201600 201800	13.3N 139.8E 13.3N 139.2E	PCN 6			PGTW
31	202100	13.7N 139.3E	PCN 6			PGTW PGTW
32	210000	13.9N 139.0E	PCN 2			PGTW
33	210300	13.9N 138.7E	PCH 4	T4.5/4.5 /D1.0/24HR5		PGTW
34	210458	14.0N 138.5E	PCN 3	1 11 2 11 2 1 2 1 1 1 1 1 1 1 1 1 1 1 1		PGTW
35	210600	14.4N 13B.6E	PCN 4			PGTW
36	210900	15.0N 138.1E	PCN 2			PGT⊍
37	211200	15.2N 137.9E	PCN 2		EYE DIA 20NM	PGTW
38	211600	15.6N 137.6E	PCN 2			PGTW
39	211743	15.8N 137.3E	PCN 1			PGTW
40 41	212100 220000	15.8N 137.0E 16.0N 136.6E	PCN 2 PCN 2			PGTW
42	220300	16.6N 136.4E	PCN 2	T5.5/5.5 /D1.0/24HRS	•	PGTW PGTW
43	220300	16.5N 136.2E	PCN 1	10.0.0.0 / DI.O/240K3		PGTW
44	220900	17.2N 136.0E	PCN 2			PGTW
45	221200	17.5N 135.8E	PCN 2			PGTW
46	221600	18.0N 135.6E	PCN 2		EYE DIA 30NM	PGTW
47	221730	18.3N 135.4E	PCN 1		EYE DIA 40NM	PGT₩
48	222100	18.8N 135.2E	PCN 2		EYE DIA 35NM	PGTW
49	230000	19.2N 135.0E	PCN 2	T6.5/6.5 /D1.0/21HRS		PGTW
50	230300	19.7N 134.7E	PCN 2			PGTW
51 52	230615	20.3N 134.5E	PCN 1			PGTU
52 53	230900 231200	20.8N 134.4E 21.3N 134.1E	PCN 2			PGTU
53 54	231200	21.3N 134.1E 21.8N 133.6E	PCN 2 PCN 2			PGTW
55	231800	22.3N 133.3E	PCN 2			PGTW PGTW
56	231900	22.2N 133.4E	PCN 1			PGTW
57	231900	22.2N 133.5E	PCN I			RP/1K
58	232100	22.6N 133.0E	PCN 2			PGTW
59	240000	23.0N 132.8E	PCN 2	T6.0/6.5 /W0.5/24HRS		PGT⊎

	ca	240700	22 24 122 55				
	60	240300	23.2N 132.6E	PCH 2			PGT⊎
	61	240603	23.7N 132.5E	PCN 1			PGTW
	62	240900	24.2N 132.2E	PCN 2			PGT⊎
	63	241200	24.6N 132.2E	PCN 2			PGTW
	64	241600	25.2N 131.9E	PCN 2			PGTW
	65	241800	25.5N 131.9E	PCN 2			PGTW
	6 6	241848	25.3N 132.0E	PCH 1			RPMK
	67	250000	26.2N 131.1E	PCN 2	T5.0/5.5 /U1.0/24HRS	EYE DIA 10NM	PGTW
	68	250300	26.6N 131.0E	PCN 4		ULCC FIX	PGTW
	69	250551	26.9N 130.9E	PCN 1			PGTW
	70	250908	27.5N 130.7E	PCN 4			PGTW
	71	251200	27.6N 130.4E	PCN 4			PGTW
	72	251600	27.9N 130.6E	PCN 4			PGTU
	73	251836	28.1N 130.7E	PCN 3			PSTW
	74	252100	28.5N 130.8E	PCN 4			PGTW
	75	260000	28.8N 130.5E	PCN 4	T4.0/4.5 /W1.0/24HRS		PGTW
	76	260300	29.3N 130.6E	PCN 4	14:0/4:5 /WI:0/24/K3		PGTW
	77	260539	29.9N 131.1E	PCN 3			
	78	260900	30.3N 130.9E	PCN 2			PGTW
	79	261200	30.7N 131.2E	PCN 4			PGTU
	80	261600	31.5N 131.5E	PCN 4			PGTW
	81	261824	31.8N 131.5E	PCN 3			PGT₩
	82	262100	32.5N 132.3E	PCN 6			PGTW
	83	270000			T7 0 2 F 411 0 0 4100		PGTW
			33.8N 131.9E	PCN 6	T3.0/3.5 /W1.0/24HRS		PGTW
	84	270300	34.9N 132.0E	PCN 6			PGTW
	85	270600	36.5N 132.4E	PCN 6			PGTW
ж	86	270900	27.9N 132.4E	PCH 6			PGT₩
	87	271200	38.4N 131.8E	PCN 6			PGTW

FIX NO.	TIME (Z)	F1X POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SE VEL/BR					-WND ∕RNG	ACC NAV		EYE SHAPE		DRIEN- TATION		TEMP (C) I/ DP/SST	MSN NO.
1	180402	8.3N 150.6E	1500FT		1003	20 15	0 60					15	15				+23 +23	,	
ž	191108	10.2N 144.4E	700MB	3055	1002	20		898	53	050	60	10	8				+11 +10		1 7
3	191852	11.1N 142.8E	700MB	2970				939		300		10	5				*11 TIE	410	3
4	192124	11.2N 142.4E	788MB	2965	987	65 05	0 30			050		8	3				+10 +14		4
5	200600	12.2N 141.2E	700MB	2935		55 06				030	49	ĕ	4				410 TI		=
6	200858	12.2N 140.BE	700MB	2925	981	30 24				150	30	6	5				+14 +15	±10	5
7	201958	13.3N 139.4E	700MB	2876						,		10	12				.14 .13		š
8	202053	13.3N 139.3E	700MB	2847	971	55 08	0 74	169	56	070	60	10	10				+12 +15	i	6
9	210722	14.5N 138.2E	700MB	2794	965	68 98	0 30	060	84	320	43	8	1					•	7
10	210903	14.6N 138.0E	700MB	2757		50 33	0 90	278	67	170	60	8	2	CIRCULAR	38		+14 +17	+18	7
11	211801	15.8N 137.1E	700MB	2689				170	91	100	30	10	0 8						8
12	212050	15.BN 136.9E	700MB	2659	950	100 09	0 20	330	98	250	30	10	8	CIRCULAR	48		+12 +16	i	Ř
13	220686	16.7N 136.2E	700MB	2491		75 36	9 108	260	105	120	20	7	3	ELLIPTICAL	40 38	090	+12 +22		10
14	220859	17.0N 136.0E	700MB	2445	926			270	97	180	20	6	5	CIRCULAR	38		+13 +21		10
15	222153	10.8N 135.2E	700MB	2331		75 30	9 8	150	101	020	22	3	2	CIRCULAR	30		+10 +25		ii
16	230112	19.5N 134.8E	709MB	2366		115 31	0 15	310	112	210	20	3	1	CIRCULAR	30		+17 +24		11
17	230612	20.3N 134.3E	700MB	2381	928	100 27	0 15	218	112	130	38	5	2				+22	+15	12
18	230845	20.8N 134.3E	700MB	2901		120 21	0 20	260	105	260	15	5	5	CIRCULAR	30		+15 +21	+13	12
19	240708	23.8N 132.2E	780MB	2536				210	81	130	30	5	5						14
20	240835	24.0N 132.2E	700MB	2538	937			290	85	220	25	5	5	CIRCULAR	40		+14 +15	+15	14
21	242211	25.8N 131.1E	700MB	2631		65 25		248	84	140	71	1	5				+17 +28	+15	15
22	250840	27.1N 130.5E	700MB	2615	946	65 13	0 120	220			100	Θ	15	CIRCULAR	36		+15 +15	i	16
23	252151	28.7N 130.6E	700MB	2698				120	78	040	90	2	5	CIRCULAR	30		+17 +18	+15	17
24	260833	30.0N 130.8E	780MB	2680		50 09	9 169	180	68	090	100	8	3				+17 +18	1	18

RADAR FIXES

	TIME (Z)	F1X POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB- ASWAR			COMMENTS	RADAR POSITION		SITE WMO NO.
1							35/04				26.1N 127		47937
2	250000 250100	26.2N 131.0E	LAND				35//3 249/4				26.1N 127 28.4N 129		47937 47909
3	250100	26.3N 131.1E 26.3N 131.1E	LAND				25//5				26.4N 127		47937
5	250200	26.4H 131.1E	LAND				249/4	53311			28.4H 129		47909
6	250200	26.4N 131.1E	LAND				65/45	73606			26.1N 127		47937
7	250300	26.5N 131.0E	LAND				22914	53408			28.4N 129		47909
8	250300 250400	26.5N 130.9E 26.7N 131.0E	LAND LAND				20913 24914	73446			26.1N 127 28.4N 129		47937 479 8 9
	250400	26.7N 130.9E	LAND				55914	735071			26.1N 127	7.7F	47937
11		26.9N 131.0E	LAND				24914	53613		•	28.4N 129	9.5E	47989
12	250500	26.9N 130.8E	LAND				65//7				26.1H 127	7.7E	47937
13		27.8N 130.8E	LAND				22973				28.4H 129		47909
14 15		26.9N 130.8E 27.1N 130.7E	LAND LAND				20972 22913				26.1H 127 28.4H 129		47937 4 79 09
16		27.3N 130.8E	LAND				20913				26.1N 127	7.7E	47937
17	251000	27.2N 130.4E	LAND				22913	53105			28.4N 129	9.5E	47909
18	251000	27.2N 130.5E	LAND				21913				26.1N 127		47937
19 20	251200 251200	27.2N 130.5E	LAND LAND				22913 2///3	72607			28.4N 129 26.1N 127	3.3E 2 7E	47909 47937
21		27.2N 130.4E 27.3N 130.4E	LAND				22913				28.4H 129		47909
22	251300	27.3N 130.5E	LAND				35913	50507			26.1N 127	7.7E	47937
		27.4N 130.5E	LAND				22913				28.4H 129		47909
		27.4N 130.5E	LAND				35//3 22913	53408			26.1N 127 28.4N 129	7.7E	47937 47989
25 26		27.5N 130.6E 27.5N 130.6E	LAND				35//3	70306			26.1N 127	7.7E	47937
27		27.7N 130.6E	LAND				22913	53613			28.4N 129	9.5E	47909
28	251600	27.8N 130.6E	LAND				5///3	53619			26.1N 127	7.7E	47937
29		27.9N 130.6E	LAND				22913	53613			28.4N 129		47909
30		28.1N 130.5E	LAND				22913 22813				26.1N 127 26.1N 127	7.7E 7.7E	47909 47909
31 32	251900	28.2N 130.5E 28.9N 130.6E	LAND LAND				54912	53508			30.6N 131		47869
33	260000	28.9N 130.6E	LAND				2291/	53208			26.IN 127	7.7E	47909
34	261199	30.4N 131.1E	LAND				20542	60411			33.4N 130		47806
35	261100	30.4N 131.1E	LAND				10472				30.6N 131 33.4N 136		47869 47806
36 37	261300 261300	30.7N 131.2E 30.7N 131.3E	LAND LAND				20512 11432				30.6N 131		47869
3f		30.9N 131.3E	LAND	FAIR		30	11-32	30200			32.1N 131		47854
39	261400	31.0N 131.3E	LAND				12612				30.6N 131	1.00	47869
40		30.9N 131.3E	LAND				20512				33.4N 138 38.6N 131	8.3E	478 0 6 47869
41 42		31.2N 131.4E 31.2N 131.3E	LAND				10512 20772				33.4N 136	8 3E	47806
42		31.3N 131.3E	LAND	GOOD		30	20112	00123	MOVG	3525	32.1H 131		47854
44	261600	31.4N 131.3E	LAND				10573				33.4N 136	0.3E	47806
45	261600	31.5N 131.4E	LAND				11512	50116			30.6N 131	1.0E	47869
46 47	261655	31.6N 131.3E	LAND LAND	GOOD		20	10422	57C11	MOVG	3620	32.1N 131 30.6N 131	I.DE	47854 47869
48	261700 261700	31.6N 131.4E 31.7N 131.3E	LAND				10573				33.4N 136	0.3E	47806
49	261755	31.8N 131.5E	LAND	POOR		5			MOVG	0330	32.IN 131	1.5E	47854
50	261800	31.9N 131.5E	LAND				255/2				34.3N 132		47792
51	261800	31.9N 131.5E	LAND				10423 54542				33.4N 138 30.6N 131		47806 47869
52 53	261800 261800	31.8N 131.6E 31.9N 131.4E	LAND				2////	////			33.3N 134		47869
54		32.0N 131.7E	LAND	FAIR		8			MOVG	0325	32.1N 13	1.5E	47854
55	261900	32.1N 131.7E	LAND				21443				33.4N 139	0.3E	47806
56	261900	32.1N 131.8E	LAND				10312				30.6N 13	1.0E	47869
57 58	261900 261900	32.1N 131.5E 32.1N 131.6E	LAND				5//// 25512				33.3N 134 34.3N 132		47899 47792
59	261955	32.3N 131.8E	LAND	FAIR		10	23312	-0111	MOVG	9135	32.1N 13		4785-
60	270600	35.7N 132.0E	LAND				55//2	53627			35.5N 133	3.1E	47791
61	270700	36.2N 131.8E	LAND				65//3	53430			35.5N 133	3.1E	47791
62 63	270800 270900	36.5N 131.8E 37.1N 131.8E	LAND LAND				65//2 65//2	53622			35.5N 133	5.1E 2 15	47791 47791
		37.1N 131.8E	LAND				65//2				35.5N 133		47791
						SYNOPT	IC FIXE	:5					
FIV	TIME	FIX	INTER	SITY NEA	PECT								
	(Z)	POSITION	ESTIM		A (NM)		co	MMENTS					

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

WMD 47835 WMD 47815 WMD 47755

1 261888 31.8N 131.6E 2 262188 32.4N 132.8E 3 270388 34.2N 132.8E

	BEST TRACK	WARN ING	24 HOUR ERRECOST	40 HOUR PORTOGOT	vous
		ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS
MO/DA/HR 082000Z		POSIT WIND DST WIND			POSIT WIND DST WIND
082006Z		0.0 0.0 00. 0. 0.0 0.0 0.0 0.0 0.0 0.0 0.0 0	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 0. -0. 0.	0.0 0.0 00. 0.
0820122		0.0 6.0 00. 0.	0.0 0.0 00. E.	0.0 0.0 00. 0. 0.0 0.0 60. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
082018Z		0.0 0.0 00. 0.		0.0 0.0 60. 0.	0.0 0.0 00. 0.
082100Z	12.1 121.0 39 1	2.2 120.2 25. 475.	12.5 117.4 30. 13215.	13.3 114.2 35. 27240.	15.0 111.6 35. 45850.
082 106Z	12.2 120.3 35 1	2.0 119.2 25. 6610.	12.2 115.7 30, 223, -25,	13.6 111.8 35. 40845.	15.8 108.2 30, 669, -60.
Ø82112Z		2.7 118.9 30. 535.		13.8 112.1 45. 39040.	15.4 108.5 35. 64950.
082118Z		2.6 118.4 30. 6410.		13.3 112.8 45. 36340.	14.3 109.5 35. 60440.
082200Z 082206Z		2.3 118.6 30. 6115.		12.6 113.5 58. 34235.	13.2 110.3 35. 62130.
082212Z		2.3 119.3 35. 1320. 2.4 119.2 55. 610.	12.8 118.1 45. 3735. 13.2 117.6 70. 6915.	13.3 115.3 55. 25535. 13.3 114.8 75. 30310.	14.0 112.2 50. 5055. 14.1 111.6 75. 560. 25.
082218Z		2.6 119.0 60. 810.		13.3 114.6 75. 348. 0.	14.1 111.6 75. 560. 25. 13.9 112.2 70. 566. 20.
0823002		2.7 118.7 70. 85.	13.3 116.2 75, 181, -10.	14.2 113.1 78. 448. 5.	15.1 109.8 55. 672. 10.
082306Z		2.8 118.4 70. 2110.	13.8 116.8 75. 16415.	14.9 114.2 70. 378. 15.	15.9 111.0 60. 646. 20.
082312Z		2.8 118.8 80. 65.	13.2 117.2 75. 18110.	13.9 114.9 70. 420. 20.	15.0 112.2 65. 666. 25.
082318Z		2.8 118.8 88. 135.	13.3 117.4 75. 209. 0.	14.2 115.1 70, 428, 20.	15.5 112.5 65. 692. 30.
082400Z		3.3 119.5 80. 135.	14.9 119.8 90. 140. 25.	16.1 117.6 100. 272. 55.	16.5 114.9 115. 606. 85.
082406Z		4.1 119.6 88. 818.	16.8 117.8 95. 142. 40.	18.2 114.8 105. 391. 65.	18.6 111.6 115. 786. 98.
0824122		4.8 119.8 80. 135.	17.0 119.0 80. 131. 30.	18.7 116.7 85. 329. 45.	19.9 114.2 85. 682. 55.
082419Z 082500Z		5.9 119.8 80. 0. 5. 7.1 120.2 80. 6. 15.	18.8 118.9 80. 82. 30. 20.2 119.1 75. 84. 30.	19.9 116.2 80. 388. 45. 20.7 115.8 75. 463. 45.	20.4 112.3 80. 856. 50.
082506Z		8.2 120.2 80. 23. 25.		21.8 116.3 69. 485. 35.	20.6 111.5 75. 999. 40. 22.5 113.7 50. 936. 0.
0825122		8.8 119.7 50. 17. 0.	21.6 118.0 60. 219. 20.	23.2 116.8 40. 553. 10.	8.0 0.0 d0. 0.
082519Z		9.5 120.0 55. 13. 5.	22.1 120.0 60. 166. 25.	24.5 120.2 40. 405. 10.	27.5 121.7 25. 50545.
082600Z		9.8 120.4 55. 8. 10.		24.4 126.3 65. 168. 30.	27.2 129.0 70. 249. 0.
082606Z		0.6 121.3 55. 12. 15.	22.5 124.4 60. 34. 35.	24.8 126.9 70. 206. 20.	27.6 129.2 75. 254. 5.
Ø82612Z		1.1 122.1 48. 13. 0.		26.2 128.1 40. 22025.	29.8 129.9 50. 35220.
082618Z 082700Z		1.7 123.0 35. 13. 0. 1.8 124.0 35. 0. 5.	24.0 126.4 30. 81. 0. 24.0 127.2 30. 1145.	26.9 128.5 48. 24530.	30.7 130.2 50. 41510.
082706Z		1.8 124.0 35. 0. 5. 2.2 125.0 35. 12. 10.	24.0 127.2 30. 1145. 0.0 0.0 00. 0.	27.1 129.2 25. 23745. 0.0 0.0 60. 0.	9.9 0.0 00. 0. 9.0 0.0 00. 0.
082712Z		0.0 0.0 00. 0.	8.0 0.0 08. 0.	0.0 0.0 60. 0.	0.0 0.0 00. 0.
082718Z		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 6.0 00. 0.
Ø828ØØZ	23.5 129.2 35 1	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 60. 0.	0.0 6.0 00. 0.
082806Z		4.2 130.8 35. 1215.	26.9 135.7 50. 22920.	30.2 139.6 58. 588. 5.	34.2 142.5 50. 887. 20.
Ø82812Z		4.7 131.7 60. 325.	28.3 135.0 70. 283. 0.	36.6 138.8 4 5. 893. 5.	0.0 0.0 CO. O.
082818Z		4.6 132.2 60. 2910.	27.6 135.4 65. 280. 5.	33.8 137.9 55. 719. 15.	0.0 0.0 00. 0.
082900Z 082906Z		4.2 132.3 65. 65. 4.5 132.8 65. 225.	25.2 134.4 60. 167. 10. 25.6 134.9 60. 218. 15.	27.7 136.5 50. 389. 15.	33.3 139.1 35. 796. 10.
082912Z		4.2 132.2 65. 65.	25.6 134.9 60. 218. 15. 24.3 133.1 60. 106. 20.	28.2 136.8 50. 425. 20. 25.6 135.2 50. 273. 20.	33.8 139.2 35. 856. 15. 29.7 138.2 30. 696. 10.
Ø82918Z		4.2 132.2 65. 13. 5.	24.6 133.3 55. 120. 15.	25.8 135.4 45. 316. 20.	0.0 8.0 00. 0.
083000Z		3.8 131.9 45. 125.	23.4 133.1 35. 80. 0.	24.3 136.1 25. 366. 0.	9.0 8.0 00. 0.
083006Z		3.3 131.8 45. 0. 0.	22.6 132.3 35. 43. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0 83012Z		2.9 131.8 40. 6. 0.	22.2 133.4 30. 136. 0.	9.0 9.8 69. 9.	0.0 6.6 60. 6.
0830182		2.8 132.1 40. 13. 0.	22.8 134.1 30. 199. 5.	0.0 0.0 00. 0.	0.0 0.0 00. O.
003100Z		2.7 131.9 40. 8. 5.	22.1 132.3 25. 159. 0.	0.0 0.6 60. 0.	0.0 0.0 00. 0.
003106Z 003112Z		2.9 131.8 35. 11. 5. 2.9 131.2 30. 8. 0.	22.6 131.5 25. 156. 5. 22.7 130.1 20. 127. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	9.9 9.0 90. 9.
0031122 003118Z		2.5 131.2 36. 8. 6. 3.1 130.4 30. 8. 5.	0.0 0.0 08. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.6 00. 0. 0.0 0.0 00. 0.
090100Z		2.9 128.3 25. 72. 8.	23.4 124.4 28. 765.	8.8 8.8 88. 9.	0.0 0.0 00. 8. 0.0 0.8 00. 0.
090106Z		3.1 128.8 25. 13. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. B.
0901122	22.8 127.8 20 23	3.0 128.1 25. 20. 5.	22.8 125.1 25. 965.	8.8 8.8 88. 8.	0.0 0.0 00. 8.
090118Z		2.9 127.2 25. 23. 0.	0.0 0.0 00. 0.	0.0 0.8 00. 0.	0.0 8.0 00. 0.
0902002		3.0 125.8 25. 6. 0 .	0.0 0.0 00. 0.	0.0 0.0 OO. O.	0.0 0.8 00. 0.
090206Z		3.0 124.3 25. 20. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 6.6 00. 0.
090212Z 090218Z		2.4 123.2 25. 135. 2.2 122.3 25. 85.	8.0 9.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
090300Z		2.2 122.3 25. 85. 1.6 121.2 20. 65.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
090306Z		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHO	ONS WHI	S WHILE OVER		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	18.	142.	384.	639.	17.	158.	376.	584.	
AVG RIGHT ANGLE ERROR	8.	89.	273.	445.	9.	109.	298.	422.	
AVG INTENSITY MAGNITUDE ERROR	6.	15.	26.	30.	7.	19.	28.	26.	
AVG INTENSITY BIAS	-2.	3.	5.	7.	-3.	2.	1.	-7.	
NUMBER OF FORECASTS	50	41	33	27	35	29	25	19	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2454. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

TYPHOON FAYE FIX POSITIONS FOR CYCLONE NO. 15

F1X NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	CDITENTS	SITE
* 1	200000	11.2N 122.7E	PCN 6			PGTW
* 2	200300	11.3N 122.3E	PCN 6	T1.0/1.0	INIT OBS	PGTU
3	200600 200652	11.6N 123.4E 11.6N 123.7E	PCN 6 PCN 5	T1.5/1.5	INIT OBS	PGTW RPMK
5	200652	11.6N 123.8E	PCN 5	T1.8/1.0	INIT OBS	RODN
6 7	200900 201200	11.7N 123.0E 11.9N 122.7E	PCN 6 PCN 6			FGTW PGTW
8	201600	12.2N 121.8E	PCN 6			PGTW
* 9 * 10	201800 201937	12.5N 120.7E 11.8N 119.5E	PCH 6 PCH 5			PGTW RPMK
11	202100	12.5N 120.6E	PCN 6			PGTU
	210000 210300	12.1N 120.4E 12.0N 119.6E	PCN 6 PCN 6	T2.0/2.0 /D1.0/24HRS		PGTW PGTW
	210600	12.3N 119.9E	PCN 6			PGTW
		12.8N 119.4E	PCN 5 PCN 6	T2.0/2.0 /D0.5/21HRS		RPMK PGTW
	210900 211200	12.7N 119.7E 12.7N 118.6E	PCN 6		ULCC FIX	PGTW
	211600	12.4H 118.6E	PCN 6		ULCC FIX	PGTW PGTW
	211800 211925	12.4N 118.5E 11.8N 119.4E	PCN 6 PCN 5		÷	RODH
21	212100	12.1N 119.1E	PCN 6		BRKS CONTINUITY	PGTW PGTW
	220000 220300	12.1N 119.4E 12.2N 119.6E	PCN 6 PCN 6	T3.0/3.0 /D1.0/24HRS		PGTW
24	220627	12.2N 119.6E	PCN 3			PGTW RPMK
25 26	220627 220900	12.1N 119.5E	PCN 3 PCN 4	T3.0/3.0+/D1.0/24HRS		PGTW
27	221200	12.6N 119.4E	PCN 2		EYE OPEN N	PGTW
28 29	221600 221800	12.6N 119.2E 12.7N 119.0E	PCN 2 PCN 2		EYE DIA 20NM	PGTW PGTW
30	221912	12.8N 119.1E	PCN 3			RPMK
31 32	222100 230000	12.7N 118.9E 12.7N 118.9E	PCN 2 PCN 2	T4.0/4.0 /D1.0/21HRS	EYE OPEN N	PGTW PGTW
33	230300	12.8N 118.6E	PCN 2	14,0,4,0 ,21,0,21,10		PGTW
34 35	230615 230615	12.7N 118.7E 12.5N 118.6E	PCN 1 PCN 1	T4.5/4.5 /D1.5/24HRS		PGTW RPMK
36	230615	12.4N 118.7E	PCN 1	T4.5/4.5+/D1.5/24HRS	EYE DIA 20NM	RODN
37 38	230900	12.7N 118.6E 12.8N 118.8E	PCN 2			PGTW PGTW
39	231200 231600	12.9N 118.9E	PCN 2 PCN 2			PGT₩
40 41	231751 231800	13.0N 118.8E	PCN 2 PCN 2			RPMK PGTW
42	231900	13.0N 118.9E 13.0N 119.1E	PCN 1			PGTU
43	232100	13.1N 119.1E	PCN 2 PCN 2	T4.0/4.0 /S0.0/24HRS		PGTW PGTW
44 45	240000 240300	13.3N 119.3E 13.7N 119.6E	PCN 2	14.074.0 730.0724113		PGTU
46	240603	14.1N 119.6E	PCN 1 PCN 1	T5.0/5.0 /D0.5/24HRS		rpmk Pgtw
47 48	240603 240900	14.2N 119.5E 14.6N 119.7E	PCN 2			PGT₩
49 E0	241200	15.2N 119.7E	PCN 2 PCN 2		EYE OPEN W	PGTW PGTW
50 51	241600 241800	15.9N 119.6E 16.3N 119.4E	PCN 6			PGTW
52 53	241848	16.0N 119.6E 16.9N 119.4E	PCN 3 PCN 6			RFMK PGTW
54	242100 250000	17.1N 120.1E	PCN 6	73.5/4.0 /W0.5/24HRS		PGT₩
55	250300	17.6N 120.1E 17.8N 119.9E	PCN 6	77 E /A E + A II E /2/LUBC		PGTW RPMK
56 57	25055 I 25055 I	18.2N 119.7E	PCH 3	T3.5/4.5+/WI.5/24HRS		PGTW
58 58	250900 251200	18.6N 119.6E	PCN 6			PGTW PGTW
59 60	251600	19.0N 119.5E 19.2N 119.8E	PCN 6			PGTW
61	251836	19.5N 120.0E	PCN 3 PCN 5			rpmk Pgtw
62 63	251836 252100	19.5N 119.9E 19.4N 120.1E	PCN 5			PGTW
64	260000	19.7N 120.6E	PCN 4	T2.5/3.0 /W1.0/24HRS		PGTW
65 66	260300 260539	20.0N 120.8E 20.2N 121.4E	PCN 4 PCN 3	T3.0/3.5 /W0.5/24HRS		PGTW RPi1K
67	260539	20.4N 121.4E	PCN 3		BASED ON EXTRAP	PGTW PGTW
		20.7N 121.5E 21.1N 121.6E	PCN 6 PCN 6			PGTW
70	261600	21.3N 122.2E	PCN 6			PGTW
		21.6N 122.7E 21.4N 122.5E	PCN 3 PCN 6			rpmk Pgtu
73	262100	21.5N 123.1E	PCN 6	TO E /O E /O B A A 4100		PGTW
		22.0N 123.8E 22.0N 124.5E	PCN 6 PCN 6	T2.5/2.5 /S0.0/24HRS		PGTW PGTW
76	278686	22.8N 125.7E	PCN 6			PGTW
77 78	271200 271890	23.0N 126.7E 22.8N 127.0E	PCN 6 PCN 4			PGTW PGTW
79	271811	22.6N 127.2E	PCN 3		ווו הפי בזיט	PGTW
		23.2N 128.5E 23.6N 129.5E	PCN 6 PCN 4	T2.5/2.5+/SB.0/24HRS	ULCC FIX	PGTW PGTW
82	280300	24.1N 130.2E	PCN 6	+		PGTW
		24.1N 130.4E 24.2N 130.6E	PCN 4 PCN 4			PGTW PGTW
04						

85	280900	24.3N 131.1E	PCN 2			PGTW
86	281200	24.1N 131.5E	PCN 2			PETU
87	281600	24.5N 131.7E	PCN 2			PGTW
88	281860	24.4N 132.0E	PCN 6			PGTU
89	282106	24.4N 132.2E	PCN 6			PGTW
98	290000	24.4N 132.3E	PCN 4			PGTW
91	290300	24.6N 132.5E	PCN 6	T4.0/4.0-/D1.5/27HRS		PGTW
92	290503	24.6N 132.5E	PCN 3			PGTW
93	290600	24.5N 132.2E	PCN 4			PGTW
94	290900	24.6N 132.3E	PCH 4			PGTW
95	291600	24.3N 132.3E	PCN 2			PGTW
96	291748	24.3N 132.3E	PCN 4		BASED ON EXTRAP	PGTW
97	292100	24.0N 132.0E	PCN 4		EXP LLCC	PGTW
98	300000	23.7N 131.9E	PCN 4		EA ELLE	PGTW
99	300300	23.5N 131.9E	PCH 4	T2.5/3.0 /W1.5/24HRS		
100	300451	23.5N 131.8E	PCN 3	12.5/5.0 /WI.5/24/R5		PGTW
101	300600	23.4N 131.8E	PCH 4			PGTU
102	300900	23.3N 131.7E	PCN 4			PGTU
103	301200	23.0N 131.0E	PCN 4		EXP LLCC	PGTW
184	301600	22.9N 132.0E	PCN 4			PGTW
105	301736	23.0N 132.0E	PCN 3		EXP LLCC	PGTW
106	302100	23.0N 132.0E	PCN 4		EXP LLCC	PGTW
107	310000	22.8N 131.8E	PCN 4		EXP LLCC	PGTW
108	310300	22.9N 131.7E	PCN 4	T1 0 0 0 411 0 0 4100		PGTW
109	310620			T1.0/2.0 /U1.0/24HRS		PGTW
118		23.0N 131.6E	PCN 3			PGTW
	310900 311200	23.0N 131.5E	PCN 6			PGTW
111		22.9N 131.3E	PCN 4			PGTW
112	311600	23.1N 130.6E	PCN 6			PGTW
113	311800	23.1N 130.4E	PCN 4			PGT⊎
114	311905	23.0N 130.4E	PCN 3			RODN
115	312100	22.9N 130.0E	PCN 4			PGT₩
116	910008	23.0N 129.7E	PCN 4			PGTW
117	010300	23.0N 129.2E	PCN 4	T1.0/1.0 /W1.0/24HR\$		PGTW
118	010600	22.9N 128.9E	PCN 3			PGTW
119	010900	23.0N 128.6E	PCN 4			PGTW
120	011200	23.0N 125.9E	PCN 4			PGTW
121	011200	22.BN 127.8E	PCN 4			PGTW
122	011000	23.0N 127.1E	PCH 4			PGTW
123	011835	23.0N 126.5E	PCN 3			PGTU
124	020000	22.9N 125.8E	PCN 4			PGTW
125	020300	22.8N 125.1E	PCN 3	T1.0/1.0 /S0.0/24HRS	EXP LLCC	PGTW
126	020556	22.5N 124.6E	PCN 3		EXP LLCC	PGTW
127	020900	22.6N 123.8E	PCN 6			PGTW
128	021200	22.5N 123.4E	PCN 6			PGTIJ
129	021600	22.4N 122.8E	PCN 6			PGTW
130	021800	22.2N 122.3E	PCN 6			PGTW
131	021841	21.9N 122.2E	PCN 5			PGTW
132	922199	21.5N 121.7E	PCN 6			PGTW
133	030000	21.5N 121.1E	PCN 6		BASED ON EXTRAP	PGTW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC- VEL/BRG/			-FLT- VEL/			ACC NAV		EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) DUT/ IN/ DP/SST	MSN NO.
1	221032	12.3N 119.4E	700MB	2965	984	60 170	18	268	80	170	18	3	2	C IRCULAR	18	+12 + 8	1
2	221200	12.3N 119.2E	700MB	2938				300	55	200	20	3	2	C IRCULAR	15	+12 +30 + 9	1
3	222024	12.6N 119.0E	700MB	2841				140	68	030	10	4	3			+14 +17 + 7	2
4	222259	12.7N 118.7E	700MB	2841	971	50 130	8	208	73	130	10	6	3	CIRCULAR	25	+11 +15 + 8	2
5	230758	12.6N 118.7E	708MB	2746		65 270	5	010	105	270	10	5	2	ELL IPTICAL	25 15 060	+11 +18 +11	3
6	230953	12.8N 118.6E	700MB	2745	963	65 150	30	220	100	140	8	5	3	CIRCULAR	15	+12 +16 +10	3
7	232032	13.0N 119.3E	700MB	2746				030	77	320	18	10	3	CIRCULAR	25	+14 +10	4
8	240706	14.2N 119.7E	700MB	2739		80 010	10	100	95	010	10	2	1				5
9	240907	14.4N 119.7E	700MB	2743	963	80 050	8					2	1	ELL IPTICAL	28 15 340	+18 + 9	5
10	250751	18.3N 119.8E	700MB	2990		48 030	8	248	37	170	8	4	3			+15 + 9	7
11	252303	19.7N 120.5E	700MB	2992	987	70 140	15	240	47	148	15	15	2			+10 +18 + 8	ė
12	260718	20.7N 121.4E	700MB	3035		40 090	30	160	41	09 2	25	10	5				9
13	261006	20.9N 121.8E	700MB	3044	997	40 350	25	060	36	020	13	5	5			+14 +10	9
14	262237	21.6N 123.7E	780MB	3078	998	39 210	30	220	43	050	30	3	1	CIRCULAR	25	+16 +17	18
15	270701	22.7N 125.2E	700MB			15 270	30	350	19	270	30	20	20				11
16	281935	24.2N 132.0E	788MB	2895				360	69	300	5	6	5				12
17	282222	24.2N 132.1E	700MB	2898	979	70 290	5	290		249	10	5	5	CIRCULAR	12	+11 +15 +10	12
18	291042	24.0N 132.1E	700MB	2941	982		-	030		310	30	10	3	CIRCULAR	13	+13 +21	14
19	291153	24. IN 132. IE	700MB	2960				020		270	9	10	3				14
20	292326	23.7N 132.0E	700MB	3029		50 200	30	280		200	30	3	10			+11 +17 + 8	15
21	300753	23.2N 131.BE	1500FT		996	40 010	20	978		369	20	ĕ	5				16
22	300929	23.1N 131.8E	1500FT		997	40 240	15	928		240	10	8	6			+23 +27 +25 27	16
23	302028	23.0N 132.0E	700MB	3060	•••	-10 2-10	••	260		140	58	2	7			123 121 123 21	17
24	302148	22.8N 131.8E	1500FT		996	40 278	25	358		270	18	2	4			+24 +26 +24 30	17
25	310738	23.0N 131.5E	1500FT		999	35 090	15	138		010	105	10	2				18
26	310907	23.0N 131.4E	1500FT		999	30 150	15	139		060	30	15	5			+23 +25 +25	16
27	312143	23.0N 129.BE	1500FT		997	25 898	5	030		696	5	- 6	3			+25 +27 +26 27	19
					231	20 000	,	030	-1	000	3	0	J			TES TEI TEO EI	13

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	POTOR	ACURY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TODEF	COMMENTS	RADAR POSITION	SITE WNO NO.
		. 001/10//	KIIDIIK		_		MJWHI 12211	COLLENIS	10311100	wild no.
1	232200	13.3N 119.6E					10571 52105		14.8N 120.2E	98426
2	232300	13.3N 119.6E					20511 50307		14.8N 120.2E	98426
3	240100	13.6N 119.4E					1151/ 50006		14.8N 120.2E	98426
4	240200	13.7N 119.4E					1142/ 50107		14.8N 120.2E	98426
5	240300	13.8N 119.4E					1048/ 70207	BEST TRACK 015 DEG 07 KTS	14.BN 120.2E	98426
* 6	240400	13.4H 119.7E					1081/ 43605	EYE BO PCT CIR OPEN SE	16.3N 120.6E	98321
. 7	240400	13.9N 119.5E					1141/ 80207		14.8N 120.2E	98426
* 8	248588	13.4N 119.7E					1081/ 43602	EYE 90 PCT CIR OPEN RE	16.3N 120.6E	98321
9	240600	14.1H 119.6E					1141/ 80207		14.8N 120.2E	98426
* 10	240600	13.6N 119.7E					1199/ 43605		16.3N 120.6E	98321
* 11	240630	13.6N 119.7E					10883 43604		16.3N 120.6E	98321
12	240700	14.2N 119.6E					1141/ 90207	BEST TRACK 016 DEG 07 KTS	14.8N 120.2E	98426
* 13	240700	13.7N 119.7E					10683 43605	EYE 100 PCT CIR	16.3H 120.6E	98321
* 14	240800	13.9N 119.8E					10783 40205	EYE 188 PCT CIR	16.3H 120.6E	98321
* 15	248988	14.1H 119.8E					10623 43605		16.3N 120.6E	98321
* 16	240930	14.2N 119.8E					11833 43606	EYE 90 PCT ELPTCL	16.3N 120.6E	98321
* 17	241138	14.6N 119.9E					1061/ 40106	BEST TRACK 016 DEG 07 KTS EYE 100 PCT CIR EYE 100 PCT CIR EYE 90 PCT ELPTCL EYE 100 PCT CIR DIA 11NM EYE 100 PCT CIR DIA 9NM	16.3N 120.6E	98321
18	241200	15.0N 119.8E					1141/ 80209		14.8N 120.2E	98426
* 19	241700	15.6N 119.6E					1031/ 43303	FIE 100 DOT DID DID 14414	16.3N 120.6E	98321
* 20	241930	15.9N 119.8E					1031/ 40205	EYE 100 PCT CIR DIA 11NM	16.3N 120.6E	98321
21	242030	16.1N 119.9E					1021/ 40306	EAE 100 LCI CIK DIH SUU	16.3N 120.6E	98321
22	242035	16.0N 120.2E		POOR			1021/ 40208			98327
23	242100	16.3N 120.0E		CATE	5		1021/ 40208	EYE 100 PCT CIR DIA 9NM ELIP AXIS 20/10	16.3N 120.6E 15.2N 120.6E	98321
24	242130	16.2N 120.2E		FAIR	ELL IPT ICAL		1022/ 40208	ELIP AXIS 20/10 EYE 100 PCT CIR DIA 9NM	16.3N 120.6E	98327 98321
25	242200 242230	16.7N 120.2E					1021/ 43608	EYE 100 DCT CIR DIA 9NM	16.3N 120.6E	98321
26	250000	16.8N 120.2E					1021/ 43000	EYE BO PCT CIR OPEN NHE	16.3N 120.6E	98321
27 28	250030	17.3N 120.3E 17.4N 120.4E					21985 ////	EYE ELLIPTICAL	18.3N 121.6E	98231
* 29	250030	17.6N 120.3E					4/// 43616	EIE EEEIFTIONE	16.3N 120.6E	98321
* 30	250300	18.3N 120.2E					11/// 53607		16.3N 120.6E	98321
* 31	250600	18.6N 120.1E					1061/ 43405		16.3N 120.6E	98321
32	250900	18.6N 119.7E					29714 53603		18.3N 121.6E	98231
* 33	250900	18.8N 119.7E					115// 40000		16.3N 120.6E	98321
34	251130	18.6N 120.0E			ELLIFICAL		10783 43608	EYE 100 PCT CIR DIA 9NM EYE 100 DCT CIR DIA 9NM EYE 80 PCT CIR OPEN NNE EYE ELLIPTICAL	18.3N 121.6E	98231
35	251130	18.8N 119.8E					115// 40000		16.3N 128.6E	98321
36	251330	18.8N 120.1E					40483 32702		18.3N 121.6E	98231
37	251330	19. IN 120.1E					1151/ 43607		16.3N 120.6E	98321
38	251400	18.9N 120.2E					10483 40205		18.3N 121.6E	98231
* 39	251400	19.3N 120.2E					1196/ 40108		16.3N 120.6E	98321
40	252200	19.6N 120.4E					2///1 53614		22.6N 120.2E	46744
41	261300	21.3N 121.9E					6//// 59999		22.6N 120.2E	46744

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
1	192100	11.2N 125.0E	828	919	WMD 98555	
2	210000	12.1N 121.0E	0 30	0 75	WMD 98630	
3	241100	14.8N 119.8E	989	030	WMD 98426	CUBI PT

	BEST TRACK	WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST	72 HOUR FORECAST
MO/DA/HR	POSIT WIND	POSIT WIND DST WIN		ERRORS POSIT WIND DST WIND	ERRORS
082700Z	14.6 153.8 30	14.5 153.8 30. 6. 0			POSIT WIND DST WIND
082786Z	15.5 152.5 35	15.5 152.4 35. 6. 0	19.8 148.8 65. 1185.	22.5 149.3 70. 5315. 23.8 148.7 70. 7520.	27.8 153.6 75. 326. -2 5. 27.5 150.3 70. 16830.
0827122	16.2 151.8 45	16.4 151.3 45. 31. 0	20.8 148.6 70. 1255.	24.8 149.1 70. 4325.	
0827182	17.0 151.2 55	16.7 150.6 50. 395		22.3 148.6 70. 13230.	28.3 151.1 70.22925. 25.1 149.2 70.13320.
082800Z	17.0 150.8 65	17.7 150.7 55. 810		23.2 148.6 75. 10925.	26.0 148.1 85. 82. 8.
Ø828Ø6Z	18.8.150.6 70	18.5 150.3 60. 2510		24.7 149.4 80. 9320.	27.4 149.9 85. 200. 0.
0828122	19.9 150.6 75	20.0 150.7 70. 85		27.2 151.0 90. 1945.	29.6 152.8 95. 411. 10.
082818Z	21.0 150.4 80	20.8 150.3 75. 135		26.8 152.9 90. 307. 0.	28.3 157.0 90. 642. 5.
082900Z	22.2 150.2 85	22.0 150.2 60. 125		27.2 146.2 95. 44. 10.	30.1 143.1 95. 200. 5.
	23.2 149.9 90	23.2 150.2 85. 175		28.2 144.6 90, 115. 5.	31.8 142.5 98. 298. 8.
0829122	24.1 149.3 95	24.2 149.6 100. 17. 5		29.2 143.7 105. 166. 20.	34.9 142.2 98. 471. 5.
Ø82918Z	24.5 148.8 100	24.9 149.1 100. 29. 0		30.2 143.2 95. 214. 10.	38.0 143.0 75. 64318.
083000Z	25.0 148.4 100	24.9 148.3 100. 8. 0		30.4 142.2 95. 237. 5.	40.4 141.2 65. 76915.
	25.6 148.0 100	25.7 147.9 90. 810		29.1 141.9 70. 16820.	35.6 140.8 60. 48015.
	26.1 147.6 95	26.2 147.4 90. 125		30.3 141.2 70. 22215.	37.3 140.8 55. 57020.
003018Z	26.4 147.2 98	26.7 147:2 85. 185		30.0 142.3 70. 16215.	37.4 140.2 50. 55225.
003100Z	26.7 146.8 85	26.9 146.7 85. 13. 0	28.4 143.6 75. 9715.	29.2 140.2 70. 12810.	30.8 136.5 65. 19710.
083106Z	26.9 146.2 85	27.0 146.3 85. 8. 0	28.2 144.2 70. 7320.	28.9 141.2 65. 8010.	29.8 137.9 60. 8615.
Ø83112Z	27.0 145.6 85	27.2 145.8 98. 16. 5	28.2 143.9 85. 73. D.	29.0 141.4 80. 89. 5.	30.7 138.3 75. 99. 0.
083118Z	27.0 145.0 85	27.0 145.2 90. 11. 5	27.4 142.8 85, 22. 0.	28.8 140.2 80. 42. 5.	31.3 138.2 70. 1305.
090100Z	27.0 144.5 90	27.0 144.4 90. 5. 0	27.7 141.4 90. 22. 10.	30.0 139.5 85. 78. 10.	33.2 139.2 80. 176. 5.
	27.0 144.0 90	26.9 143.9 90. 8. 0		29.8 139.7 80. 39. 5.	32.8 139.2 70. 192. 0 .
	27.1 143.3 85	27.0 143.4 90. 8. 5		29.8 139.7 75. 19. 0.	32.6 139.2 55. 26315.
090118Z	27.3 142.4 85	27.2 142.7 90. 17. 5	28.5 140.6 80. 46. 5.	31.1 139.2 70. 835.	34.0 138.9 50. 36820.
	27.6 141.8 80	27.6 141.6 80. 11. 0		29.0 136.6 60. 26215.	28.9 134.0 55. 81210.
	27.6 140.9 75	27,6 140.8 75. 5. 0.		28.7 134.9 55. 45015.	29.2 132.2 50. 97515.
	27.8 140.4 75	27.7 140.5 75. 8. 0		28.7 136.0 60. 50110.	0.0 0.0 30 . 0 .
	28.2 139.8 75	28.1 139.9 75. 80		29.2 134.7 55. 66615.	0.0 0.0 00. 0.
	28.7 139.4 75	28.6 139.2 75. 12. 0		29.8 134.4 55. 76610.	8.0 9.9 9 9. 9 .
	29.2 139.4 75	29.2 138.7 70. 375		30.5 133.0 50. 89815.	0.0 0.0 0 0. 0 .
	29.5 139.6 75	29.6 139.4 75. 12. 0		0.0 0.0 00. 0.	0.0 0.0 0 0. 0.
	30.1 140.3 75	29.8 139.9 75. 28. 0		0.0 0.0 00. 0.	0.0 0.0 0 0. 0.
	30.8 141.2 75	31.0 141.2 75. 12. 0		0.0 0.0 00. 0 .	8.0 0.0 00 . 0.
	31.8 142.8 70	32.0 142.6 70. 16. 0.	39.7 148.2 45. 16320.	8.8 8.0 00. 0.	0.0 0.0 00. 0.
	32.9 144.4 70	33.0 144.9 75. 26. 5.		0.0 0.0 00. 0.	0.0 0.0 00. 0.
	34.3 146.3 70	34.3 146.4 70. 5. 0.		0.0 0.0 00. 0.	0.0 0.0 00. 0.
	35.5 148.0 65	35.5 148.2 70. 10. 5.		0.0 0.0 00. 0.	0.0 0.0 00. 0.
090506Z	37.1 149.2 65	37.1 149.6 65. 19. 0.	9.8 9.8 98. 9.	0.0 0.0 08. 0.	0.0 0.0 00. O.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72~HR	WRNG	24-HR	49-HR	72-HR		
AVG FORECAST POSIT ERROR	15.	100.	214.	364.	15.	100.	214.	364.		
AVG RIGHT ANGLE ERROR	11.	63.	101.	218.	11.	63.	101.	210.		
AVG INTENSITY MAGNITUDE ERROR	3.	11.	12.	12.	3.	11.	12.	12.		
AVG INTENSITY BIAS	-1.	-4.	-7.	-9.	-1.	-4.	-7.	-9.		
NUMBER OF FORECASTS	38	34	30	26	37	34	30	26		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2014. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

TYPHOON GORDON FIX POSITIONS FOR CYCLONE NO. 16

FIX NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMENTS	SITE
1 2 3	251800 260000	9.8N 160.8E 10.5N 159.4E	PCN 6 PCN 6	T1.0/1.0	INIT OBS	PGTW PGTW
4	260600 261200	11.7N 158.6E 12.9N 156.1E	PCN 6			PGTW PGTW
5	261642	13.2N 154.8E	PCN 5			PGTW
6 7	262100 270000	13.9N 154.2E 14.8N 153.5E	PCN 6 PCN 6			PGTW
	270300		PCN 6			PGTW PGTW
9	270345		PCN 5	T2.5/2.5 /D1.5/28HRS		PGTW
10 11	270600 270900		PCN 6 PCN 6			PGTW PGTW
12	271200	16.0N 151.5E	PCN 6			PGTW
13 14	271600 271630		PCN 6 PCN 5			PGTW
15	271800	16.7N 151.6E	PCN 6			PGTW PGTW
16 17	272100		PCN 6			PGTW
	280000 280300	17.8N 151.1E 18.2N 150.8E	PCN 6 PCN 2	T4.0/4.0 /D1.5/24HRS		PGTW PGTW
19	280600	18.8N 151.0E	PCN 2			PGT⊎
	280900 281200	19.4N 150.8E 20.0N 150.5E	PCN 5 PCN 6			PGTW PGTW
22	281600	20.5N 150.5E	PCN 6			PGTW
23 24	281618 281800	20.5N 150.4E 21.0N 150.6E	PCN 6 PCN 6			PGTW
25	282100	21.8N 150.5E	PCN 6			PGT₩ PGT₩
26	290000	22.4N 150.3E	PCN 2			PGT₩
27 28	290300 290503	22.7N 150.2E 23.1N 150.2E	PCN 2 PCN 1	75.0/5.0-/D1.0/24HRS		PGTW PGTW
29	290600	23.4N 150.0E	PCN 2			PGTW
	290900 291600	23.9N 149.8E 24.6N 149.1E	PCN 2 PCN 4			PGTW PGTW
32	291748	24.7N 148.6E	PCN 4			PGTW
33	292100		PCN 2			PGTW
	300000 300300	25.0N 148.4E 25.5N 148.4E	PCN 4 PCN 4	T3.5/4.5 /W1.5/24HRS		PGTW PGTW
	300451	25.5N 148.3E	PCN 3			PGTW
37 38	300600 300900	25.8N 148.2E 26.0N 147.9E	PCN 4 PCN 4			PGTW PGTW
39	301200	26.3N 147.8E	PCN 2			PGTW
48	301600	26.4N 147.6E	PCN 2			PGTW
41 42	301736 302100	26.4N 147.3E 26.8N 147.1E	PCN 1 PCN 2			PGTW PGTW
	310000	26.7N 146.8E	PCN 2			PGTW
	310300	27.0N 146.6E 26.8N 146.7E	PCN 2 PCN 1	T4.8/4.8 /D0.5/24HRS		PGTW PGTW
46	310600	27.1N 146.4E	PCN 2			PGTW
47 48	310900	26.9N 146.0E 27.0N 145.7E	PCN 2 PCN 2			PGTW PGTW
49	311600	26.8N 145.4E	PCN 2			PGTW
50 51		27.0N 145.2E 27.0N 144.8E	PCN 2 PCN 2			PGTW PGTW
52	010000	27.0N 144.6E	PCN 2			PGTW
53	010300	26.9N 144.3E	PCN 2	T5.0/5.0-/D1.0/24HRS		PGTU
54 55		27.0N 144.2E 27.2N 144.0E	PCN 1 PCN 2			PGTW PGTW
56	010900	26.9N 143.8E	PCN 2			PGTW
57 58		26.8N 143.3E 27.3N 142.8E	PCN 6 PCN 2			PGTW PGTW
59	011711	27.4N 142.4E	PCN 2			PSTW
68 61		27.7N 142.5E 27.6N 142.1E	PCN 2 PCN 6			PGTW PGTW
62	020000	27.5N 141.7E	PCN 4		MLCC FIX	PGTW
63 64	020414 020600	27.4N 141.0E 27.5N 140.8E	PCN 1 PCN 4	T4.0/4.5 /WI.0/25HRS	ULCC FIX	PGTW PGTW
65		27.6N 140.6E	PCN 4		ULCC FIX	PGTW
66		27.8N 140.5E	PCN 4			PGTW
67 68		28.2N 140.0E 28.4N 139.8E	PCN 4 PCN 4			PGTW PGTW
69	021041	28.4N 139.7E	PCN 3			PGTW
70 71		28.4N 139.6E 28.6N 139.5E	PCN 4 PCN 4			PGTW PGTW
72	030300	28.9N 139.2E	PCN 2		EYE OPEN SW	PGTW
73	030544		PCN 1	T4.0/4.0 /S0.0/25HRS		PGTU
74 75	030900 031200		PCN 2 PCN 4			PGTW PGTW
76	031829	30.0N 140.6E	PCN 3		ULCC FIX	PGTW
77 78	032100 040000	30.5N 140.8E 31.0N 141.2E	PCN 4 PCN 4		ULCC FIX	PGTW PGTW
79	040300	31.3N 142.8E	PCN 4			PGTW
80 81	040532 040600	31.4N 142.8E 31.4N 142.8E	PCN 3 PCN 4	T3.0/4.0 /WI.0/24HRS		PGTW PGTW
82	040900	32.3N 143.8E	PCN 6			PGTW
83	041200	33.3N 144.5E	PCN 6			PGTU

90 000900 38.0H 149.9E PCH 4 PGTW

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC VEL/BRG			FLT- VEL/					EYE SHAPE			RIEN- ATION			EMP (C) / DP/SST	MSN NO.
1 2	2623 47 271026	14.5N 153.9E 16.2N 151.8E	1500FT 700MB	2998	1001 991	30 030		150 330	34	939 259	48 20	2 15	4	CIRCULAR	18			+10	+25 +12	+12	1 2
3	272335 280705	17.7N 150.7E 18.8N 150.6E	700MB 700MB	2894 2835	977 972	50 140 75 090	30 20	300 210		180	12 30	12 10	8 5					+ 9	+13	+10	3
5	280852	19.4H 150.6E	700118	2807	312	12 636	20	160		080	25	10	- 3	CIRCULAR	25			412	+18	+12	4
6	282012	21.4N 150.2E	700MB	2676	953	80 180	8	200	85		10	5	2	CIRCULAR	30				+19		5
7	290644	23.3N 149.BE	700MB	2629	946	100 190	20	180	99	100	30	5	4	CIRCULAR	18				+18		6
8	290853	23.7N 149.7E	700MB	2612		80 320	68	949	71	320	30	10	4	CIRCULAR	20				+17		6
9	291906	24.7N 148.8E	700MB	2607		78 278	90	300	73	218	31	5	5	CIRCULAR	40				+18		7
10	300604	25.6N 147.9E	700MB	2616		50 130		259	79		35	5	5								8
11	300832	25.7N 147.9E	700MB	2612	945	65 040	120	110	80		36	5	5	CIRCULAR	30			+13	+18	+16	8
12	301800	26.4N 147.2E	700MB	2617				198	90		57	5	3			25	310		+19		9
13	302043	26.6N 147.0E	700MB	2631	947	80 270			81		80	3	3	CIRCULAR	30			+16	+17	+15	9
14	310602	27.1N 146.2E	700MB	2624		65 170		280	76		60	10	5								10
15	310833	27.0N 146.1E	700MB	2624	947	65 270	30	030	85		69	10	5	CIRCULAR.	20			+14	+16	+15	18
16	311811	26.8N 145.0E	788MB	2652	050			070	82		90	2	3								11
17 18	312057 010810	27.0N 144.7E	700MB	2661	952	CE 200		220	85		60	2	6	CIRCULAR	25				+17		11
19	011851	27.0N 143.8E 27.5N 142.3E	700MB	2657 2729	949	65 300	120	959 139	68		70	2	5	C IRCULAR	20			+18	+18	+15	12
20	012036	27.2N 141.9E	700MB 700MB	2742	960	65 310	90	969	59 67		120 69	3	3 5	C T D C III A D	••						13
21	020905	27.6N 140.8E	700MB	2748	960	55 350		100			127	8	3	CIRCULAR ELLIPTICAL	18	_	0.40		+16		13
22	021155	27.8N 140.5E	700MB	2772	300	33 330	110	180	81		72	15	2	CONCENTRIC	•	5	949	+14	+17	+15	14
23	021133	28.3N 139.3E	788MB	2820				080	77		87	5	6	CONCENTRIC							14
24	022206	28.5N 139.5E	788MB	2834		65 260	90	168		980		4	6	CIRCULAR	15			+15	±16	114	15 15
25	030857	29.3N 139.4E	700MB	2778	963	65 350		686		350		4	ž	CIRCULAR	20				+16		16
26	031200	29.3N 139.4E	700MB	2805	200			180		090		4	2	CIRCULAR	20			+10	+10	T14	16
27	031431	29.4N 139.8E	700MB	2802	968						•••	5	6	CIRCULAR	15			+14	+15	417	17
28	031801	30.2N 140.4E	700MB	2796				190	76	098	90	3	5							.15	17
29	032123	30.7N 140.7E	700MB	2787	964	80 320	60	330	75	260	45	2	4					+17	+17	+15	18
30	040012	30.8N 141.2E	700MB	2773		60 190	11	200	85	689	87	3	3								18
31	040230	31.4N 142.0E	700MB	2805	965	90 320	105	160	61	0 30	70	5	1					+15	+18	+14	18
32	040857	32.2N 143.7E	700MB	2794	966	80 290	130	250	96	170	85	8	10					+15	+15	+15	19
33	041205	32.9N 144.5E	780MB	2798				190	71		90		10								19
34	041440	33.3N 145.1E	700MB	2806				260	84		90		10					+17	+16	+15	19
35	042123	35.1N 147.4E	700MB	2849	973	88 090		150		090		2	4					+12	+14	+14	20
36	050008	35.6N 147.8E	700MB	2848		60 180	98	010	78	626	68	2	2								20

TROPICAL STORM HOPE BEST TRACK DATA

BEST TR	RACK	WARN	NG ERRORS	24 H	DUR FORECAST ERRORS	48 HOUR F	ORECAST ERRORS	72 HOU	R FORECAST ERRORS
MO/DA/HR POSIT WI	IND POSI	T WIND	DST WIND	POSIT	WIND DST WIND	POSIT WIND	DST WIND	POSIT W	IND DST WIND
090400Z 16.2 118.5	25 0.0	8.8 8.	-0. 0.	0.0 0.0	00. 0.	0.0 0.0 0.	-0. O.	0.0 0.0	00. 0.
090406Z 16.5 118.2	30 0.0	0.9 0.	-0. 0.	0.0 0.0	00. 0.	8.6 0.6 0.	-0. 0.	0.0 0.0	00. 0.
0904122 16.6 117.7	35 16.8 1	18.0 30.	215.	17.8 116.8	40. 19915.	18.4 115.4 50.	49110.	0.0 0.8	00. 0.
090418Z 16.6 116.9	40 17.0 1	17.8 30.	5710.	18.0 116.4	40. 24920.	18.6 115.0 50.	450. 8.	0.0 0.0	00. 0.
090500Z 16.6 116.0	45 16.5 1	16.0 40.	65.	16.8 114.2	50. 17610.	8.0 0.0 0.	-0. 0.	0.0 0.0	00. 0.
090506Z 16.5 114.8	50 16.5 1	15.4 45.	355.	17.3 113.6	50. 218. ~10.	8.6 9.9 8.	-0. 0.	0.0 0.9	00. 0.
090512Z 16.5 113.6	55 16.5 1	13.6 55.	0. 0.	17.9 109.9	60.142. 0.	0.0 0.0 0.	-0. 0.	0.0 0.0	00. 0.
0905182 16.4 112.4	60 16.4 1	12.2 60.	12. 0.	17.8 108.2	60. 134. 10.	0.0 0.0 0.	-0. 0.	0.0 0.0	00. 0.
090600Z 16.2 111.2	60 16.2 1	111.0 60.	12. 0.	0.0 0.0	00. 0.	8.6 0.9 9.	-8. 0.	8.0 0.0	00. 0.
090606Z 15.9 110.1	60 16.0 1	109.6 60.	29. 0.	0.0 0.0	0. - 0. 0.	9.0 0.0 0.	-0. 0.	0.0 0.0	00. 0.
0906122 15.7 109.0	60 15.8 1	09.0 60.	6. 0.	0.0 0.0	00. O.	0.0 0.0 0.	-8. 8.	0.8 8.9	80. 0.
090618Z 15.6 107.8	50 15.5 1	00.0 40.	1310.	0.0 0.0	00. 0.	8.6 8.8 0.	-0. 0.	0.0 0.0	00. 8.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR		WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	19.	186.	426.	Ð.		0.	ø.	0.	Ø.	
AVG RIGHT ANGLE ERROR	9.	79.	118.	ø.		0.	0.	0.	9.	
AVG INTENSITY MAGNITUDE ERROR	4.	11.	5.	0.		ø.	8.	0.	8.	
AVG INTENSITY BIAS	-4.	-8.	-5.	0.		0.	0.	0.	0.	
NUMBER OF FORECASTS	10	6	2	8		9	0	0	0	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 630. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

10. KNOTS

TROPICAL STORM HOPE FIX POSITIONS FOR CYCLONE NO. 17

FIX	TIME	FIX				
ND.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	041600	15 EN 115 CC	DOM C			
_		15.5N 115.6E	PCN 6	T	***** ***	PGTW
2	040000	16.4N 118.3E	PCN 6	T2.0/2.0	INIT OBS -	PGTW
3	040300	16.5N 118.3E	PCN 6			PGTW
4	040600	16.7N 118.5E	PCH 4			PGT⊍
5	040714	16.7N 118.1E	PCN 5	T2.0/2.0	INIT OBS	RPMK
6	040900	15.9N 117.5E	PCN 6			PGT⊎
* 7	041200	16.0N 116.4E	PCN 6			PGT⊌
* 8	041800	16.5N 116.9E	PCN 6			PGTW
9	042100	17.1N 116.6E	PCN 6			PGTW
10	9 59999	16.5N 115.3E	PCN 6	T3.0/3.0 /D1.0/24HRS		PGTW
11	050 300	16.5N 115.2E	PCN 6			PGTU
12	0 50600	16.3N 114.5E	PCN 6			PSTW
13	050702	16.3N 114.4E	PCN 5	T3.5/3.5+/D1.5/24HRS	•	RPMK
14	050900	16.3N 114.2E	PCN 6			PGTW
15	051200	16.1N 113.1E	PCN 6			PGTW
16	051600	16.1N 111.9E	PCN 6			PGTU
17	051800	16.2N 111.6E	PCN 6			PGTW
18	052100	16.0N 111.9E.	PCN 6			PGTW
19	969999	15.8N 110.8E	PCN 6			PGTW
20	969399	15.5N 110.2E	PCN 6	T3.5/3.5-/D0.5/27HRS		PGTW
21	868688	15.8N 109.8E	PCN 6			PGTW
22	060650	15.5N 110.2E	PCN 5	T4.0/4.0-/D0.5/24HRS		RPMK
23	060900	15.7N 109.5E	PCN 6			PGTW
24	861200	15.7N 109.1E	PCN 6		ULCC FIX	PGTW
25	961600	15.8N 108.3E	PCN 6		ULCC FIX	PGTW
26	061800	15.7N 107.9E	PCN 6		ULCC FIX	PGTU
		101.JL			OLCC FIX	raiw

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT		MAX-SFU VEL∕BRO								EYE SHAPE	EYE DRIEN- DIAM/TATION		
1	042357	16.5N 116.0E	700MB	2986	994	45 066	10	160	47 1	9 59	12	5	5			+13 +17 +16	•
							RADAI	RFIXE	5								
FIX NO.	TIME (Z)	FIX POSITION	RADAR AL	CRY	EYE SHAPE	E)	Æ AM	RADOB ASWAR						COMMENTS		RADAR POSITION	SITE WHO No.
1 2	051750 052050	16.9N 112.7E 17.1N 112.0E	LAND LAND					5///3 5///3								16.8N 112.3E 16.8N 112.3E	59981 59981
						51	NOPT	IC FIX	ES								
FIX NO.	TIME (Z)	FIX POSITION	INTENSIT ESTIMATE		REST A (NM)			C	OMMEI	NTS							

HBDF SHIP OBSERVATION HBDF SHIP OBSERVATION WMO 59981 WMO 59985

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

1 041200 16.8N 118.0E 2 041800 16.8N 117.1E 3 051800 16.5N 112.3E 4 060000 16.2N 111.2E

TYPHOON IRVING BEST TRACK DATA

		•		
BEST TRACK	WARNING	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
	ERRORS	ERRORS	ERRORS	ERRORS
MO/DA/HR POSIT WIND POSIT	WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DST WIND
0904182 13.8 133.3 25 0.0 8	.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 JC. O.
090500Z 12.9 132.8 25 0.0 8	.0 00. 0.	0.0 0.0 08. 0.	0.0 0.0 0 0. 0.	0.0 0.0 d0. O.
090506Z 13.2 132.2 30 13.2 132	.1 30. 6. 0.	14.8 130.5 40. 124. 5.	15.8 127.8 55. 190. 0.	16.3 124.5 6 5. 192. 5.
090512Z 13.7 131.4 30 13.6 131	.7 30. 18. 0.	15.2 130.0 45. 163. 5.	15.9 127.0 60. 187. 0.	16.4 123.7 7A. 192. 15.
090518Z 14.1 130.7 30 13.9 131	.0 35. 21. 5.	14.9 128.7 50. 117. 5.	15.6 125.7 65. 156. 5.	15.9 122.2 79, 173, 20,
090600Z 14.2 129.6 35 14.3 129	.8 35. 13. 0.	15.5 126.2 50. 165. 0.	15.8 122.5 70. 230. 10.	16.8 118.6 63. 292. 10.
090606Z 13.7 128.7 35 14.4 126	.2 40. 51. 5.	15.0 124.0 50. 1935.	16.2 120.0 45. 31615.	18.4 117.0 55. 391. 5.
0906127 13.2 128.1 40 13.4 126	.2 50. 13. 16.	13.0 125.0 65. 65. 5.	13.4 121.8 55. 117. 0.	14.0 118.2 55. 158. 5.
090618Z 13.2 127.7 45 13.2 127		13.8 124.0 60. 99. 0.	13.6 120.8 55. 136. 5.	14.2 117.2 60. 170. 10.
0907002 12.9 127.1 50 13.0 127		13.0 124.1 70. 64. 10.	13.5 121.2 55. 70. 5.	13.9 118.4 60. 76. 10.
090706Z 12.9 126.5 55 12.9 126		13.1 123.2 60. 70. 0.	13.8 120.4 55. 82. 5.	14.3 117.3 60. 75. 10.
0907122 12.9 126.1 60 13.0 126		13.0 123.9 55. 13. 0.	13.7 120.8 50. 31. 0.	14.3 117.8 60. 57. 5.
0907182 13.0 125.7 60 12.8 125		13.0 122.5 50. 37. 0.	14.1 119.5 55. 42. 5.	15.0 116.3 60. 26. 0.
090800Z 13.0 125.2 60 13.1 125		13.2 123.3 55. 58. 5.	13.7 120.9 50. 122. 0.	14.9 118.3 55. 14110.
090806Z 13.1 124.4 60 13.1 124		13.5 121.4 50. 29. 0.	14.6 118.8 55. 42. 5.	16.2 115.9 60. 515.
090812Z 13.2 123.8 55 13.0 123		13.8 120.5 50. 33. 0.	15.2 117.8 55. 17. 0.	16.8 114.8 60. 60. 10.
0908182 13.2 123.1 50 13.2 122		14.2 119.8 50. 25. 0.	15.5 117.2 60. 34. 0.	17.3 114.0 60. 7215.
090900Z 13.6 122.4 50 13.4 122		13.8 120.0 50. 81. 0.	14.2 117.5 55, 114, -10.	14.7 113.B 60. 106. 20.
090906Z 13.8 121.8 50 13.6 121		14.6 119.4 50. 92. 0.	14.3 116.7 55. 10410.	14.7 112.9 60. 13630.
090912Z 14.2 120.9 50 14.1 120		14.6 118.2 60. 54. 5.	14.9 114.8 60. 5418.	15.4 110.5 60. 21330.
090918Z 14.5 120.1 50 14.8 119		15.9 116.5 60. 44. 0.	16.5 113.2 60. 7715.	17.8 109.2 60. 24130.
0910002 14.9 119.2 50 15.0 119		16.0 115.6 60. 455.	16.8 112.2 60. 12320.	18.1 108.5 55. 26930.
091006Z 15.1 118.3 50 15.0 117		15.1 114.3 60. 685.	15.1 111.4 65. 17825.	16.3 107.9 50. 31530.
0910122 15.2 117.5 55 15.3 117	,	16.7 114.8 65. 545.	16.9 111.9 60. 10930.	17.0 109.4 55. 20920.
0910182 15.2 116.7 60 15.5 116		16.8 114.2 60. 4015.	17.0 111.2 55. 12835.	17.0 108.2 50. 26625.
091100Z 15.3 115.9 65 15.4 115		16.2 112.8 55. 8725.	16.6 109.8 50. 20635.	16.7 106.8 35. 33835.
091106Z 15.5 115.4 65 15.8 115		16.5 112.3 55. 9835.	16.5 109.4 50. 23030.	16.7 106.9 35, 328, 35,
0911122 15.8 114.9 70 15.8 114		16.9 112.6 55. 6935.	17.3 110.2 50. 16025.	17.3 107.8 51. 262. 15.
091118Z 16.2 114.5 75 16.2 114		18.0 113.7 70. 4020.	19.2 112.0 65. 4110.	19.3 111.0 55. 4810.
091200Z 16.4 114.3 80 16.7 114		18.8 113.2 70. 6615.	20.2 111.0 60. 7510.	22.2 110.5 45. 109. ~15.
091206Z 16.4 114.5 00 16.7 114		18.5 112.8 95. 35. 15.	20.2 111.7 80. 49. 10.	22.1 110.8 65. 98. 5.
0912127 17.0 113.8 90 17.0 113		18.4 112.4 95. 24. 20.	20.1 111.3 80. 16. 15.	22.0 110.8 65. 119. 5.
0912182 17.4 113.4 90 17.2 113		18.2 111.7 95. 55. 20.	19.9 110.5 70. 36. 5.	21.9 110.2 60. 129. 5.
091300Z 17.7 113.2 85 17.6 112		19.0 111.4 80. 45. 10.	20.8 110.8 70. 41. 10.	22.9 110.0 50. 179. 5.
		18.8 112.8 75. 62. 5.	20.5 111.6 65. 115. 5.	0.0 0.0 00. 0.
091306Z 18.0 113.1 80 18.0 113 091312Z 18.3 112.8 75 18.3 113		19.9 112.1 65. 34. 0.	21.8 111.2 60. 137. 0.	8.0 0.0 00. 0.
		21.0 111.1 50. 5415.	23.0 108.4 30. 8325.	8.8 8.8 90. 8.
		21.1 111.1 65. 66. 5.	8.8 0.8 00. 0.	0.0 0.0 00. 0.
0914002 19.0 112.2 76 19.1 112		20.9 110.9 60. 73. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
091406Z 19.4 111.9 70 19.3 113		22.1 110.8 50. 12110.	0.6 0.0 00. 0.	0.0 0.0 00. 0.
0914122 19.9 111.5 65 20.0 111		22.1 110.8 50. 12110.	0.8 0.8 60. 0.	0.0 0.0 00. 0.
0914182 20.1 111.1 65 20.3 113			8.0 8.0 80. 0.	0.0 0.0 00. 0.
0915002 20.4 110.2 60 20.6 110			9.0 8.0 60. 0.	0.0 0.0 00. 0.
091506Z 20.9 109.6 60 20.8 109		0.0 0.0 08. 0.	9.0 0.0 00. 0. 9.0 0.0 00. 0.	8.8 8.8 60. 0.
0915122 21.3 108.8 60 21.5 106		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.8 00. 0. 0.0 0.8 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
091510Z 21.7 107.9 55 21.7 107			2.2 2.3 2. 2. 2.	0.0 0.0 00. 0.
0916002 21.8 107.0 45 21.8 107	.0 45. 0. 0.	0.6 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KT					
	WRNG	24-HR	48-HR	72-HR	LIRHG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	13.	73.	118.	172.	13.	73.	110.	172.		
AVG RIGHT ANGLE ERROR	9.	42.	72.	126.	9.	42.	72.	126.		
AVG INTENSITY MAGNITUDE ERROR	2.	Θ.	11.	15.	2.	8.	11.	15.		
AVG INTENSITY BIAS	ø.	-2.	-6.	-8.	-0.	-2.	-6.	-8.		
NUMBER OF FORECASTS	44	40	35	32	41	40	35	32		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1778. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 7. KNOTS

TYPHODN IRVING FIX POSITIONS FOR CYCLONE NO. 18

FIX NO.	TIME	FIX	occov.	PLODOK CORE	CONTRACT LI TOPO	CITT
nu.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
		12,8N 132,6E	PCN 6			PGTW
2	050300	13.2N 132.0E 13.5N 132.6E	PEN 6 PCN 3	T1.0/1.0	INIT GBS	PGTW
4	050520 050600	13.4N 132.5E	PCN 4	11.071.0	1411 002	PG TW PGTW
		13.4N 132.2E	PCN 4			PGTW
		13.6N 131.7E	PCN 6			PGTW
7	051600	13.5N 130.8E	PCN 6			PGTU
* 9	051000 052100	12.8N 130.3E 14.0N 120.9E	PCN 6 PCN 6			PGTW PGTW
10	060000	13.7N 128.7E	PCN 6			PGTW
11	060300	13.7N 128.4E		T2.5/2.5 /D1.5/21HRS		PGTW
12	969699	13.5N 127.8E	PCN 6	TO 0.00	***** 000	PGTW
1.5	060650 060650	13.2N 128.0E 13.2N 127.7E	PCN 6	T2.0/2.0	INIT OBS	RPMK PGTW
15	061200	13.6N 127.9E	PCH 6		ULCC FIX	PGTW
16	96 1 699	13 3N 127 6F	PCN 6		ULCC FIX	PGTW
17	061753	13.3N 127.5E	PCN 5			PGTW
19	052100	13.3N 127.5E 13.2N 127.3E 13.2N 127.0E	PCN 6 PCN 6			PGTW PGTW
20	979399	13.0N 126.6E		T3.5/3.5-/D1.0/24HRS		PGTW
21	070600	13.1N 126.4E	PCN 4			PGTW
22	070637	13.0N 126.5E 13.0N 126.2E	PCN 5	T3.5/3.5 /D1.5/24HRS		RFMK PGTW
23	070900	13.0N 126.2E	PCN 6			PGTW
25	071600	12.7N 125.4E	PCN 6			PGTW
26	971899	12.5N 125.2E	PCN 6		ULCC FIX	PGTW
27	071922	13.1N 125.1E	PCN 5		ULCC FIX	RODH
28	072100	13.1N 125.1E 12.9N 125.1E 13.2N 124.6E	PCN 6 PCN 6		ULCC FIX	PATW PGTW
30	080300	13.1N 124.6E	PCN 6	T3.5/3.5 /S0.0/24HRS		PGTW
31	999626	13.2N 124.3E	PCN 5			PGTW
32	090626	13.1N 124.1E	PCN 3	T4.0/4.0-/D0.5/24HRS		RPMK
33	080900	13.1N 124.0E 13.1N 123.7E	PCN 6 PCN 6		ULCC FIX	PGTW PGT⊍
35	981699	13.2N 122.9E	PCN 6		ULCC FIX	PGTW
36	081800	13.3N 122.4E	PCN 6		ULCC FIX	PGTW
37	882100	13.BN 122.1E	PCN 6		ULCC FIX	PGTW
38	090000	13.6N 122.4E 13.9N 122.3E	PCN 6	T2.5/3.5+/W1.0/24HRS		PGTW PGTW
39 40	090613	14.3N 121.3E	PCN 5	12.5/3.5#/WI.8/24NK5		PGTW
41		14.2N 120.4E	PCN 3			RPMK
42	090900	14.1N 120.3E	PCN 6			PGTW
		14.2N 121.1E	PCN 4		III og Etu	RPMK
		14.6N 120.2E 15.0N 119.8E	PCN 6 PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
		15.4N 119.3E	PCN 6		occo (in	PGTW
47	091858	15.1N 119.7E	PCN 5		ULCC FIX	RODH
* 48	091858	15.5N 119.0E	PCN 5		ULCC FIX	PGTIJ
49 50	092100	14.9N 119.7E 14.9N 119.0E	PCN 6 PCN 4		ULCC FIX BRKS CONTINUITY	PGTW PGTW
51	100300	15.3N 118.6E		T3.5/3.5 /D1.0/24HRS		PGTW
	100601	15.4N 118.0E	PCN 5			PGTW
53	100601	15.1N 117.6E	PCN 5	T3.5/3.5 /D0.5/24HRS		RPMK PGTU
		15.3N 117.3E	PCN 6		ULCC FIX	PGTU
55 56	101200 101600	15.5N 116.8E 15.3N 116.7E	PCN 6			PGTW PGTW
		15. IN 116.6E	PCN 6			PGT₩
58	101846	15.8N 116.5F	PCN 5			PGTW
59 68	102100	15.2N 116.3E 15.5N 115.9E	PCN 6		ULCC FIX	PGTW PGTW
61	110300	15.7N 115.7E	PCN 4		OLCC FIN	PRTW
62	110600	15.8N 115.4E	PCN 2	13.5/3.5 /S0.0/27HRS		PGTW
63		15.8N 115.2E	PCN 4			PGTW
64 65	111200	15.9N 115.1E 16.0N 114.8E	PCN 4			PGTW PGTW
66	111600	16.3N 114.6E	PCN 4 PCN 4			PGTW
67	112100	16.4N 114.3E	PCN 4			PGTW
68	120000	16.6N 114.1E	PCN 4		ULCC FIX	PGTIJ
69 70	120300	16.7N 113.9E	PCN 4	TE 9 & 9 01 E 04000		PGTU
70 71	120600 120719	16.7N 113.9E 16.8N 113.9E	PCN 1 PCN 1	T5.0/5.0-/D1.5/24HRS T5.0/5.0 /D1.5/25HRS		PGTW RODN
72	120900	16.9N 113.7E	PCN 2			PRITU
73	121200	17.1N 113.5E	PCN 2			FGTW
74	121600	17.1N 113.2E	PCN 2			PG fU
75 76	121888 122100	17.3N 113.1E 17.4N 113.0E	PCN 2 PCN 2			PG TW PG TW
77	130000	17.6N 113.0E	PCH 2			PGTW
78	130300	17.8N 113.1E	PCN 2	T4.0/4.5 /U1.0/21HRS		PGTIJ
79	130600	18.1N 112.9E	PCN 2			PG FW
80 81	130706 130900	10.2N 113.1E 10.3N 112.8E	PCN 6	T4.5/5.0 /W0.5/24HRS	ULCC FIX	RAINN FISTW
82	131200	18.5N 112.5E	PCN 6		OLGG (IA	PGTW
83	131600	18.8N 112.5E	PCN 6			PSTW
84	131800	18.8N 112.2E	PCN 6			PGIW

85 87 88 99 91 92 93 93 95 97 98 99 100 101 103 104 105 106 107 108	131951 132100 140000 140300 140600 140600 141600 141600 141600 141939 142100 150600 150643 150643 150643 150600 151600 151600 151800 151800 151800 151800 151800 151800 151800 151800 151800 151800 161800 161800 160631	18.7N 112.3E 18.9N 112.2E 19.1N 112.1E 19.2N 112.9E 19.7N 111.9E 19.8N 111.5E 20.2N 111.4E 20.2N 110.5E 20.2N 110.5E 20.2N 110.5E 20.2N 110.5E 20.2N 109.9E 20.6N 109.9E 20.6N 109.9E 20.9N 109.4E 20.9N 109.4E 20.9N 109.6E 21.5N 109.6E 21.4N 109.2E	PCN 2 PCN 1 FCN 6 PCN 6 PCN 6 PCN 6 PCN 2 PCN 2 PCN 2 PCN 1 FCN 2 PCN 2 PCN 2 PCN 4 PCN 2 PCN 1 FCN 2 PCN 1 FCN 2 PCN 1 FCN 2 PCN 4 PCN 4 PCN 4 PCN 6	4.0/4.0-/50. 4.5/4.5-/50. 3.5/4.0-/JJ0. 3.5/4.5-/JJ1. 4.0/4.0-	9/24HRS 5/24HRS 8/24HRS	ULCC F	IΧ	RPPK PGTW PGTW PGTW RODN PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW		
					AIRCE	RAFT FIXES				
FIX NO.	TIME (Z)	FIX POSITION			AX-SFC-WND EL/BRG/RNG	MAX-FLT-LVL-I DIR/VEL/BRG/		EYE ORIEN- DIAM∕TATION		MSN NO.
* 2 3 4 5 6 7 8 9 10 11 12	050729 052218 060715 060928 070722 070947 071920 072205 092008 092306 100844 101043 120623	13.2N 132.0E 14.2N 129.9E 13.5N 128.4E 13.6N 128.4E 13.0N 126.4E 13.0N 126.3E 13.1N 125.4E 14.9N 119.4E 14.9N 119.4E 14.9N 119.7E 15.1N 117.0E 15.2N 117.7E 16.8N 113.9E	700MB 38 700MB 36 700MB 25 700MB 25 700MB 25 700MB 25 700MB 25 700MB 25 700MB 25 700MB 25	991 999 154 1000 1774 1000 1776 1045 1000 1045 1000 1040 1000	35 240 52 38 350 30 58 300 27 58 138 30 45 350 30 45 350 30 40 070 60 55 080 35 55 360 10 40 360 60 20 220 90 90 120 18	238 23 258 088 39 359 109 35 309 109 60 029 296 65 140 248 44 109 030 49 270 060 70 310 060 59 310 060 59 310 060 58 359 290 53 220 120 95 060	48 5 3 60 5 5 5 7 10 3 20 10 3 2 5 5 3 3 3 5 5 5 3 3 3 6 5 5 2 8 10 1 3 0 3 3 2 0 1	20	+25 +22 34 +14 +12 +11 32 +11 + 8 +15 +14 +11 +17 +17 + 9 +13 +17 +12 +19 + 7 +12 +19 +12 +17 +28 +12	1 2 3 3 5 5 6 6 7 7 8 8 10
FIX NO.	TIME (Z)	FIX POSITION	RADAR ACCR	EYE RY SHAPE	EYE	RADOB-CODE ASWAR TODEF	COMMENTS	P	RADAR SITE OSITION UMO NO.	
11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28	998830 999980 991980 991280 9913280 991480 991580 991580 992158 892155 892280 892235 892235 892235 892235 892236 89226 8926 89	15.4N 119.7E 14.8N 119.2E 15.0N 119.2E 14.8N 119.1E 14.8N 119.0E 15.0N 119.0E 14.9N 118.8E 14.9N 118.5E	LAND FAILAND GOOLAND GOOLAND GOOLAND LAND LAND LAND LAND LAND LAND LAND	D D D ELLIPTIO	CAL	10/1/ 42/06	EYE OPEN N EYE OPEN NU MVG WNW 4 KTS MVG WNW 4 KTS N TO 5 AXIS 37/20 N TO 5 AXIS 24/14 EYE 100 PCT CIR DIA 20 EYE 100 PCT CIR DIA 15 EYE 100 PCT CIR DIA 30 EYE 100 PCT CIR DIA 30 EYE 90 PCT CIR DIA 32N EYE 90 PCT CIR DIA 32N EYE 90 PCT CIR OPEN E	14 14 14 14 14 14 16 16 15 16 16 16 16 16 16 16 16 16 16 16 17 18 18 18 18 18 18 18 18 18 18 18 18 18	3N 120.5E 98321	

31	100600	15.0N 117.7E	LAND	1072/ 430			120.6E	98321
32	100738	15.0N 117.7E	LAND	1871/ 400	100	16.3N	120.6E	98321
33	100666	15.0N 117.5E	LAND	1077/ 417	'05	16.3H	120.6E	98321
34	101030	15.1N 117.2E	LAND	1071/ 439	05	16.3N	128.6E	98321
35	112350	16.4H 114.1E	LAND	10683 529	96	16.BN	112.3E	59981
36	120050	16.5N 114.1E	LAND	10732 430			112.3E	59981
37	120250	16.5N 114.0E	LAND	10413 530			112.3E	59981
38	120650	16.8N 113.8E	LAND	10512 535			112.35	59981
39	120950	17.0N 113.7E	LAND	10512 534			112.3E	59981
40	121150	17.2N 113.5E	LAND	10512 534			112.3E	59981
41	121250	17.3N 113.5E	LAND	10512 534			112.3E	59981
42	121350	17.3N 113.4E	LAND	10512 534			112.3E	59981
43	121450	17.4N 113.4E	LAND	10512 534			112.3E	59981
44	121550	17.4N 113.4E	LAND	10512 534			112.3E	59981
45	121650	17.5N 113.4E	LAND	10511 534			112.3E	59981
46	121750	17.4N 113.3E	LAND	10511 534			112.3E	59981
47	121850	17.5N 113.3E	LAND	10512 533			112.3E	59981
48	121950	17.5N 113.2E	LAND	10512 533			112.3E	59981
49	122150	17.6N 113.1E	LAND	11712 533			112.3E	59981
59	122250	17.6N 113.1E	LAND	10712 533			112.3E	59981
				10712 533				
51	130050	17.7N 113.1E	LAND				112.3E	59981
52	130550	18.0N 112.8E	LAND	30762 534			112.3E	59981
53	130650	18.1N 112.8E	LAND	30713 534			112.3E	59981
54	130850	18.3N 112.8E	LAND	30713 534			112.3E	59981
55	131150	18.5N 112.6E	LAND	3///3 534			112.3E	59981
56	131250	18.6N 112.6E	LAND	3///3 534			112.3E	59981
57	131450	18.7N 112.5E	LAND	3///3 534			112.3E	59981
58	131858	19.0N 112.3E	LAND	5///3 ///			112.3E'	59981
59	132200	18.8N 112.3E	LAND	10512 531	04	20.0N	110.3E	59758

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		CONTENTS
1 2 3 4 5 6 7	081200 081600 091200 091600 130000 142100 151600	13.0N 123.7E 13.1N 123.0E 14.0N 121.0E 14.5N 120.2E 17.8N 113.1E 20.4N 110.7E 21.7N 107.9E	055 055 050 050 050 085 060 055	015 050 025 025 075 030 045	umo 98444 umo 98448 umo 98428 umo 98426 umo 59981 umo 59758	

TYPHOON JUDY BEST TRACK DATA

	BEST TR	ACK		WARN		RORS		24 H	OUR F				48 H	OUR FO	ORECA			72 H		ORECAS	
MO/DA/HR	POSIT WI	MT	POSIT	MIND		WIND	200			ERR					ERRO					ERRORS	
0905002		20 20	0.0 0.0		-8.		P09		MIND		MIND	POS		MIND		MIND	POS		MIND	DST	
0905062		25	0.0 0.0	Ø.		ø.	8.9	0.0	e.	-0.	0.	0.0	8.0	0.	-0.	0.	0.0	0.0	9.	-e.	0.
6905 122		20 30		0.	-0.	0.	8.0	0.0	υ.	-0.	0.	8.8	8.8	0.	-0.	0.	0.0	0.0	8.	-0.	0.
090518Z		35	0.0 0.0 12.7 144.2	8.	-0.	. 0.	0.0	0.0	0.	-0.	0.	0.0	0.0	. 0.	-0.	.0.	0.0	0.0	٥.	-9.	0.
0906002		30 40	12.7 144.2 12.8 143.2	25.	8.	-10.	13.3	140.4	48.	113.	-10.		137.2	50.	197.	-15.		134.1	65.		-15.
090606Z		40 48		40.	19.	ø.	13.2	139.1	50.	160.	0.		135.1	60.	256.	-10.		131.0	70.	427.	15.
090612Z		40 45		40.	6.	ø.		140.5	58.	84.	-5.		136.8	65.	228.	-10.		133.1	75.	452.	-15.
090618Z				40.	8.	-5.		139.7	55.	78.	-5.		136.1	65.	246.	-10.		132.4	84.	461.	-5.
090700Z		50 50	13.8 142.2	50.	12.	0.		140.0	65.	144.	ø.		136.8	75.	315.	-5.		133.0	85.	535.	0.
090706Z			14.4 141.6	50.	в.	ø.		139.1	65.	109.	-5.		136.2	80.	266.	-5.		133.0	95.	3 99.	15.
090712Z		55	14.7 140.8	55.	21.	0.			70.	133.	-5.		134.8	85.	257.	-5.		130.7	100.	417.	20.
6907122		60	15.7 140.0	55.	18.	-5.		136.8	75.	91.	0.		133.6	90.	210.	5.			110.	354.	35.
		65	16.7 139.2	60.	23.	-5.		135.7	80.	73.	ø.		132.2	95.	215.	10.			115.	368.	40.
090800Z		78	17.4 137.8	60.	8.	-10.		133.8	85.	114.	0.		131.0	110.	195.	30.			115.	313.	40.
898886Z		75	18.1 136.9	65.	8.	-10.		133.4	90.	112.	0.		138.8	115.	227.	35.		129.7	95.	353.	20.
0908122		75	18.8 136.1	70.	31.	-5.		133.1	95.	106.	10.		131.0	105.	211.	30.		129.B	95.	374.	20.
090818Z		88	20.5 135.3	75.	13.	-5.		133.3	95.	42.	10.		135.3	90.	224.	15.		142.9	80.	376.	5.
		85	21.8 134.5	90.	26.	5.		133.3		100.	25.		137.0	70.	388.	-5.	0.0	0.0	0.	-0.	0.
		90	22.5 133.8	90.	8.	0.		133.4	90.	103.	10.		137.3	65.	379.	-10.	0.0	0.0	8.	-8.	0.
		85	23.4 133.4	90.	13.	5.		134. I	85.	169.	10.		139.2	60.	465.	-15.	0.0	0.0	0.	-0.	0.
		85	24.2 133.2	90.	27.	5.		134.6	65.	192.	-10.		141.3	40.	540.	-35.	0.0	0.0	₽.	-6.	0.
091000Z		80	24.8 133.8	75.	ø.	-5.		134.7	65.	136.	-10.		140.9	45.	403.	-30.	0.0	0.0	9.	-a.	0.
091006Z		80	25.7 133.8	75.	24.	-5.		135.8	60.	216.	~15.		143.0	40.	434.	-30.	0.0	0.0	0.	-0.	0.
		75	26.3 134.0	75.	32.	0.		136.2	60.	187.	-15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
		75	26.4 134.8	75.	6.	0.		137.6	70.	45.	-5.	0.0	8.0	0.	-0.	Ø.	0.0	0.0	0.	-0.	0.
		75	27.1 135.3	80.	Ø.	5.		138.5	70.	81.	-5.	0.0	9.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
		75	27.9 135.8	75.	8.	0.	32.7	139.2	60.	110.	-10.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
	28.7 136.5	75	28.4 136.3	75.	21.	0.	32.8	139.7	60.	234.	5.	0.0	0.8	ø.	-0.	0.	0.0	0.0	ø.	-0.	ø.
		75	29.5 136.9	70.	19.	-5.	36.1	139.7	60.	204.	20.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
		75	31.7 137.2	70.	21.	-5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	ø.
091206Z	33.6 137.3	70	33.5 137.3	70.	6.	ø.	0.8	6.8	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	ø.	-0.	ø.
091212Z	36.2 137.4 5	55	35.4 139.3	60.	104.	5.	8.8	0.0	0.	-0.	0.	0.0	8.0	0.	-0.	ø.	0.0	0.0	ø.	-ē.	ø.
091218Z	39.5 139.5	40	40.0 148.8	45.	38.	5.	0.0	0.0	ø.	-8.	0.	9.0	0.0	ø.	-0.	ø.	0.0	0.0	ø.	-8.	ē.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS						
	WRNG	24-HR	48-HR	72-HR	WRNG	24-H	48-HF	? 72-HR			
AVG FORECAST POSIT ERROR	19.	125.	298.	401.	19.	125.	298.	481.			
AVG RIGHT ANGLE ERROR	15.	73.	126.	262.	15.	73.	126.	262.			
AVG INTENSITY MAGNITUDE ERROR	4.	8.	16.	19.	4.	8.	16.	19.			
AVG INTENSITY BIAS	-2.	-0.	-3,	11.	-2.	-0.	-3.	11.			
NUMBER OF FORECASTS	29	25	19	13	29	25	19	13			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2133. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON JUDY FIX POSITIONS FOR CYCLONE NO. 19

FIX	TIME	F1X				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
1	050000	12.1N 147.3E	PCN 6			PGTW
ż	050300	12.3N 146.9E	PCN 6			PGTW
3	050520	12.5N 146.6E	PCN 5	T1.5/1.5	INIT OBS ULCC FIX	
4	050600	12.6N 146.5E	PCN 6	11.3/1.3	INTI UBS QUOC FIX	PGTW PGTW
5	050900	12.8N 146.3E	PCN 6			PGTW
š	051200	12.7N 145.5E	PCN 6			PGTW
7	051600	12.3N 144.2E	PCN 6			PGTW
. 8	051800	12.1N 143.5E	PCN 6			PGTW
9	052100	13.1N 143.6E	PCN 6			PGTW
10	060000	13.4N 143.3E	PCN 6			PGTW
11	060300	13.3N 143.1E	PCN 6	T2.5/2.5 /D1.8/21HRS		PGTW
12	060508	13.1N 142.8E	PCN 5	12.3/2.5 /DI.6/211R3		PGTW
13	060600	13.3N 142.7E	PCN 6			
14	060900	13.4N 142.5E	PCN 6			PGTW
15	061200	13.5N 142.5E	PCN 6			PGTW
16	061600	13.3N 141.6E	PCN 6		ULCC FIX	PGTW
17	061753	14.0N 141.9E	PCN 5			PGTW
18	062100	14.4N 141.8E	PCN 6		BRKS CONTINUITY	PGTW
19	070000					PGTW
20	070300	14.4H 141.4E	PCN 6	77 E 2 E 21 2 2 4 10 1		PGTW
21	070456	14.3N 141.1E	PCN 6	T3.5/3.5 /D1.0/24HRS		PGTW
		14.3N 140.9E	PCN 5			PGTW
22	070600	14.7N 140.7E	PCN 6			PGTW
* 23	070900	14.8N 140.5E	PCH 4			PGTW

24	071200	15.9N 139				PGTU
25	071600	16.7N 139.				PGTW
26	071741	16.9N 138.			ULCC FIX	PRTU
27	071741	16.8N 138.	.6E PCN 5			RODH
28	072100	17.5N 138	.0E PCN 6		ULCC FIX	Pritu
29	080000	17.5N 137	.7E PCN 6			PGTW
30	080300	17.7N 137	.4E PCN 6	T4.5/4.5 /D1.0/24HRS		PGTW
31	080444	17.9N 137	.2E PCN 5			PGTW
32	080600	17.9N 137	.2E PCN 6			PGTW
33	080900	18.3N 137	.2E PCN 6			PGTW
34	081200	19.4N 136			ULCC FIX	reno
35	081600	19.7N 135			ULCC FIX	PUTW
36	081720	20.4H 135			ULCC FIX	PATU
37	090000	21.9N 135			0200 1 111	PGTW
38	090300	21.9H 135		T5.0/5.0 /D0.5/24KRS		PGTU
39	090613	22.4N 134		12.0.010 . 20.0.0 . 2		PGTW
40	090900	22.9N 133				PSTW
41	091200	23.1N 133				PGTW
42	091600	23.7N 133				PGTW
43	091800	23.8N 133				₽GTW
44	091858	24.1N 133				PGTW
45	091858	24. IN 133				RODH
46	092100	24.4N 133				PGTU
47	100000	24.8N 133			EXP LLCC	PGTW
48	100300	25.1N 133		T5.0/5.0 /S0.0/24HRS	CALLES.	PGTW
49	100601	25.5N 134		10.0, 5.0 , 55.0, 24.10		PCTW
50	100900	25.7N 134				PSTW
51	101200	26.0N 134				PGTU
52	101600	26.3N 134				PGTW
53	101800	26.1N 134				PGTW
54	101846	26.0N 135				PGTW
55	102100	26.4N 135				PGTW
56	110000	26.9N 135				PSTW
57	110300	27.4N 135				PGTW
58	110500	27.7N 135		T4.0/4.5 /WI.0/27HRS		PGTW
59	110900	28.0N 135		14.0/4.3 /WI.0/2/11K3		PGTW
60	111200	28.3N 136				PGTW
61	111600	29.2N 136				PGTW
62						
	111800	29.8N 136				PGTU
63	111834	30.0N 137.				PGTW
64	112100	30.3N 137.			III CC 21 7H 120 05	PGTW
65	120000	31.8N 137.			ULCC 31.3N 138.0E	PGTW
66	120300	32.3N 137.				PGTW
* 67	121800	41.1N 142.				PGTW
* 68	121810	41. IN 142.	.1E PCN 5			RODN

FIX ND.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-Si VEL∕BI			MAX- DIR/						EYE SHAPE			RIEH- ATION			EMP (I		MSN NO.
1	052239	12.8N 143.7E	1500FT		994	45 1		15	270		198	25	8	3							+23	31	1
2	060836	13.3N 142.8E	700MB	3009		35 0	20	50	020		320	90	3	5					+12	+13	+11		2
3	061107	13.6N 142.7E	700MB	3013					300		220	120	5	8									2
4	061801	14.1N 142.2E	780MB	2985					110		060	40	9	5									3
5	062100	14.3N 141.8E	700MB	2987		50 1		45	210			30	9	7					+12	+15	+ 9		3
6	070623	15.2N 140.5E	700MB	2964		60 1		40	230		120	100	5	4									4
(070843	15.5H 140.2E	700MB			50 2		60	140		040	90	5	. 3					+12				4
8	072059	17.1N 138.2E	780MB	2906	978	45 1		30	220		120	80		10	ELL IPTICAL	40	20	149	+15				5
10	080607	18.2N 136.8E	700MB	2832		70 1		90	188		100	75	10	5							+12		~
10	080902	18.7N 136.8E	700MB	2814	968	50 2	96	60	140		030	40		10	CIRCULAR	25			+12	+15	+14		7
11	081805	20.6N 135.2E	700MB	2743					158		700	40	5	3									8
12	082034	21.0N 135.0E	700MB	2786		70 2		15	300		190	20	5	3	ELL IPTICAL	40	30	090	+20	+19	+11		8
13	090600	22.5N 133.7E	700MB	2729		69 0		68	200		120	65	8	5									10
14 15	090848 092102	22.8N 133.6E	700MB	2730	959	55 3		75	288		200	69	.5	5						+17			18
16	092316	24.3N 133.8E	700MB	2777	965	59 9:		78	160		000	90	10	3					+15	+13	+13		11
17	101230	24.7N 133.7E 25.9N 134.4E	700MB 700MB	2791 2793	967	69 3	20	89	020		310	70	10	3									11
18	101230	26.2N 134.4E	700MB		361				130		650	65		10					+12				12
19	102207			2786	000	EE 0	20		350		250	75	10	9							+15		12 13
20	102311	26.8N 135.2E 26.8N 135.2E	700MB	2787	966	55 2:		90	300		210	65	10	2					+15	+10	+14		13
21	110322	27.4N 135.3E	700MB 700MB	2787 2800		65 31 68 31		60 90	360 220		200 130	100 120	5 5	2 5					+15				14
22	110522	27.8N 135.9E	700MB	2798				126	140		030			5					713	T10	+13		14
23	110810	28.0N 136.0E	788MB	2798	000	68 3 65 2		98			248	120	5	5 5						=			14
24	112219	30.9N 136.7E	700MB	2803	966				230			80	5	•					+15 +18				16
25	120203	32.1N 136.9E	700MB		967 964	70 11 75 2		89 88	160 300		040 200	120	4						+10				16
26	120203	34.0N 137.3E	811007	2776	964			48	240			30	3	10									17
20	150101	34.0H 137.3E	regiles	2775	213	75 0	70	40	240	69	130	40	3	3					+ 8	713	A11		11

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	F.YE SHAPE	DIAM	RADOB-CODE ASWAR TODFF	CONTENTS	RADAR POSITION	SITE WMO NO.
1	051835	13.0N 143.8E		POOR					13.6N 144.9E	91218
2	052035	13.0N 143.6E	LAND	POOR					13.6N 144.9E	91218
3	969935	13.5N 143.2E	LAND	FAIR					13.6N L44.9E	91218
4	0 60135	13.6N 143.2E	LAND	FAIR					13.6N 144.9E	91218
5	060235	13.6N 143.2E	LAND	FAIR					13.6N 144.9E	91218
6	120800	34.3N 137.9E	LAND				6//// 5////		34.6N 135.7E	47773
7	120800	34.5N 137.6E	LAND				6//// 4////		35.2N 137.0E	47636
8	120800	34.4N 137.6E	LAND				227/5 53132		35.3N 138.7E	47639
9	120900	34.9N 13B.1E					5///5 73619		35.3N 138.7E	47639
10	121000	35.3N 138.4E					5///5 70124		35.3N 138.7E	47639

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
1	120600	33.9N 138.1E	060	065	umo 47665	
2	120900	34.9N 138.4E	055	025	umo 47696	
3	121200	36.3N 138.3E	050	050	umo 47684	
4	121500	37.7N 138.8E	045	020	umo 47684	
5	121800	39.5N 139.5E	040	025	umo 47582	

TYPHOON KEN BEST TRACK DATA

	BEST TRACK	UARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST	72 HOUR FORECAST
MO/DA/HR	POSIT WIND	POSIT WIND DST WIND		ERRORS POSIT WIND DST WIND	ERRORS
Ø91600Z	17.5 133.7 30	17.8 132.9 30. 49. 0.			POSIT WIND DST WIND
091686Z	17.7 132.3 39	17.8 132.2 30. 8. 0.		19.2 126.4 45, 10945.	19.5 121.3 55. 26855.
0916122	17.8 131.8 35	17.8 131.8 35. 0. 0.		19.2 125.2 50. 14050.	19.5 120.0 60. 30640.
091618Z	18.1 131.1 40			17.8 126.6 50, 146, -50.	17.2 123.2 60. 23140.
091700Z	18.3 130.5 45		18.1 127.9 45. 9540.	17.9 124.5 55. 18745.	17.5 120.8 50. 26950.
091706Z			18.2 128.4 50. 7840.	18.1 125.4 60. 15350.	18.5 122.0 65. 19035.
0917122		18.6 129.9 50. 8. 0.	19.2 127.0 60. 4940.	19.5 124.1 65. 9535.	19.8 120.8 65. 19740.
	19.1 129.6 65	18.9 129.5 50. 1315.	19.8 126.7 60. 2940.	19.8 123.8 65. 8235.	19.5 120.4 65. 23740.
0917182	19.2 129.1 85	19.0 120.0 80. 215.	19.2 125.8 95. 805.	19.0 122.8 100. 144. 0.	18.5 119.4 100. 318. 0.
091800Z	19.5 128.3 90	19.6 128.5 90. 13. 0.	20.4 125.8 100. 1310.	20.7 122.6 115. 84. 15.	21.2 119.4 85. 29710.
091806Z	19.8 127.6 100	20.0 127.0 95. 165.	21.0 124.9 105. 33. 5.	21.2 121.8 115. 130. 10.	21.3 118.4 85. 3585.
091B12Z	20.2 127.0 100	20.2 126.9 100. 6. 0.	20.8 124.8 110. 8. 10.	21.1 122.6 115. 95. 10.	21.1 120.1 90. 269. 5.
091818Z	20.3 126.6 100	20.2 126.3 100. 18. 0.	20.7 124.3 110. 17. 10.	21.0 122.2 110. 118. 10.	21.0 119.5 B5. 300. 5.
091900Z	20.6 125.9 110	20.8 126.0 105. 135.		21.8 122.1 100. 151. 5.	22.1 119.8 80. 300. 5.
0 91906Z	20.6 125.3 100	20.8 125.3 105. 12. 5.		21.9 120.5 90. 244. 0.	21.8 117.7 80. 447, 5,
091912 Z	20.7 124.9 100	20.6 124.8 105. 8. 5.	21.2 123.0 105. 74. 0.	21.8 121.0 90. 219. 5.	21.9 118.4 75. 437. 0.
0919182	20.7 124.6 100	20.8 124.2 105. 23. 5.		22.4 119.8 75. 2895.	24.5 117.7 45, 507, -30,
092000Z	20.8 124.3 100	21.0 124.1 105. 16. 5.	22.4 122.3 110. 155. 15.	24.7 121.9 90. 236. 15.	27.4 122.4 85, 331, 20,
092006Z	20.9 124.1 105	21.2 123.9 110. 21. 5.	22.3 123.5 110. 98. 20.	24.8 122.2 95. 233. 20.	27.7 123.7 85. 307. 15.
0920122	21.0 124.3 105	21.0 124.0 110. 17. 5.	22.2 123.6 110. 87. 25.	24.5 123.7 98. 164. 15.	27.8 125.2 80. 249. 10.
092018Z	21.1 124.3 100	21.0 124.0 110. 18. 10.	22.2 123.6 110. 71. 30.	24.5 123.7 90. 183. 15.	27.8 125.2 80, 273, 5,
092100Z	21.1 124.7 95	21.0 124.8 90. 85.	21.8 124.5 90. 46. 15.	23.2 124.4 90. 175. 25.	25.8 [24.8 85. 331. 5.
092106Z	21.2 124.8 90	21.2 124.6 90. 11. 0.	21.9 124.5 90. 79. 15.	24.2 124.5 90. 216. 20.	27.3 124.7 85. 360. 15.
09 2112Z	21.4 124.9 85	21.8 124.8 90. 25. 5.	. 23.2 125.2 80. 56. 5.	25.6 125.1 70. 222. 0.	28.8 125.0 60. 39610.
092118Z	21.8 124.8 80	21.6 124.8 85. 12. 5.	22.2 !24.7 80. 148. 5.	23.8 124.2 70. 3725.	26.0 123.4 60. 6455.
092200Z	22.2 125.2 75	22.2 125.1 75. 6. 0.	23.8 125.5 70. 107. 5.	25.2 124.6 65. 35515.	26.4 122.3 60. 756. 15.
092206Z	22.6 125.7 75	22.7 125.4 70. 185.	24.7 126.2 50. 12020.	27.0 125.4 35. 33235.	0.0 0.0 00. 0.
Ø92212Z	23.0 126.2 75	23.2 126.2 70. 125.	25.7 127.6 55. 8715.	27.8 128.0 45. 29625.	0.0 0.0 00. 0.
092218Z	23.6 126.9 75	23.5 126.6 70. 185.	25.5 128.0 50. 14225.	28.2 128.8 40. 36125.	0.0 0.0 00. 0.
092300Z	24.2 127.4 65	24.1 127.5 65. 8. 8.	27.2 130.1 50. 4030.	30.2 132.1 40. 3195.	0.0 0.0 00. B.
092306Z	24.8 128.4 70	24.7 128.2 65. 125.	27.5 130.7 50. 10020.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
092312Z	25.7 129.2 70	25.9 129.5 70. 20. 0.	31.9 133.5 50. 8320.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
092310Z	26.8 130.2 75	26.8 130.2 65. 010.	32.8 134.0 50. 8115.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
092400Z	27.7 130.6 80	28.0 130.5 .70. 1910.	33.7 133.4 45. 117. Ø.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
092406Z	29.1 131.2 70	28.9 131.1 70. 13. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
092412Z	31.2 132.1 70	30.8 132.2 70. 25. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
0924182	33.3 132.5 65	33.6 132.8 70. 23. 5.	0.0 0.0 00. 0.	8.0 8.0 80. 8.	0.0 0.0 00. 0.
092500Z	35.5 132.5 45	35.7 132.7 45. 15. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
	· ·•	,			

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 3					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48~HR	72-HR		
AVG FORECAST POSIT ERROR	15.	75.	201.	344.	14.	75.	201.	344.		
AVG RIGHT ANGLE ERROR	9.	49.	134.	263.	9.	49.	134.	263.		
AVG INTENSITY MAGNITUDE ERROR	4.	16.	20.	19.	4.	16.	20.	19.		
AVG INTENSITY BIAS	-1.	-5.	-9.	-10.	-1.	5.	-9.	-10.		
NUMBER OF FORECASTS	37	33	29	25	35	33	29	25		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1647. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 8. KNOTS

TYPHOON KEN FIX POSITIONS FOR CYCLONE NO. 20

F1X NO.	TIME (Z)	FIX POSITION	ACCRY	DVORÁK CODE	COMMENTS	SITE
2	151745	16.1N 134.4E 17.6N 134.6E	DOM E		INIT OBS BASED ON EXTRAP	PGTW PGTW
3	160000	17.4N 132.7E	PCN 6		BASED ON EXTRAP	PGTW
5	160600	17.4N 132.3E	PCN 6	T2.0/2.0 /D1.0/21HRS T1.5/1.5	BASED ON EXTRAP	PG I W PG T W
6	160631	17.5N 131.9E	PCN 5	T1.5/1.5	BASED DH EXTRAP INIT DBS ULCC FIX ULCC FIX ULCC FIX ULCC FIX ULCC FIX ULCC FIX BASED ON EXTRAP	RPOK
8	161200	17.7N 132.3E	PCN 6		ULCC FIX	PG FW PG FW
9	161600	17.9N 131.1E	PCH 6		ULCC FIX	PGTW
11	161888	17.9N 132.5E 17.9N 131.1E 18.0N 131.0E 17.8N 130.9E 17.9N 130.8E	PCN 5		ULCC FIX ULCC FIX	PG TW PG TW
12	162106	17.9N 130.8E	PCH 6		ULCC FIX	PGTW
13	170000	18.2N 130.6E	PEN 6	T3.0/3.0 /D1.0/27HRS	BASED ON EXTRAP	PGTW PGTW
15	178618	18.6N 130.1E	PCN 5	T3.0/3.0 /D1.0/27HRS T4.5/4.5 /D1.5/21HRS		RUMK
16 17	170900	18.8N 129.3E	PCN 6			PGTW PGTW
18	171600	18.9N 129.0E	PCN 6			PGTW
19 29	171800	19.2N 128.8E	PCN 2			PGTW PGTW
21	180000	19.7N 128.4E	PCN 2			PGTW
22 23	180300	19.8N 127.9E	PCN 2	T4.5/4.5 /D1.5/21HRS		PGTW PGTW
24	180900	20.1N 127.2E	PCN 2			PSTW
25	181200	20.1N 127.0E	PCN 2			PGTW PGTW
27	181800	20.1N 126.5E	PCN 4			PGTW
28	190000	20.5N 125.8E	PCN 2	TE 0 /E 0 /D0 E /O4UDC		PGTW
30	190554	20.5N 125.1E	PCN 1	T5.0/5.0 /D0.5/24HRS T5.5/5.5	INIT OBS	PGTW RODN
31	190600	20.4N 125.2E	PCN 4			PGTW
32 33	190900	20.5N 125.0E 20.7N 124.8E	PCN 4			PGTU PGTU
34	191600	20.3N 123.8E 20.7N 124.8E 20.7N 124.5E 20.8N 124.5E 20.9N 124.6E	PCN 4			PGTW
35 36	191888	20.8N 124.5E 20.9N 124.6E	PCN 4 PCN 1			PGTW RODN
31	192100	21.0N 124.5E	PEN 4			PGTU
38 39	200000 200300	20.8N 124.2E	PCN 2	T5.5/5.5 /D0.5/24HRS		PGTW PGTW
40	200542	20.9N 124.2E	PCH 1	T6.0/6.0	INIT OBS	RPIK
41	200600 200900	21.0N 124.0E	PCN 2	T5.5/5.5 /D0.5/24HRS T6.0/6.0	•	PGTW PGTW
43	201200	21.0N 124.3E	PUN 2			PGT₩
44 45	201600	20.8N 124.3E	PCN 2			PGTW PGTW
46	202100	20.8N 124.3E 21.1N 124.4E 20.9N 124.6E	PCN 2			PGTW
47 48	210000	20.9N 124.6E	PCN 4	T5.0/5.5+/W0.5/24HRS		PG TW PG TW
49	210600	21.6N 124.8E	PCN 4	1310/ 313 // WG13/ Z-HING		PGTU
58 51	210900	21.8N 124.9E 21.7N 124.9E	PCN 4			PGTW PGTW
52	211600	21.6N 124.8E	PCH 4			PGTW
53 54	211800	21.6N 125.0E 21.6N 125.2E	PCH 4 PCH 4			PGTW PGTW
	220000	22 111 125 25	DOM: 4		ULCC FIX	PGTW
56 57	220300	22.4N 125.4E	PCN 4			PGTU
58	220600	22.5N 125.8E	PCN 4	T4.0/4.5 /WI.0/27HRS T4.5/4.5		PGTW PGTW
59 60	220700	22.6N 125.7E	PCN 3	T4.5/4.5	INĮT OBS	RPMK PGTW
61	221200	23.0N 126.1E 23.2N 126.3E	PUN 4		EXP LLCC	PGTW
62 63	221600	23.2N 126.3E 23.3N 126.5E	PCN 4 PCN 3			PGTW PGTW
64	222100	23.6N 127.3E	PCN 4	4		PGTW
65	230866	24.1N 127.3E	PCN 4			PGTIJ
66 67	230300 230506	24.4N 127.5E 24.7N 128.0E	PCN 4 PCN 3			PGTW PGTW
68	230600	24.9N 128.3E	PCN 4	T4.0/4.0-/50.0/24HRS		PG TW
69 78	230648 230900	24.8N 128.5E 25.4N 128.8E	PCH 3 PCH 4	T4.5/4.5 /S0.0/24HRS		RPMK PGTW
71	231200	25.8N 129.3E	PCN 4		END ILEC	PGTW
72 73	231600 231751	26.4N 129.9E 26.7N 130.1E	PCN 4 PCN 3		EXP LLCC	PGTW PGTW
74	232100	27.2H 130.5E	PCH 4			PGT₩
75 76	240000 240300	27.7N 130.9E 28.0N 131.0E	PCN 4 PCN 4			PGTW PGTW
77	240453	29.3N 131.4E	PCN 1	T4.8/4.8 /W0.5/22HRS		RP11K
78 79	240600 240900	29.0N 131.5E 30.0N 132.3E	PCN 4 PCN 4	T4.0/4.0-/S0.0/24HRS		PGTW PGTW
80	241200	31.0N 132.5E	PCN 4			PGTW
81 82	241600 241738	32.9N 132.6E 33.2N 132.6E	PCN 4 PCN 3		ULCC FIX	PGTW PGTW
83	241930	33.8N 134.2E	PCN 5	T4.8/4.5 /W0.5/24HRS	ondo i sn	RPMK
84	242100	35.3N 132.4E	PCN 6			Wraq

FIX	TIME	F1X	FLT 70	IOMB ORS	MAX-SFC-UND	MAX-FLT-LVL-M	ND ACCRY	EYE	EYE ORIEN-	EYE TEMP	(C) MSN
NO.	(Z)	POSITION		IGT MSLP	VEL/BRG/RNG	DIR/VEL/BRG/R				OUT/ IN/ DP	
1 2 3 4 4 5 6 7 8 9 100 111 12 13 4 15 5 16 7 18 19 20 21 22 34 4 22 6 27 8 29 30 31 33 33 33 33 33 33 33 33 33 33 33 33	160814 168851 170823 170646 170837 17198 180688 182083 182249 190613 1908513 190863 200902 20203	17.7N 132,7E 17.8H 132,2E 18.4H 130,4E 18.9N 130,0E 19.3N 129,0E 19.3N 129,0E 19.3N 129,127,3E 20.6N 127,3E 20.6N 126,2E 20.6N 125,1E 20.6N 125,1E 20.6N 124,4E 21.0N 124,2E 21.0N 124,2E 21.0N 124,2E 21.1N 124,3E 21.1N 124,3E 21.1N 124,3E 21.1N 124,2E 21.2N 125,2E 21.3N 124,3E 21.3N 127,4E 22.7N 125,0E 22.7N 125,0E 22.8N 126,0E 23.8N 127,4E 25,7N 129,2E 25,5N 130,3E 27.9N 130,7E 33,7H 132,1E	1500FT 700HB 30 700HB 29 700HB 29 700HB 25 700HB 26 700HB 25 700HB 25 700HB 26 700HB 27 700HB	198 198	35 050 65 35 020 35 45 348 11 50 278 18 45 318 56 100 240 7 100 150 16 100 360 10 100 360 10 65 070 66 60 260 80 60 260 80 60 360 20 60 360 20 60 300 100 70 220 78 55 360 83 60 100 120 70 240 120 80 210 60 55 300 120 70 220 92	128 35 036 1 248 39 159 039 46 310 039 46 310 128 88 010 050 92 088 239 88 160 050 92 188 050 93 186 050 97 310 050	45 8 15 3 10 2 2 2 1 1 3 2 5 2 3 1 2 2 2 1 1 2 2 5 2 3 1 2 2 2 1 1 3 2 5 2 3 1 2 2 3 4 2 2 1 1 2 5 5 5 5 6 10 3 3 5 5 7 6 10 3 3 5 5 7 7 7 3 3 5 5 5 5 6 10 3 3 3 5 7 7 5 5 5 5 6 10 3 3 3 5 5 5 5 5 6 10 3 3 3 5 5 5 5 5 6 10 3 3 3 5 5 5 5 5 6 10 3 3 3 5 5 5 5 6 10 3 3 3 5 5 5 5 5 6 10 3 3 3 5 5 5 5 5 6 10 3 3 3 5 5 5 5 6 10 3 3 3 5 5 5 5 6 10 3 3 3 5 5 6 10 3 3 5 5 5 5 5 6 10 3 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 5 6 10 3 3 5 6 10 3 5 6 10	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR ELLIPTICAL CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	15 35 40 30 15	+24 +25 +24 +18 +22 +22 +12 +16 +14 +13 +14 +11 +18 +14 +16 +12 +16 +12 +11 +17 +8 +11 +18 +12 +28 +23 +10 +18 +17 +14 +16 +16 +14 +16 +17 +13 +14 +19 +14 +12 +15 +15 +11 +12 +12 +18 +10 +10 +11 +11 +10 +11 +11 +10 +11 +11 +13 +12 +18 +13 +15 +12 +13 +14 +13 +11 +13 +12	28 2 3 4 4 4 5 5 6 6 7 7 7 7 7 8 8 9 9 18 11 11 12 12 12 14 14 15 15 15 16 16 17 17 18 18
-	241105	J	TOOLD NO		RADAR	FIXES	., .				
FIX NO.	TIME (Z)	FIX POSITION	RADAR ACCR	EYE Y SHAPI		RADOB-CODE ASWAR TDDFF		COMENTS		RADAR POSITION	SITE WMO NO.
23 24 25 26 27 28 29 30 31	232200 232300 232300 240000 240100 240300 240400 240500 240600	20. 2N 124. 9E 20. 2N 124. 9E 20. 8N 124. 2E 21. 6N 124. 4E 21. 3N 124. 4E 21. 3N 125. 4E 23. 3N 125. 4E 23. 3N 126. 6E 23. 6N 126. 7E 24. 9N 127. 2E 24. 1N 127. 3E 24. 1N 127. 8E 24. 1N 128. 4E 24. 1N 128. 4E 24. 1N 128. 4E 24. 1N 128. 5E 27. 1N 130. 1E 27. 1N 130. 5E 27. 4N 130. 5E 27. 4N 130. 5E 27. 4N 130. 5E 27. 4N 130. 5E 27. 6N 130. 6E 27. 1N 130. 7E 27. 1N 130. 7E 27. 1N 130. 7E 28. 2N 131. 1E 28. 7N 131. 2E 28. 6N 131. 1E 28. 7N 131. 2E	LAND LAND LAND LAND LAND LAND 6 LAND LAND LAND LAND LAND LAND LAND LAND	•		359/4 70008 359/4 4008 15/// 63096 15/// 63096 15/// 63096 354/3 4//// 353/3 50080 6///4 5//// 6//// 58488 6591/ 70699 6591/ 70699 6591/ 70699 6591/ 70699 6591/ 70612 20912 70612 20912 70613 21912 70613 21912 70613 65/// 50316 65/// 50316 65/// 50316 65/// 50316 65/// 70216 65/// 50316 55/// 30316 55913 50508 50913 50613 51912 50213 51912 50213 51912 50213 55/// 50311 55/// 50314				0.4N 122.0E 0.4N 122.0E 0.4N 122.0E 0.4N 122.0E 0.4N 122.0E 0.4N 122.0E 0.4N 127.0E 6.2N 127.0E 8.4N 129.5E 8.4N 129.5E	98136 98136 98136 98136 98136 98136 98136 47927 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47937 47939 47939 47939 47939 47939 47939 47909
	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE)	CONMENTS					
2	241800	26.6N 130.1E 33.2N 132.5E 34.0N 132.6E	065	080 050 020	umo 479 umo 478 umo 477		UMO 47887				

TROPICAL STORM LOLA BEST TRACK DATA

	BEST	TRACK			WARN I		RORS		24 HC	UR FO	RECAS			48 HI	OUR F	DRECAS ERROS			72 HO		RECAS	T
MO/DA/HR	POSIT	1.17.17	000					200	~				nor									
		MIND	POS		MIND	DST	WIND	POS		MIND	DST	MIND	POS		MIND		MIND	POS		MIND		MIND
091500Z	22.0 168.1	25	0.0	0.0	8.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
091506Z	22.7 166.9	25	0.0	0.0	Ð.	-0.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	Ø.	-0.	0.
091512Z	23.3 165.7	30	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-8.	e.	0.0	0.0	8.	-0.	ø.
091518Z	24.0 164.7	30	0.0	0.0	9.	-0.	0.	0.8	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	8.	0.0	9.0	8.	-0.	ø.
091600Z	24.5 163.5	35	0.0	0.0	8.	-0.	0.	0.8	0.0	0.	-0.	0.	0.0	9.8	8.	-0.	0.	0.0	0.0	ø.	-0.	ø.
091606Z	25.1 162.3	35	25.2	162.3	30.	6.	-5.	28.5	158.2	45.	52.	-5.	33.2	159.1	55.	105.	10.	0.0	9.0	a.	-0.	ø.
Ø91612Z	25.6 161.3	49	25.6	161.3	30.	ø.	-10.	28.6	158.2	45.	34.	-5.	33.2	159.1	55.	211.	10.	0.0	0.0	ø.	-0.	ø.
091618Z	26.2 160.3	45	26.2	160.3	30.		-15.	29.7	158.0	45.	48.	8.	34.5	160.0	50.	322.	5.	0.0	0.0	۵.	-0.	ø.
091700Z	26.9 159.5	45	27.5	159.3	35.		-10.	33.7	160.2	50.	152.	5.	40.0	172.3	40.	289.	e.	0.0	8.0	ø.	-0.	a.
091706Z	27.9 158.9	50	28.5	159.0	45.	36.	-5.	35.5	162.2	45.	190.	0.	0.0	0.0	0.	-0.	ø.	0.0	9.0	ø.	-0.	ø.
091712Z	28.8 158.8	50	28.6	159.2	50.	24.	0.	35.0	162.8	45.	93.	0.	0.0	0.0	Ð.	-8.	0.	0.0	0.0	ø.	-0.	ø.
091718Z	29.9 158.9	45	30.0	159.3	45.	22.	0.	35.8	166.6	45.	98.	ø.	0.0	0.0	8.	-0.	ø.	0.8	0.0	Ñ.	-0.	0.
0918002	31.2 159.7	45	31.4	160.5	50.	43.	5.	36.2		40.	43.	ø.	0.0	0.0	Ø.	-8.	ø.	8.0	8.8	ø.	-0.	ø.
091806Z	32.5 161.0	45	32.2	161.2	45.	21.	ø.	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-0.	9.	0.0	0.0	ñ.	-0.	ø.
0918127	33.5 163.3	45	33.7	163.1	45.	16.	Ñ.	8.8	0.0	Đ.	-8.	ø.	0.0	0.0	8.	-0.	Ð.	0.0	0.0	ñ.	-0.	ø.
Ø91818Z	34.3 166.5	45	34.2	166.3	45.	12.	Ñ.	0.0	0.0	ø.	-ē.	ø.	0.0	8.8	Ñ.	-0.	ø.	8.8	0.0	A.	-0.	ø.
091900Z	35.5 170.1	40	35.0	170.0	40.	30.	а.	8.8	0.0	P.	~B.	ø.	0.0	0.0	a.	-B.	ø.	0.0	0.0	9.	9.	в.
0212005	33.3 110.1	40	33.0	170.0	40.	30.	o.	0.0	0.0	٥.	0.	٠.	0.0	0.0	о.	-0.	o.	0.0	0.0	9.	٠.9.	ь.

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1424. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 15. KNOTS

TROPICAL STORM LOLA FIX POSITIONS FOR CYCLONE NO. 21

SATELLITE FIXES

FIX	TIME	FIX	40001	NICEOU CORE	COMMENTS	SITE
ND.	(Z)	POSITION	ACCRY	DVORAK CODE	COMMENTS	2115
1	150318	22.5N 167.9E	PCN 6	T1.5/1.5	INIT OBS ULCC FIX	KGWC
2	151603	24.1N 164.5E	PCN 6		ULCC FIX	KGWC
3	151604	24.1N 164.3E	PCN 6			PGT₩
4	152100	24.4N 163.9E	PCN 6		ULCC FIX	PGTW
5	160000	24.2N 163.4E	PCN 6	T2.0/2.0	INIT OBS	PGTW
6	160300	24.8N 162.8E	PCN 6			PGTW
7	160600	25.2N 162.3E	PCN 6			PGTW
8	160900	25.0N 161.7E	PCN 6			PGTW
9	161600	26.0N 161.0E	PCN 6			PGTW
10	161800	26.2N 160.8E	PCN 6			PGTW
11	162100	26.8N 159.8E	PCN 6			PGTW
12	170000	26.8N 159.5E	PCN 6	T3.0/3.0 /D1.0/24HRS		PGT₩
13	170436	27.8N 158.9E	PCN 6			PGTW
14	170600	27.8N 158.9E	PCN 6			, PGTW
15	170900	28.1N 159.4E	PCN 6			PGT⊍
16	171200	20.7N 159.1E	PCN 6		ULCC FIX	PGT₩
17	171600	29.5N 159.2E	PCN 6			PGTW
18	171800	30.3N 159.6E	PCN 6			PGTW
19	172100	30.0N 159.9E	PCN 6			PGTW
20	180000	30.9N 159.4E	PCN 4	T3.0/3.0 /S0.0/24HR5		PGT₩
21	180424	31.9N 160.BE	PCN 3			PGTW
22	180600	32.4N 161.2E	PCH 4			PGTW
23	180900	32.8N 162.2E	PCN 6			₽GTW
24	181200	33.3N 162.9E	PCN 6			PGTW
25	181600	33.5N 165.5E	PCN 6			PGTW
26	181800	34.1N 166.3E	PCN 6			PG™
27	182100	34.5N 168.1E	PCN 6			PGTW
28	190000	36.0N 170.9E	PCN 6	T2.0/2.5 /W1.0/24HRS		PGTW

TROPICAL DEPRESSION 22 BEST TRACK DATA

BEST TRACK	WARNING ERRORS	24 HOUR FORECAST ERRORS	48 HOUR FORECAST ERRORS	72 HOUR FORECAST ERRORS			
MO/DA/HR POSIT WIND	POSIT WIND DST WIND	POSIT WIND DST WIND	POSIT WIND DET WIND	MIND TEG DRIW TEOP			
092106Z 18.6 139.3 30	18.2 139.5 30. 27. 0.	19.6 136.9 40. 155. 15.	0.0 0.0 00. 0.	8.0 0.0 00. 0.			
092112Z 19.8 138.8 30	18.9 139.5 30. 67. Ø.	0.0 0.0 80. 9.	6-0 0.0 U. 0. 9.	0.0 0.0 00. 0.			
0921182 20.7 137.8 30	21.0 138.5 30. 43. 0.	8.9 8.9 99. C.	0.0 0.0 00. 0.	0.0 0.0 00. 0.			
0922002 21.2 136.6 30	21.4 136.6 30. 16. 0.	0.0 0.0 00. c.	0.0 0.0 0. -0. 0.	0.0 0.0 00. 0.			
092206Z 22.1 136.2 25	22.3 135.9 20. 215.	0.0 0.0 O0, O.	0.0 0.0 00. 0.	0.0 0.0 00. 0.			

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	URNG	24-HR	48-HR	72-HR	LIPHG	24~HR	48~HR	72-HR		
AVG FORECAST POSIT ERROR	35.	155.	0.	0.	8.	0.	0.	0.		
AVG RIGHT ANGLE ERROR	21.	83.	0.	0.	e.	0.	0.	ø.		
AVG INTENSITY MAGNITUDE ERROR	1.	15.	0.	Ð.	8.	0.	8.	0.		
AVG INTENSITY BIRS	-1.	15.	0.	0.	e.	Ø.	0.	0.		
NUMBER OF FORECASTS	5	1	6	8	8	0	Р	0		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 282. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 12. KNOTS

TROPICAL DEPRESSION TD22 FIX POSITIONS FOR CYCLONE NO. 22

SATELLITE FIXES

F1X NO.	TIME (Z)	F1X POSITION	ACCRY	DVORAK CODE	CONTENTS	SITE
1 2 3 4 5 6 * 7 * 8 9	210000 210300 210600 210900 211200 211600 211800 212100 220000 220300	17.4N 139.8E 18.1N 139.6E 18.4N 140.0E 18.8N 140.0E 19.5N 139.4E 21.2N 136.0E 21.0N 139.5E 21.4N 136.7E 21.2N 137.0E 21.2N 137.0E	PCN 6 PCN 4 PCN 4 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6 PCN 6	T1.0/1.0 T1.0/1.0 /S0.0/24HRS	INIT OBS	PGTW PGTW PGTW PGTW PGTW PGTW PGTW PGTW

AIRCRAFT FIXES

FIX NO.	TIME (Z)	F1X POSITION	FLT LVL		MAX-FLT-LVIUND ACCRY DIR/VEL/BRG/RHG NAV/MET	EYE SHAPE	EYE ORIEN- DIAM/TATION	EYE TEMP (C) OUT/ IN/ DP/SST	MSN NO.
1 2		16.7N 140.5E 21.1N 136.9E	1500FT 1500FT		828 22 288 58 12 12 258 18 368 18 12 5			+27 +25 25 +25 +25 +25 27	1 2

SUPER TYPHOUN MAC REST TRACK DATA

BES	WARHING	nhone	24 H	DRECAST	48 H	OUR FI	ORECAST	72 HOUR FORECAST ERRORS					
MO MA AIR DOCKT			RRORS			ERRORS			ERRORS				
MO/DA/HR POSIT	WIND POSIT		T WIND	POSIT	MIND	DST WIND	POSIT	MIND	DST WIND	POSIT	MIND	DST	
1001002 11.8 15		0.0 00		6.0 0.0		-0. 0.	0.0 0.0		-0. 0.	9.8 0.6		-9.	0.
1001062 11.9 15).0 O6		0.0 0.0		-0. 0.	0.0 0.0		-0. 0.	8.0 0.0		-0.	0.
1001122 12.0 150				13.3 147.3		6710.	14.0 144.3		8440.	14.0 141.4		113.	
1001182 12.0 149	3.4 30 12.4 149	3.1 30. 30	. Ә.	13.0 145.6	45.	27 <i>.</i> -5.	13.4 142.8	55.	5935.	13.8 139.6	65.	123.	-65.
1002002 12.1 148	3.5 30 11.9 149	3.5 30. 12	. 0.	12.2 146.3	45.	11815.	12.7 144.5	55.	21145.	13.6 143.2	2 65.	321.	-75.
100206Z 12.5 147	.5 40 12.4 147	7.5 40. 8	. 0.	13.4 143.8	50.	820.	14.9 141.8	60.	7050.	17.0 140.6	70.	174.	-65.
1002122 12.6 146	.4 45 12.8 146	5.5 40. 13	5.	13.8 143.2	55.	1830.	15.5 141.1	65.	6560.	18.2 138.8	80.	91.	-50.
1002182 12.6 145	.4 50 12.9 145	.4 45. 18	. <i>-</i> 5.	14.3 142.4	65.	1325.	16.0 140.0	90.	6040.	17.2 136.1	115.	44.	-10.
100300Z 13.1 144	1.5 60 12.8 144	1.7 55. 21	5.	13.2 141.6	75.	7925.	13.8 138.2	95.	13845.	14.5 134.3	105.	265.	-10.
100306Z 13.3 143	3.7 70 13.3 143	3.7 70. 8	. 0.	14.0 139.8	110.	76. 0.	14.6 135.7	125.	16310.	15.2 131.6	140.	346.	20.
100312Z 13.7 142	.9 85 13.7 142	2.8 85. 6	. 0.	14.8 139.2	115.	5510.	15.8 135.3	130.	120. 0.	16.8 131.5	130.	310.	ø.
1003182 14.2 142	.2 90 14.1 142	2.2 90. 6	. 0.	15.8 138.6	120.	2410.	17.3 134.8	130.	93. 5.	19.1 131.2			5.
1004002 14.5 14	.4 100 14.5 14	1.2 90. 12	10.	16.0 137.9	100.	2440.	17.3 134.5	110.	1165.	19.3 131.3		281.	ø.
100406Z 15.0 140			15.	16.5 137.8	105.	1330.	17.9 134.8	115.	1095.	19.3 131.3		352.	10.
1004122 15.3 146			. 0.	17.8 138.8		120. 0.	19.9 138.2		16115.	22.0 138.0			-15.
1004182 15.7 139	.0 130 16.2 139	9.0 130. 30	. е.	19.4 137.6	135.	116, 10.	22.2 137.2	115.	12210.	24.7 137.2	95.	88.	-15.
100500Z 16.1 136				17.9 135.6		48. 5.	20.2 133.8		14010.	22.4 132.9			-10.
100506Z 16.6 137				18.3 135.1		815.	20.7 133.5		20810.	23.1 132.8		502.	-5.
1005127 17.2 136				19.1 134.4		9615.	21.7 133.1		22810.	24.1 132.6		597.	-5.
1005182 17.9 136				20.2 133.8		10320.	22.5 132.9		30015.	24.8 132.4		735.	~5.
100600Z 18.6 136				21.8 134.2		6820.	26.5 134.1		19025.	34.0 139.2			-20.
190606Z 19.6 135				22.2 134.2		11415.	25.3 133.9		36129.	32.8 138.4			-15.
100612Z 20.4 135				25.8 135.2		8710.	31.8 139.2	90.	4310.	0.0 0.0		-0.	e.
100618Z 21.2 135				25.9 135.2		82 10.	32.0 139.5	90.	1695.	0.0 0.0		-0.	ø.
1007002 22.0 135				26.2 136.0		11710.	32.8 142.3		146. 5.	9.0 0.0		-ø.	ø.
100706Z 23.5 139				30.9 149.4		12310.	36.2 157.2	60.	53220.	0.0 0.0		-0.	ø.
100712Z 24.5 135				31.8 141.6	90.	8310.	0.0 0.0	a.	-0. 0.	8.0 0.0		-8.	В.
100718Z 26.1 136				33.7 145.2		14115.	0.0 0.9		-8. 8.	0.0 0.0		-8.	0.
100800Z 27.7 137				35.2 149.2		2495.	0.0 0.0	ø.	-8. 8.	0.0 0.0		-0.	0.
100806Z 29.8 136				36.0 153.8		36710.	6.0 0.0	ø.	-0. 0.	0.0 0.0		-0.	ø.
1008127 31.6 148				9.9 9.9	0.	-0. 0.	0.0 0.0	ø.	-8. 8.	0.0 0.0		-0.	ø.
1008182 33.4 142				0.6 0.0	A.	-8. 8.	0.0 0.0	ø.	-0. 0.	0.0 0.0		-0.	0.
100010Z 33.4 142				0.0 0.0	В.	-0. 6.	0.0 0.0	ø.	-8. 8.	0.0 0.0		-0.	0.
100906Z 35.4 146				8.0 8.8	Ð.	-0. 0. -0. 0.	6.6 6.6	о. О.	-8. 8.	0.0 0.0		-ø. -0.	ø.
1007004 33.4 146	.3 80 35.2 146	00. 12	. 0.	9.9 9.9	υ.	~ບ. ອ.	0.0	υ.	-o. o.	0.0 0.0	ь.	~⊌.	٠.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER					
	WRNG	24~HR	48-HR	72-HR	wrng	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	14.	90.	162.	294.	13.	90.	162.	294.		
AVG RIGHT ANGLE ERROR	13.	63.	104.	149.	12.	63.	104.	149.		
AVG INTENSITY MAGNITUDE ERROR	2.	14.	21.	24.	3.	14.	21.	24.		
AVG INTENSITY BIAS	-2.	-13.	-20.	-20.	-2.	-13.	-20.	-20.		
NUMBER OF FORECASTS	32	28	24	20	29	28	24	20		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2287. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

12. KNOTS

SUPER TYPHOON MAC FIX POSITIONS FOR CYCLONE NO. 23

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVORAK CODE	COMENTS	SITE
	010000	10 54 150 05	PCN 6	T1.0/1.0	INIT OBS.	PGTW
	010300	12.5N 152.0E 12.4N 151.5E	PCN 6	11.0/1.0	INTI ODS:	PGTW
2						PGTW
3	010510	12.6N 151.0E	PCN 5			PGTW
4	010600	12.5N 150.8E	PCH 6			
5	010900	12.7N 151.0E	PCN 6		ULAC FIX	PGTW
6	911200	12.7N 150.1E	PCH 6			PG™
7	011600	12.2N 149.1E	PCN 6			PGT₩
8	011800	12.0N 148.7E	PCH 6		•	PGTW
9	012100	12.0N 148.4E	PCN 6			PGTW
10	020000	11.8N 148.6E	PCN 6	T2.0/2.0 /D1.0/24HRS		PGTW
11	020300	12.2N 148.8E	PCN 6		BASED ON EXTRAP	PGTW
12	929458	12.8N 147.6E	PCN 5			PGTU
13	020600	12.6N 147.4E	PCN 6		•	PGTW
14	020900	12.9N 146.8E	PCN 6		BASED ON EXTRAP	PGTW
15	021200	12.9N 146.2E	PCN 6			PGTW
16	021600	12.6N 145.3E	PCN 6			PGTW
17	021743	12.6N 145.6E	PCN 5			PGTW
18	021800	12.6N 145.5E	PCN 6			PGTW
19	022100	12.9N 144.9E	PCN 6			PGTW
20	939999	13.1N 144.7E	PCN 6	T4.0/4.0+/D2.0/24HRS		PGTW
			PCN 4	14.0/ 4.0 / DE.O/ Z4IKS		PGTW
21	939399	13.3N 144.2E				PGTW
22	030446	13.4N 143.9E	PCN 4			PGTW
23	030600	13.4N 143.8E	PCN 2			
24	030900	13.6N 143.4E	PCN 2			PGTW

25	031200	13.6N 143.0E	PCN 4			PGTW
26	031600	14.1N 142.3E	PCH 4			PGTW
27	031731	14.3N 142.0E	PCN 3			PG FW
28	031800	14.3N 142.0E	PCN 4			PGTW
29	032100	14.3N 141.7E	PCN 4			PGTW
30	040000	14.5N 141.5E	PCH 2	T5.0/5.0 /D1.0/24HRS		PGTW
31	040300	14.8N 141.1E	PCN 2	1510/510 / D110/ E-1103	EYE DIN 20NM	PGTU
32	040434	15.0N 140.7E	PCH 1		EYE DIA 20NM	PGTW
33	040600	15.1N 140.6E	PCN 2		LIL SIN ZOWI	PGTW
34	040900	15.2N 140.3E	PCN 2		EYE DIA 20NII	PGTW
35	941200	15.5N 140.0E	PCN 2		ETE DIN 20MT	PGTW
36	041600	15.7N 139.2E	PCN 2			PGTW
37	041719	16.1N 139.1E	PEN 1			PCTU
						PGTW
38	041800	15.8N 139.1E	PCN 2			
39	042100	16.0N 138.7E	PCH 2			PGTW
40	050000	16.3N 138.4E	PCN 2	T6.0/6.0 /D1.0/24HRS		PGTW
41	050300	16.5N 138.0E	PCN 2			PGTW
42	050604	16.7N 137.8E	PCN 1			PGTW
43	050900	17.1N 137.2E	PCN 2		EYE DIA 15NM	PGTW
44	051200	17.4N 137.0E	PCN 2			PGTW
45	051500	17.6N 136.1E	PCN 4			PGTW
45	051800	17.8N 136.0E	PCN 4			PGTU
47	052100	18.3N 136.0E	PCH 4			PGTW
48	060000	18.5N 136.1E	PCN 2	T5.0/6.0 /W1.0/24HRS		₽GTW
49	660466	19.2N 135.7E	PCN 2			PGTW
50	060552	19.6N 135.7E	PCN 2			PGTW
51	060900	20.0N 135.6E	PCN 2			PGTW
52	961299	20.4N 135.4E	PCN 2			PGT₩
53	061600	20.8N 135.2E	PCN 2			PGTW
54	961800	21.1N 135.1E	PCN 2			PGTW
55	062100	21.4N 135.3E	PCN 2			PGTW
56	070000	21.8N 135.5E	PCN 2	T6.0/6.0-/D1.0/24HRS		PGTW
57	070400	22.8N 135.7E	PCN 2			PGTW
58	070540	23.4N 135.8E	PCH 1			PGTW
59	070900	23.9N 135.9E	PCN 2			PGTW
60	071200	24.5N 136.1E	PCN 2			PSTW
61	071600	25.5N 136.5E	PCN 2			PSTU
62	071800	26.0N 136.6E	PCN 2			PGTW
63	072100	26.9N 137.0E	PCN 2			PGTW
64	080000	27.6N 137.5E	PCN 2	T5.0/5.0 /W1.0/24HRS		PGTW
65	080400	28.9N 138.2E	PCN 2	13.0/3.0 / WI:0/2-HING		PGTW
66	080527	29.7N 138.5E	PCN 1			PGTW
67	080900	30.7N 139.4E	PCN 6			PGTW
68	081200	31.4N 140.0E	PCN 4			PGTW
69			PCN 4		ULCC F1X	PGTU
	081600	33.2N 142.1E			ULCC FIX	PG (U)
* 70	081812	34.0N 143.7E	PCN 5		OLCC FIA	PGTW
71	002100	33.9N 143.4E	PCN 4	T7 E /4 E AU E /3/4/00	ULCC FIX	PGTU
72 73	090000	34.1N 144.1E	PCN 4	T3.5/4.5 /U1.5/24HRS	OLCE PIA	PGTW
13	090400	35.1N 145.6E	PCH 4			r610

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-9			MAX-				ACC		EYE SHAPE			RIEH- ATION			MP (E		MSN NO.
nu.	(2)	FUSTITUM	LVL	nuı	ISLF	VELZE	ORGZ	KIIG	DIKA	VEL,	DKG/	KIIG	11111 47	12.	JAN L	יוע	31 11	1111011	0012	1117	1472	,	
1	012204	11.9N 148.8E	1500FT		1000	30 6	950	20	120	36	939	24	7	2					+24	+23	+23	30	1
ž	020130	12.2N 148.3E	1500FT		1000	25 2		20	290		220	14	7	5								30	i
3	020601	12.4N 147.5E	1500FT		993	45		20	220		148	20	10	10					-				
4	020902	12.5N 146.9E	700MB	3050	1002				170		070	15	5	5					+ 8	+13	+11		2 3 3 3
5	021505	12.7N 145.8E	786MB	2980					169	44	090	10	5	2					+10	+14			3
6	021800	12.6N 145.4E	700MB	2929					100	57	090	5	5	1	ELL IFTICAL	17	12	090					3
7	022005	12.8N 145.2E	700MB	2920	981	30 2	290	90	020	51	020	10	5	2	ELL IPTICAL	22	12	150	+11	+16	+13		3
8	030133	13.2N 144.4E	700MB	2810	966	87 6	030	5	140	79	040	7	5	2	ELLIPTICAL	15	10	120	+12	+15	+14		
9	030600	13.3N 143.7E	700MB	2751		69 6	948	10	160	77	040	8	4	3						+17	+10		4 5 5 7
10	030820	13.5N 143.4E	700MB	2799	955	69 :	150	30	989	98	350	11	5	2	ELL. IPTICAL	18	8	090	+14	+18	+13		5
11	031211	13.8N 142.0E	700MB	2692					100	82	0 70	-12	8	1									
12	031436	13.9N 142.6E	700MB	2688	954				200		130	19	5	1	CIRCULAR	8				+15			7
13	032015	14.2N 141.8E	700MB	2690	954	90 3	360	10	359	45	268	35	15	2	CIRCULAR	30				+15			8 9
14	040850	15.6N 139.9E	700MB	2331	989	100	330	6		104		18	25	1	CIRCULAR	15			+11	+29	+ 1		9
15	941156	15.2N 140.0E	700MB	2291						112		18	15	1									9
16	042197	15.9N 138.6E	700MB	2173	895	100	360	7		102		8	. 5	1	CIRCULAR	12				+24	+10		10
17	051009	17.1N 137.1E	700MB	2273	968				130		020	15	5	2	CONCENTRIC	97	40		+10	+21			11
18	051249	17.4N 136.7E	700MB	2350					210		130	25	8	2									11
19	051924	18.0N 136.3E	700MB	2372					230		110	20	19	5									12
20	052219	18.3N 136.0E	700MB	2383	920	89 6		10		110		35	10		CONCENTRIC	12	25		+11	+17	+16		13
21	060704	19.8N 135.6E	700MB	2396		60 (050	10	190			25	ខេ	3									15
22	060931	20.1N 135.5E	700MB	2332	914					100		25	15	5	CIRCULAR	25			+12	+20	+12		15
23	061913	21.2N 135.3E	700MB	2314					100		939	10	5	5									16
24	062145	21.6N 135.3E	700MB	2346	918	50 (048	90		100		30	5	5	CIRCULAR	25				+17			16
25	070937	24.0N 135.8E	700MB	2421	924					110		25	19	2	CIRCULAR	30			+13	+17	+15		18
26	071214	24.6N 135.9E	780MB	2441					100		ษรษ	30	10	2									18
27	071835	26.2N 136.7E	700MB	2467					289		160	19	7	3									19
28	072112	26.8N 136.8E	700MB	2500	932	90		60		100		30	7	4	ELL IPTICAL	30	20	140	+14	+17	+15		19
29	080627	29.8N 138.4E	760MB	2545		100	250	5	200		090	30	5	1									20
30	080853	30.7N 139.1E	700MB	2566	945				140		020	20	5	5						+22			28
31	082035	33.8N 143.0E	700MB	27.33	959	90 (9 90	120	210				3	5					+19	+20	+12		21
32	002332	34.4N 144.2E	700MB	2763					938	82	289	110	10	4									21

RADAR FIXES

FIX NO.	TIME (Z)	FIX POSITION	RADAR	ACCRY	EYE SHAPE	EYE DIAM	RADOB-CODE ASWAR TDDFF	CI	DMMENTS	RADAR POSITIO		SITE WMO NO.
1	020635	12.7N 147.3E		FAIR						13.6N 14	14.9E	91218
2	020735	12.7N 147.3E		GOOD						13.6H 14	14.9E	91218
3	020835	12.7N 147.2E		GDOD						13.6N 14		91218
4	020935	12.8N 147.1E		POOR						13.6N 14		91218
5	021035	12.7N 146.7E		FAIR						13.6N 14		91218
6 7	021135 021235	12.7N 146.6E		6000						13.6N 14		91218
8	021235	12.8N 146.3E 12.8N 146.2E		600D						13.6N 14		91218
9	021435	12.8N 146.1E		GOOD						13.6N 14		91218
10	021540	12.8N 145.8E		GOOD						13.6N 14		91218
11	021640	12.8N 145.7E		FAIR						13.6N 14		91218
12	021735	12.8N 145.7E		HAIR	C IRCULAR	25				13.6H 14		91218
13	021835	12.8H 145.4E		GOOD	CIRCULAR	25				13.6N 14		91218 91216
14	021935	12.8N 145.3E		FAIR	CINCOLIN	25				13.6N 14		91218
15	022040	12.9N 145.1E		GCOD	CIRCULAR	18				13.6N 14		91213
16	022140	12.8N 144.8E		GOOD	CIRCULAR	16				13.6N 14		91218
17	022235	12.BN 144.6E		G000	ELL IPTICAL			ELIP AXIS 18	3/4	13.6N 14		91218
18	030035	13.1N 144.5E		GOOD	CIRCULAR	11			· ·	13.6N 14		91218
19	030135	13.1H 144.3E		GOOD	CIRCULAR	18				13.6N 14		91216
20	030235	13.2N 144.2E		GOOD	C I R CULAR	9				13.6N 14		91218
21	030335	13.2N 144.0E	LAND	COOD	CIRCULAR	10				13.6N 14		91218
22	030435	13.2N 143.9E	LAND	FAIR		14				13.6N 14		91218
23	030535	13.3N 143.8E	LAND	FAIR		16				13.6N 14	4.9E	91218
24	030630	13.4N 143.8E		FATR		11				13.6N 14	4.9E	91218
25	028830	13.5H 143.4E		POOR		13		OPEH N-SE		13.6N 14	4.9E	91218
26	031030	13.6N 143.2E		FAIR		7				13.6N 14	4.9E	91218
27	031130	13.6N 143.0E		FA1R		5				13.6N 14		91218
28	031235	13.7H 142.8E		FAIR		6				13.6N 14		91218
29	031335	13.8N 142.8E		FAIR		В		OPEN NE		13.6H 14		91218
30	031435	13.8N 142.7E		GOOD		7		OPEN N		13.6H 14		91218
31	031535	13.9N 142.2E	LAND	FAIR						13.6H 14		91218
32 33	031635 080900	14.1N 142.2E	LAND	POOR			FE			13.6N 14		91218
33 34	081300	30.4N 138.9E 31.6N 141.2E	LAND LAND				65/// ///// 65/// 50749			35.3H 13H		47639
35	082000	34.2N 141.2E					35/// 50422			35.3N 131		47639
33	502000	34.6N 143.6E	LHID				33/// 304ZZ			35.3N 13	8.7E	47639

BEST TRACK	WARNING ERRORS	24 HOUR FORECAST	48 HOUR FORECAST	72 HDUR FORECAST
MO/DA/HR POSIT WIND POSIT	WIND DST WIND	ERRORS POSIT WIND DST WIND	ERRORS	ERRORS
	ערונט טכני ערונט 00. 0.		POSIT WIND DST WIND	POSIT WIND DST WIND
	.0 00. 0.		0.0 0.0 00. A.	0.0 0.0 00. 0.
	.0 00. 0. .0 00. 0.		0.0 0.0 00. 0.	0.0 0.0 00. 0.
101100Z 15.9 141.3 30 16.1 141			0.0 0.0 00. 0.	0.0 8.0 00. 0.
101106Z 16.2 139.9 35 16.2 139		18.7 136.2 35. 1705. 17.8 135.2 45. 128. 0.	22.2 133.3 45. 38220. 21.6 132.2 55. 33715.	27.8 133.9 55. 78045.
1011122 16.2 138.5 40 16.3 138		18.2 133.8 55. 147. 0.		26.8 133.0 55. 76360.
1011187 16.0 137.0 45 16.4 136		18.3 132.2 55. 1295.		26.8 133.0 55. 82750.
101200Z 15.9 135.7 40 16.0 135		16.2 130.8 50. 2115.		26.8 133.0 55. 87725.
1012062 15.9 134.2 45 15.6 134		15.7 129.3 55. 6015.	17.8 126.1 60. 6340. 17.3 124.8 65. 7750.	19.4 120.4 50. 1215.
1012127 15.9 132.9 55 15.9 132		16.3 127.1 75. 71. 0.		19.2 120.0 55. 1425.
1012182 16.2 131.7 60 16.0 131		16.9 125.7 75. 605.	18.3 122.2 70. 6035. 18.8 120.8 60. 8420.	20.1 117.2 60. 1745.
101300Z 16.4 130.5 65 16.5 130		18.6 126.4 90. 9610.	20.9 124.2 100. 326. 45.	20.2 115.7 50. 18820. 23.1 123.1 118. 602. 35.
1013062 16.7 129.3 70 17.0 129		19.2 125.8 90. 16225.	21.3 123.8 100. 384. 49.	23.1 123.1 110. 602. 35. 24.3 123.0 110. 702. 35.
101312Z 17.1 120.0 75 17.1 128		18.8 124.2 95. 14510.	21.2 120.8 85. 311. 20.	24.4 118.8 60. 58520.
1013182 17.4 126.6 80 17.3 126		19.2 121.9 85. 122. 5.	22.3 119.2 75. 355. 5.	26.2 117.7 45. 65635.
1014002 17.7 125.0 100 17.9 125		20.0 120.4 80. 155. 25.	23.0 117.3 70. 3945.	25.9 115.9 35. 60540.
1014062 17.6 123.5 115 18.2 123		20.5 119.7 80. 204. 20.	23.8 116.9 70. 4615.	0.0 0.0 00. 0.
1014122 17.3 122.2 105 17.3 122		16.3 117.8 65. 61. 0.	16.3 112.8 70. 6210.	17.0 107.9 80. 78. 5.
1014102 17.4 120.9 80 17.5 120		17.2 116.1 75. 8. 5.	18.0 111.2 85. 49. 5.	20.0 106.6 55. 7420.
101500Z 17.5 119.7 55 17.5 119		17.7 114.8 85. 48. 10.	18.6 110.6 70. 775.	20.2 106.6 50. 8025.
101506Z 17.3 118.5 60 17.7 118	3 70. 27. 10.	17.6 113.4 90. 42. 15.	18.1 199.3 65. 3919.	19.9 105.5 45. 5725.
1015122 17.2 117.3 65 17.3 117		18.3 112.2 80, 79, 0,	20.5 108.2 55. 13420.	0.0 0.0 00. 0.
1015102 17.1 116.2 70 17.5 115	8 70, 33, 0.	18.6 110.8 80. 97. 0.	20.3 106.2 40. 9B35.	0.0 0.0 00. 8.
101600Z 16.9 114.7 75 17.0 114	.8 70. 85.	16.8 109.9 65. 4210.	16.4 105.8 30. 15645.	0.0 0.0 00. 0.
1016062 16.9 113.3 75 16.8 113	2 75. 8. 0.	16.3 108.0 55. 9920.	0.0 0.0 00. 0.	0.0 0.0 80. 0.
1016127 17.0 112.0 80 17.0 112	.0 80. 0. 0.	17.7 107.4 60. 4315.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1016182 17.2 111.0 80 17.2 111	.0 75. 05.	18.8 106.8 45. 630.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1017002 17.5 109.9 75 17.7 109	7 75. 17. 0.	19.2 105.7 45. 2130.	0.0 0.0 00. 0.	0.0 0.0 80. 0.
101706Z 17.8 108.7 75 17.7 108	.9 75. 13. 0.	18.8 104.9 30. 2140.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1017122 18.3 107.8 75 18.2 107	7 80. 8. 5.	0.8 0.8 00. 0.	0.0 0.0 00. 0.	0.0 0.0 D9. D.
101718Z 18.8 106.9 75 18.9 106	. 8 70. 8 5.	0.0	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1018002 19.0 106.0 75 19.1 106	.0 70. 65.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
101806Z 19.0 105.2 70 0.0 0	.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.9 00. 0.

	ALL	FORECAS	TS		TYPHOO	35 KTS		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	12.	86.	213.	430.	12.	86.	213.	430.
AVG RIGHT ANGLE ERROR	10.	74.	175.	333.	10.	74.	175.	333.
AVG INTENSITY MAGNITUDE ERROR	2.	12.	23.	27.	2.	12.	23.	27.
AVG INTENSITY BIAS	0.	-6.	-12.	-18.	9.	-6.	-12.	-18.
NUMBER OF FORECASTS	29	26	21	17	28	26	21	17

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 2400. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

13. KNOTS

TYPHOON NANCY FIX POSITIONS FOR CYCLONE NO. 24

FIX	TIME	FIX				
NO.	(Z)	POSITION	ACCRY	DVDRAK CODE	COMMENTS	SITE
1	100503	16.1N 147.0E	PCN 3	T1.5/1.5	INIT OBS	PGTW
2	100900	16.3N 145.8E	PCN 6			PGTW
3	101200	16.1N 144.5E	PCN 6		ULAC FIX	PGTW
4	101600	15.8N 143.5E	PCN 6		ULAC FIX	PGTW
5	101800	15.7N 142.6E	PCN 6		ULAC FIX	FGTW
6	102100	15.9N 141.6E	PCN 6		ULAC FIX	PGTU
7	110000	15.9N 141.4E	PCN 4			PGTM
8	110400	16.0N 139.8E	PCN 6	T2.5/2.5 /D1.0/23HRS		PG TW
9	110451	16.0N 139.6E	PCN 3			PGTW
10	110600	15.9N 140.1E	PCN 4			₽G ПJ
11	110900	16.2N 139.2E	PCN 6			PGTW
12	111200	15.8N 138.0E	PCN 6		ULAC FIX	PG (U
13	111600	16.1N 137.3E	PCN 6		ULAC FIX	₽GTW
14	111736	16.3N 136.6E	PCN 6		ULAC FIX	PGTW
15	112100	16.3N 136.1E	PCN 6		ULAC FIX	PG FU
16	120000	15.8N 135.5E	PCN 4			PGTM
17	120400	15.8N 134.7E	PCN 4	T3.0/3.0 /D0.5/24HRS		คราม
18	120621	15.9N 134.2E	PCN 3			PCTU
19	120900	16.0N 133.9E	PCN 4	•		FGTU
20	121200	16.0N 132.8E	PCN 4			PGTU
21	121600	16.2N 131.8E	PCH 4		•	Pisityi
22	121800	16.3N 131.5E	PCH 4			PGT⊎
23	122100	16.4N 131.1E	PCN 4			PGTW

24	130000	16.4N 130.6E	PCH 4		ULCC FIX		PGTU
25	-130300	16.6N 130.0E	PEN 2	T4.5/4.5-/D1.5/23HRS			FGTM
26	130609	16.8N 129.2E	PCH 1				PGTM
27	130609	16.9N 129.3E	PCN 1	T4.5/4.5	INIT OBS EYE DIA 6N	IM	RPIK
28	130900	17.1N 128.8E	PCN 2	1410, 110	IIII ODO ETE DIN GI		PGTW
29	131200	17.2N 128.1E	PCN 4				
	131600						PSTU
30		17.4H 126.9E	PCN 2				FBTU
31	131854	17.6N 126.5E	PCN 1				PGTU
32	132100	17.6N 125.7E	PCH 2				PGHA
33	140000	17.7N 124.9E	PCN 2				PG IM
34	140300	17.8N 124.2E	PCN 2	T5.5/5.5 /D1.8/24HRS			PGTU
35	140556	17.7N 123.4E	PCN 1				PGIU
36	140556	17.7N 123.4E	PCN 1	T6.0/6.0-/D1.5/24HRS			REHK
37	140900	17.7N 123.0E	PCN 2				FOTH
38	141200	17.7N 122.3E	PCN 2				FGTU
39	141600	17.7N 121.2E	PCN 6				FGTM
48	141800	17.7N 120.9E	PCN 6				Pi;TU
41	141841	17.8N 120.5E	PCN 5				PGTW
42	142100	17.6N 120.0E	PCN 6		ULCC FIX		PGTW
				T4 F # 0: 411 0 011100			
43	150000	17.5N 119.6E	PCN 6	T4.5/5.0+/W1.0/21HRS	ULAC FIX		PGTU
44	150300	17.4N 119.1E	PCH 2	*			PSTW
45	150600	17.5N 118.5E	PCN 2				PGTW
46	150726	17.4N 118.1E	PCN 5	T4.0/4.5+/W2.0/25HRS			REHK
47	150900	17.4N 117.8E	PCN 2				PGTW
48	151200	17.7N 117.1E	PEN 4				PGTU
49	151600	17.7N 116.1E	PCN 6				PGTW
50	151800	17.6N 115.6E	PCN 6				PGTW
51	151829	17.2N 116.0E	PCN 5				RPMK
52	152166	17.1N 115.2E	PCN 6				PGTM
53	160000	17.0N 114.4E	PCN 4				PGTW
54	160300	16.9N 113.8E	PCN 2	T5.0/5.0 /D0.5/27HRS			PGTU
55	160600	16.9N 113.4E	PCN 2	13.0/3.0 / 20.3/2/11/0			PGTW
56	160714	17.0N 113.8E	PCN 1	T4.5/4.5-/D0.5/24HRS			RPMK
57	160900	17.0N 112.7E	PCN 2	14.374.3-700.3724NS	EYE DIA 25NM		PG FW
					EIE DIN SOMI		
58	161200	17.0N 112.1E	PCN 2				PGTW
59	161600	17.2N 111.3E	PCN 2				PGTW
60	161800	17.3N 110.9E	PCN 2				PGTW
61	161959	17.4N 110.7E	PCH 1		EYE DIR 36NM		RITIK
62	162100	17.5N 110.4E	PCN 2				PGTW
63	170000	17.6N 109.9E	PCN 2				PGTW
64	170300	17.6N 109.4E	PCN 2	T5.5/5.5-/D0.5/24HRS			PGTW
65	170600	17.9N 108.BE	PCN 2				PGTW
66	170702	10.0N 10B.3E	PCN 1	T5.0/5.0-/D0.5/24HRS	EYE DIA 40NM		RPMK
67	170900	18.1N 108.1E	PCN 2				PGTW
68	171200	18.4N 107.8E	PCN 2				PGTW
69	171600	18.7N 107.2E	PCN 2				PGTU
70	171800	18.9N 106.9E	PCN 2				PGTW
71	171947	19.0N 106.7E	PCN 1				RPIK
72	172100	19.0N 106.5E	PCN 2			•	PGTW
73	180000	18.8N 106.0E	PCN 2				PGTW
				T4 9 /E 9 411 E /3 /1170			PG (M
74	180300	18.9N 105.7E	PCN 4	T4.0/5.0-/W1.5/24HRS			
75	180600	18.9N 105.2E	PCN 4		00 =		PGTW
76	180900	19.0N 105.0E	PCN 6		ULCC FIX		PGTW
77	181200	18.8N 104.7E	PCN 6		ULAC FIX		PGTW
78	181600	18.8N 105.0E	PCN 6				PGTW
79	181898	18.8N 104.9E	PCN 6				PGTU
80	200000	18.8N 104.3E	PCN 6				PGT₩

AIRCROFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB 08S HGT MSLP	MAX-SFC-WND VEL/BRG/RNG	MAX-FLT-LVL-U DIR/VEL/BRG/1		EYE SHAPE	EYE ORIEH- DIAMVIATION	E'YE TEMP OUTV INV DP	
1 23 4 5 6 7 8 9 10 11 12 13 14 15 16 17 18	110135 110543 110750 112114 112350 120613 120623 122085 122217 130615 132158 140015 140701 150725 151005 152123 160023	15.8N 141.2E 16.2N 148.1E 16.2N 133.4E 15.9N 136.2E 15.9N 134.2E 15.9N 133.8E 16.2N 131.2E 16.3N 139.9E 16.6N 128.8E 17.7N 125.4E 17.6N 125.0E 17.6N 123.4E 17.5N 122.8E 17.2N 18.3E 17.2N 118.3E 17.0N 117.6E	1500FT 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB 700MB	1086 999 998 998 2992 2982 2930 985 2968 2975 2867 2798 970 2616 2616 2627 2547 2547 2935 983 2938 979 2839 2939 979 2839 2839 2839 2839 2839 2839 2839 283	25 360 10 40 360 10 25 250 40 40 80 10 20 35 270 30 50 300 18 55 270 7 50 090 10 80 040 12 75 350 20 100 140 5 100 890 5 100 890 5 100 890 13 65 040 30 66 340 65 55 360 66 70 000 15	228 28 130 118 52 039 348 21 259 160 58 010 040 55 308 050 38 300 160 63 039 060 73 360 138 76 060 138 76 060 138 78 148 028 73 350 109 117 070 019 60 270 150 117 070 090 117 360 150 45 040 046 63 350 046 63 350 108 23 360 060 79 360	30 2 5 90 5 1 90 5 2 20 10 10 40 10 4 90 8 3 21 10 2 27 5 2 21 10 2 27 5 2 40 15 2 10 15 3 10 15 3 10 15 3 10 15 3 10 15 5 10 1 1 13 10 1 15 5 16 5 17 5 18 5 18 5 18 6 18 6 18 7 18 8 18 8 18 8 18 8 18 8 18 8 18 8	CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR CIRCULAR	10 20 12 20 35 50	+23 +23 +22 +31 +31 +24 +24 +22 + 9 +13 + 9 +12 +17 +10 +14 +13 +14 +17 +10 +12 +21 + 9 +11 +15 + 8 +12 +12 +12	30 1 2 27 2 3 3 4 4 5 5 6 6 7 7 8 8 9 9
					RADAI	R FIXES					
FIX NO.	TIME (Z)	FIX POSITION	RADAR AC	EYE CRY SHAF		RADOB-CODE ASWAR TDDFF	(COMMENTS		RADAR POSITION	SITE WMO NO.
1 2 3 4 5 6 7 8 9 10 11 12 13 14	140400 140600 140630 141300 141330 141400 141500 150300 150300 150330 150400 151200 151430	18.8N 124.8E 17.8N 123.6E 18.4N 123.6E 17.7N 122.0E 17.6N 121.9E 17.6N 121.9E 17.6N 121.6E 17.6N 119.7E 17.6N 119.7E 17.8N 118.7E 17.8N 118.7E 17.7N 118.7E 17.7N 117.0E	LAND LAND LAND LAND LAND LAND LAND LAND			22982 //// 42618 4/// 42618 4/// 11852 42513 11194 42518 12334 42718 18184 42518 18637 //// 1297/ 42718 1297/ 42708 1297/ 42705 1297/ 42705 1091/ 42718 1091/ 42718	EYE 100 PC	ELPTCL 65/5 T ELLIPTICAL ELLIPTICAL	ie kms	18. 3N 121.6E 18. 3N 121.6E 18. 3N 121.6E 18. 3N 121.6E 18. 3N 121.6E 18. 3N 121.6E 18. 3N 121.6E 16. 3N 120.6E 16. 3N 120.6E 16. 3N 120.6E 16. 3N 120.6E 16. 3N 120.6E 16. 3N 120.6E	98231 98231 98231 98231 98231 98231 98231 98321 98321 98321 98321 98321 98321 98321
						IC FIXES					
FIX ND.	TIME (Z)	F1X POSITION	INTENSIT EST IMATE		1)	COMMENTS					
1 2	141500 160900	17.3N 121.8E 17.0N 112.7E	090 080	020 030	WMO 98 WMO 59						•

	BEST	TRACK		WARNI				24 H	OUR FO				48 H	DUR FO	RECAS	ST.		72 H	OUR FO	RECAS	Т
					ER	rors				ERR	ors '				ERROR	२९			Ε	RRORS	
MO/DA/HR	POSIT	⊍1ND	POSIT	WIND	DST	MIND	P05	TI	MIND	DST	MIND	P051	ΙT	MIND	DST	WIND	POS	ΙT	WIND	DST	MIND
101506Z	18.3 137.	8 20	18.0 137.8	25.	18.	5.	19.0	134.0	30.	133.	15.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
1015122	18.9 136.	9 20	18.8 136.8	25.	8.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.	0.0	8.8	8.	~0.	0.
1015182	19.8 136.	1 20	18.9 135.2	20.	74.	0.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101600Z	20.5 135.	4 15	19.5 135.2	20.	61.	5.	0.0	0.0	Ø.	-0.	ø.	9.9	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	0.
101606Z	21.0 135.	0 15	21.2 134.9	15.	13.	ø.	0.8	0.0	ø.	-0.	0.	8.6	0.0	0.	-0.	8.	0.0	0.0	0.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS						
	LIRNG	24-HR	48~HR	72-HR	₩RHG	24~HR	48-HR	72-HR			
AVG FORECAST POSIT ERROR	35.	133.	0.	0.	0.	0.	0.	0.			
AVG RIGHT ANGLE ERROR	33.	119.	0.	0.	0.	0.	0.	0.			
AVG INTENSITY MAGNITUDE ERROR	3.	15.	0.	0.	0.	0.	0.	0.			
AVG INTENSITY BIAS	3.	15.	ø.	0.	8.	Ø.	0.	0.			
NUMBER OF FORECASTS	5	1	8	8	8	9	0	0			

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 228. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

10. KNOTS

TROPICAL DEPRESSION TD25
FIX POSITIONS FOR CYCLONE NO. 25

SATELLITE FIXES

F1X NO.	TIME (Z)	FIX POSITION	ACCRY	DVORAK CODE	COMMENTS	SITE
i	140000	17.1N 143.7E	PCN 6	T1.5/1.5	INIT OBS	PGTW
2	140300	17.5N 142.8E	PCN 6			PGTW
3	140600	17.9N 142.0E	PCN 6		ULAC FIX	PGTW
4	140900	18.1N 141.3E	PCN 6		ULAC FIX	PGTW
5	141200	17.6N 140.4E	PCN 6		ULCC FIX	PGTU
6	141600	18.2N 139.4E	PCN 6			PGTW
7	141800	17.7N 139.0E	PCN 6		ULAC FIX	₽GT₩
8	142100	18.1N 138.1E	PCN 6		ULAC FIX	PGTW
9	150000	17.8N 138.8E	PCN 6	T2.0/2.0 /D0.5/24HRS		PGTW
18	150300	17.9N 138.2E	PCN 6			PGTW
11	150544	18.7N 137.9E	PCN 6			PSTU
12	150600	18.7N 137.9E	PCN 4			₽GTW
13	150900	18.9N 137.4E	PCN 6	•		PGTW
14	160000	20.6N 135.3E	PCN 4	T1.0/1.5 /W1.0/24HRS		PGTW
15	160532	20.9N 135.6E	PCN 3			PGTW

AIRCRAFT FIXES

NO.	(Z)	POSITION			VEL/BRG/RNG					DIAM TATION	DUTY INV DP/SST	NO.
1	142336	17.8N 138.9E	1500FT	1006	20 030 60	210	26 140	50	5 2	•	+24 +25 +25 30	1

	BEST TRACK	WARNING	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
MOZDAZHE	POSIT WIND	ERRORS POSIT WIND DST WIND	ERRORS POSIT WIND DST WIND	ERRGRS POSIT WIND DST WIND	ERRORS POSIT WIND DST WIND
101400Z	10.9 161.8 20	0.0 0.0 00. 0.	0.0 0.0 U0. A.	0.0 0.0 00. 0.	POSIT WIND DST WIND 0.0 0.0 00. 0.
101406Z	11.0 160.8 20	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
101412Z	11.8 159.7 20	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1014182	11.7 158.2 25	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
101500Z 101506Z	11.7 156.7 25	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1015122	12.0 155.3 25 12.8 154.1 30	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.	8.0 0.0 00. 0.
1015182		11.8 152.9 30. 115. 0.	8.8 0.8 00. 0. 12.8 147.4 45. 192. 5.	0.0 0.0 00. 0. 14.0 142.7 60. 25B. 5.	0.0 0.0 00. 0. 15.6 137.9 70. 373. 0.
1016002		13.8 151.6 35. 56. 0.	14.9 145.5 55. 159. 10.	17.0 141.2 75. 235. 15.	15.6 137.9 70. 373. 0. 19.4 136.8 95. 386. 20.
101606Z	15.0 150.9 35	14.8 150.2 40. 42. 5.	15.6 144.2 60. 180. 15.	17.0 139.8 80. 283. 20.	20.2 135.2 100. 462. 20.
101612Z		15.2 149.5 45. 13. 5.	15.6 144.6 60. 128. 10.	17.2 139.7 75. 259. 10.	20.1 136.2 95. 402. 10.
101618Z		15.5 148.4 45. 26. 5.	16.3 144.0 65. 121. 10.	17.4 140.1 80. 217. 10.	20.2 137.1 100. 369. 10.
101700Z 101706Z		16.5 147.8 45. 19. 0.	18.1 144.2 65. 87. 5.	20.0 140.9 85. 164. 10.	22.6 138.7 100. 290. 5.
1017122		16.2 146.8 55. 26. 10. 16.8 146.5 55. 6. 5.	17.5 143.1 70. 93. 10. 17.5 143.4 65. 46. 0.	19.2 140.2 90. 186. 10.	21.8 137.8 105. 421. 5.
1017182		16.9 146.3 60, 17, 5,	18.4 144.5 75. 42. 5.	18.8 140.6 90. 202. 5. 20.4 142.8 100. 102. 10.	21.0 138.3 115. 508. 10. 22.9 140.9 120. 428. 15.
101800Z		17.2 145.7 60. 24. 0.	18.2 143.5 75. 48. 0.	20.0 141.7 95. 233. 0.	22.9 140.9 120. 428. 15. 22.6 140.2 115. 599. 15.
1018062		17.3 144.4 60. 18. 0.	18.1 140.9 80. 178. 2.	19.4 138.3 100. 477. 0,	21.8 136.3 110. 925. 20.
1018122	17.6 144.2 65	17.3 144.1 60. 195.	17.8 141.0 80. 2325.	19.8 137.8 100. 5745.	21.6 136.2 110.1027. 30.
101818Z		17.4 143.6 65. 495.	18.1 141.0 85. 2705.	20.0 137.8 100. 6735.	21.8 136.2 110.1102. 40.
101900Z 101906Z		18.8 143.7 75. 13. 0.	21.8 142.5 85. 11910.	25.1 142.6 90. 40310.	28.5 146.3 85. 488. 20.
1019062		19.7 143.2 80. 16. 0. 21.0 143.2 85. 6. 0.	22.7 142.4 90. 17410. 25.2 142.8 100. 1725.	26.1 143.2 85. 4675. 29.5 145.8 80. 350. 0.	29.0 147.6 88. 478. 20.
1019182		22.2 143.4 85. 125.	26.3 144.4 95. 15710.	29.5 145.8 80. 350. 0. 31.2 148.4 75. 288. 5.	31.3 149.8 65. 437. 5. 31.4 151.8 68. 482. 5.
1020002		23.2 143.6 100. 18. 5.	28.8 145.8 100. 163. 0.	34.2 149.7 80. 353. 15.	39.6 154.5 65. 797. 10.
102006Z		24.5 144.6 95. 125.	30.5 147.1 80. 20010.	39.1 152.1 60. 602. 0.	0.0 0.0 00. 0.
1020122		26.0 146.0 95. 1310.	31.1 150.4 75. 1065.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1020182		27.4 147.5 90. 2215.	32.3 152.7 70. 102. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
102100Z 102106Z		28.8 148.8 105. 5. 5. 29.8 151.2 90. 17. 0.	"33.8 155.2 60. 1865. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	9.0 9.0 99. 9.
1021122		30.8 152.7 85. 17. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1021182		31.2 154.0 70. 12. 0.	0.0 0.0 00. 0.	0.0 9.0 00. 0.	0.0 0.0 00. 0.
102200Z		31.0 155.5 50. 2115.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	8.0 0.0 00. 0.
102206Z	29.8 156.7 60	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
102212Z 102218Z	28.8 157.7 60	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1023162	27.8 158.3 55 26.9 159.2 55	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1023062	26.2 160.2 55	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1023122	25.9 161.4 55	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 0, -0. 0.	8.8 0.8 00. 0.
102318Z	25.7 162.5 50	0.0 0.0 00. 0.	0.0 0.0 00. 0.	8.8 8.8 88. 8.	0.0 0.0 00. 0.
1024002	25.5 163.6 50	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 0 0. 0 .	0.0 0.0 00. 0.
102406Z 102412Z		25.6 164.7 50. 20. 0. 25.5 165.8 50. 28. 0.	25.8 169.2 60. 100. 10.	26.2 173.6 50. 418. 10.	0.0 0.0 00. 0.
102412Z		25.5 166.1 50. 5. 0.	26.7 170.2 50. 145. 0. 26.2 169.1 50. 126. 5.	0.0 0.0 00. 0. 27.6 172.2 45. 377. 10.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
102500Z		25.5 167.1 50. 16. 0.	26.1 170.3 45. 227. 8.	27.7 174.5 45. 515. 15.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
102506Z		26.1 167.8 45. 225.	27.3 170.8 40. 255. 0.	28.3 174.2 35. 505. 5.	0.0 0.0 00. 0.
1025122		26.6 168.5 45. 555.	28.5 171.8 40. 322. 5.	29.9 175.9 35. 544. 10.	0.0 0.0 00. 0.
1025102		27.5 167.5 45. 24. 0.	29.8 167.8 45. 135. 10.	0.8 0.8 08. 0.	0.0 0.0 00, 0.
102600Z 102606Z		28.0 167.3 45. 44. 0.	30.2 167.8 40. 147. 10.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1026062		28.3 166.4 45. 17. 5. 28.8 166.2 45. 27. 10.	30.6 165.2 35. 15. 5. 31.0 165.2 0. 2925.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
102618Z		29.3 165.2 40. 9. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1027002		30.1 164.8 35. 21. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1027062		30.2 164.2 35. 43. 5.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1027122		31.4 165.3 35. 10. 10.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
102718Z 102800Z	32.3 166.7 25 33.3 167.3 20	0.8 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
.020002	22.2 101.2 20	0.0 0.0 0	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL FORECASTS				TYPHO	LE OVER	R 35 KTS		
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	24.	146.	362.	550.	21.	154.	339.	550.	
AVG RIGHT ANGLE ERROR	10.	103.	236.	285.	16.	108.	212.	285.	
AVG INTENSITY MAGNITUDE ERROR	4.	6.	8.	14.	4.	6.	8.	14.	
AVG INTENSITY BIAS	1.	1.	6.	14.	0.	1.	5.	14.	
NUMBER OF FORECASTS	49	32	24	18	36	29	21	18	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 3604. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON OWEN FIX POSITIONS FOR CYCLONE NO. 26

SATELLITE FIXES

FIX NO.	TIME (2)	FIX POSITION	ACCRY	DVORAK CODE	CUITENTS	CITE
110.	\L/	103111011	HOOKI	DAGKHY CODE	COLLIENTS	SITE
1	140000	9.4N 161.5E 10.3N 160.9E		T1.0/1.0	INIT DBS	PGTW
3	140414	10.6N 160.9E	PEN 6 PEN 6			PGTW PGTW
4	140900	10.8N 160.2E	PCN 6		ULAC FIX	PGIU
	141200	11.5N 160.0E	PCN 6			PGTW
	141600	12.2N 159.3E 11.8N 158.8E	PCN 6 PCN 5			PGTW PGTW
8	141800	11.6N 158.4E	PCN 6			PGT₩
		11.7N 157.4E	PCN 6	TO 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0 0	# 00 ETV	PGTU
	150000 150402	11.8N 156.4E 11.8N 155.5E	PCN 6 PCN 5	T2.0/2.0 /D1.8/24HRS	ULAC FIX ULAC FIX	PGTU PGTU
12	150600	12.2N 155.3E	PCN 6		ULAC FIX	PGTW
13	150900 151200	12.6N 154.9E 12.3N 154.9E	PCN 6		ULAC FIX	PGTW PGTW
		11.6N 153.4E	PCN 6			PGTW
* 16	151800	11.5N 152.7E	PCN 6		BASED ON EXTRAP	PGTW
* 17 * 19	152100	13.3N 151.7E 14.7N 151.0E	PCN 6 PCN 6	T2.5/2.5 /D0.5/24HRS		PGTIJ PGTU
19	160300	14.6N 150.6E	PCN 6	12.0/210 / 20:0/2-41/0		PGTW
20	160600	14.6N 150.3E	PCN 6			PGTW
21	161200	14.6N 149.7E 14.6N 149.5E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
23	161635	15.2N 148.8E	PCN 6		ULCC FIX	PGTW
		15.2N 148.5E	PCN 6		ULCC FIX	PGTW
25 26	170000	16.0N 148.0E	PCN 6	T3.0/3.0 /D0.5/24HRS		PG TW PG TW
27	170300	16.5N 147.6E 16.1N 147.5E	PCN 4			PGTW
28	170520	16.4N 147.3E	PCN 3			PGTW PGTW
29 30	171200	16.3N 147.0E 16.4N 146.8E	PCN 6 PCN 6			PGTW
31	171600	16.9N 146.4E	PCN 6			PGTW
32 33	171800	17.5N 146.0E 17.5N 145.8E	PCN 6 PCN 6		BASED ON EXTRAP BASED ON EXTRAP	PGTW PGTW
		17.4N 145.0E	PCN 6		BASED ON EXTRAP	PGTW
	180300			T4.0/4.0 /D1.0/24HRS		PGT₩
		17.2N 144.0E 17.0N 144.5E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
38	181200	17.1N 144.1E	PCN 6		ULAC FIX	PGTW
	181600 181800	17.6N 144.0E 18.3N 144.0E	PCN 6 PCN 6		ULAC FIX	PGTW PGTW
41		18.4N 143.9E	PCN 6		ULAC FIX	PGTW
42	190000	18.7N 143.6E	PCN 6		ULCC FIX	PGTW
43 44	190300 190600	19.2N 143.4E 19.9N 143.4E	PCN 4 PCN 2	T4.5/4.5 /D0.5/24HRS	EYE OPEN SW-NU	PGTW PGTW
	190900	20.6N 143.2E	PCN 2		EYE OPEN SSE	PGT₩
		21.1N 143.3E	PCN 4		ULAC FIX	PGTW
47 48	191600	21.8N 143.6E 22.8N 143.3E	PCN 4 PCN 2			PGTW PGTIJ
49	191800	22.0N 143.3E 22.2N 143.3E	PCN 2			PGTW
50 51	192100 200000	22.5N 143.4E 23.3N 144.0E	PCN 2 PCN 2			PGTW PGTW
52	200300	24.0N 144.3E	PCN 2	T5.5/5.5-/D1.0/24HRS		PGTW
53	200443	24.2N 144.5E	PCN 1			PGTW
54 55	200600	24.7N 144.8E 25.3N 145.4E	PCN 2 PCN 2			PGTW PGTW
56	201200	26.2N 146.1E	PCN 2			PGTW
57 50	201600	27.0N 147.0E	PCN 2			. PGTW PGTW
58 59	202100	27.4N 147.2E 28.2N 147.8E	PCN 1 PCN 2			PGTW
69	210000	28.6N 148.7E	PCN 2	T4 F M 0 411 0 0 0 0 0 0		PGTW
		29.1N 149.9E 29.5N 150.8E	PCN 2 PCN 4	T4.5/5.0 /U1.0/24HRS		PGTU PGTU
63		29.9N 151.8E	PCN 4			PGTW
64	210900	30.1H 152.1E	PCN 4		ULCC FIX	PGTW
	211200	30.6N 152.8E 30.9N 153.5E	PCN 6 PCN 6			PGTW PGTW
67	211716	30.7N 153.7E	PCN 5			PGTW
		30.9N 154.1E 30.8N 154.7E	PCN 6 PCN 6			PGTW PGTW
		30.7N 155.1E	PCN 6	T3.0/3.0 /W1.5/21HRS	ULAC FIX	PGTW
71	220300	30.7N 155.5E	PCN 6		ULAC FIX'	PGTW
	220419 220600	30.2N 156.1E 29.6N 156.7E	PCN 6 PCN 6		ULAC FIX ULAC FIX	PGTW PGTW
74	220900	29.2N 157.2E	PCN 6		ULAC FIX	PGTW
		28.7N 157.9E	PCN 6		ULCC FIX	PGTU PCTU
		27.7N 158.2E 27.5N 158.5E	PCN 6		ULCC FIX ULCC FIX	PGTW PGTW
78	222100	27.2N 158.7E	PCN 6		ULCC FIX	PGTW
		26.9N 159.2E	PCN 4 PCN 4	T2.0/2.0 /U1.0/24HRS	EXP LLCC	PGTW PGTW
	230300	26.7N 159.6E 26.2N 160.1E	PCN 4		EXP LLCC	PGTW
82	230600	26.2N 160.4E	PCN 6			PGTW
93 84		25.7N 160.6E 25.7N 162.5E	PCN 6 PCN 6			PGTW PGTW
54	231200	23.1M 102.3E	FUR D			raiw

85	231600	25.8N 163.0E	PCN 6			PGTW
86	232100	25.3N 163.3E	PCN 6			PGTW
87	240000	25.7N 163.6E	PCN 6	T3.0/3.0-/D1.0/24HRS		PGTW
88	240355	25.6N 164.3E	PCN 5			PG"TW
89	240600	25.7N 164.8E	PCN 4			PGTW
90	240900	25.7N 165.2E	PCN 6			PGTW
91	241200	25.6N 165.5E	PCN 6			PGTW
92	241600	25.7N 165.6E	PCN 6		ULCC FIX	PGTW
93	241639	25.4N 165.8E	PCN 6			KGWC
94	241640	25.6N 166.0E	PCN 6		ULCC FIX	PGTU
95	241800	25.6N 166.4E	PCN 6			PGTW
96	242100	25.6N 166.8E	PCN 6			PGTW
97	250000	25.8N 166.9E	PCN 6	T3.0/3.0-/S0.0/24HRS		PGTW
98	250300	26.1N 167.2E	PCN 6			PGTW
99	250342	26.2N 167.4E	PCH 6	T2.0/3.0-/W1.0/24HRS		KGUC
100	250343	26.1N 167.4E	PCN 5			PGTW
101	250600	26.3N 167.8E	PCN 6			PGTW
102	250980	26.4N 168.0F	PCN 6			PGTW
103	251200	26.5N 160.1E	PCN 6			PGTW
104	251600	26.9N 167.4E	PCN 4			PGTW
105	251627	27.1N 167.4E	PCN 4		ULCC FIX	PGTW
106	251627	27.0N 166.9E	PCN 6			KGUC
107	251800	27.5N 167.5E	PCN 6		ULCC FIX	PGTU
108	252100	27.7N 167.2E	PCN 6		ULCC FIX	PGTW
109	260000	27.9N 167.0E	PCN 6			PGTU
110	260300	27.7N 166.2E	PCN 6	T2.0/3.0-/W1.0/27HRS		PSTU
111	260330	27.7N 166.2E	PCN 6	T3.0/3.0 /D1.0/24HRS		KGWC
112	260600	28.3N 165.8E	PCN 6			PGTW
113	260900	28.5N 165.8E	PCN 6			PGTW
114	261200	29.1N 165.6E	PCN 6		ULAC FIX	PGTW
115	261600	29.2N 165.3E	PCN 6		ULAC FIX	PGTW
116	261800	29.4N 165.4E	PCN 6		ULAC FIX	PGTW
117	262100	29.7N 164.9E	PCN 6			PGTW
118	270000	29.5N 164.4E	PCN 4		EXP LLCC	PGTW
119	270300	29.9N 164.5E	PCN 4	12.0/2.5-/S0.0/24HRS		PGTU
120	270318	30.1N 165.0E	PCN 4	T2.0/2.0 /W1.0/24HRS	EXP LLCC ULAC 31.6N 165.6E	KGUC
121	270600	30.5N 164.9E	PCN 4		EXP LLCC	PGTW
122	270900	31.0N 165.0E	РСИ 6			PGTW
123	271200	31.4N 165.5E	PCN 6		ULAC 32.7N 165.6E	PGTW
124	271600	32.1N 166.5E	PCN 6			PGTW
125	271603	31.8N 166.0E	PCN 4		EXP LLCC ULAC 33.3N 167.2E	KGWC
126	271800	32.4N 167.0E	PCN 6			PGTW
127	272100	33.0N 167.4E	PCN 6			PGTW
128	280000	33.6N 168.7E	PCN 4	T1.0/1.5 /W1.0/21HRS		PGTW
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AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFO VEL/BRO				-LVL ∕BRG		ACC NAV		EYE SHAPE	EYE C	RIEN- ATION	EYE TE			MSN NO.
1	142312	11.2N 158.0E	1500FT		1005	15 366	60	020	21	280	50	5	28				+24 +18	+18	27	1
2	152317	14.3N 152.5E	1500FT			30 198	35	248	38	160	50	5	5				+25 +25		30	ż
3	169636	15.1N 150.8E	700MB	3036	995	45 128	15	040	35	270	60	5	4							3
4	160927	15.0N 150.1E	700MB	3041	999			170	45	070	70	5	4				+12 +11	+11		3
5	161422	15.6N 148.9E	700MB	3038	995			340	41	249	70	10	10				+10 +13			4
6	161801	15.8N 148.8E	700MB	3023				149	37	050	90	8	10							4
7	162013	16.1N 148.4E	700MB	3022	992	30 266	69	360	43	260	120	8	8				+12 +13	+12		4
8	170228	16.2N 147.4E	1500FT		992	65 088	99	190	72	080	24	8	5				+25	+24	30	5
9	170606	16.6N 147.3E	700MB	2987		75 136	60	190	46	150	30	8	10							5
10	170833	16.4N 146.8E	700MB	2986	988			220	54	130	110	5	4				+10 +16	+11		6
11	171122	16.4N 146.9E	700MB	2985				140	55	040	90	5	4							6
12	172054	17.1N 145.8E	700MB	2933	983	60 090	30	190	52	080	120	2	5				+13 +14	+13		7
13	172325	17.1N 145.3E	700MB	2945		60 020	90	270	61	180	140	3	4							7
14	180845	17.2N 144.4E	700MB	2925	980			110	56	949	40	5	3				+13 +15	+14		9
15	181123	17.3N 144.3E	700MB	2914				200	60	110	60	10	8							9
16	182054	18.4N 143.8E	700MÐ	2823	969	75 020	30	140	73	020	30	5	2				+13 +16	+ 9		10
17	182336	18.8N 143.6E	700MB	2800		50 220	60	300	62	220	60	5	2							10
18	190612	20.0N 143.5E	700MB	2776		65 149	120	210	75	140	78	6	3							11
19	190848	20.4N 143.2E	700MB	2736	958			310	64	239	60	6	3	C IRCULAR	20		+14 +15			11
20	192056	22.5N 143.5E	700MB	2613		50 078		250	90	170	30	10	4	C IRCULAR	40		+11 +17	+10		13
21	192343	23.2N 143.8E	700MB	2616		70 278	20	320	79	230	30	19	4							13
22	200605	24.8N 144.8E	700MB	2616		70 326	10	230	102	140	40	5	5							14
23	200844	25.2N 145.3E	700MB	2609	944			300		159	30	5	5	ELL IPTICAL	50 40	040	+15 +18	+10		14
24	202040	28.0N 147.7E	700MB	2555	939	90 066	5	240	98	150	30	5	2	ELL IPTICAL	50 30	050	+14 +20	+13		15
25	202254	28.5N 148.6E	700MB	2573		90 178		210	95	170	25	5	3	C IRCULAR	60					15
26	210704	30.1N 150.9E	700MB	2655	950	55 116	135	200	84	120	200	10	5				+11 +19	+11		16
27	210940	30.5N 151.8E	700MB	2679				298	74	210	113	4	5							16

BEST TRACK	UARN ING	24 HOUR FORECAST	48 HOUR FORECAST	72 HOUR FORECAST
MO/DA/HR POSIT WIND POSIT	ERRORS WIND DST WIND	POSIT WIND DST WIND	ERRORS	ERRORS
112118Z 7.6 176.7 15 0.0 0		POSIT WIND DST WIND 8.0 00 00. 9.	POSIT WIND DST WIND 8.8 0.0 00. 0.	POSIT WIND DST WIND 0.0 0.0 0. 0. 0.
1122002 7.0 177.2 20 0.0 0	.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 9.0 00. 0.
112206Z 7.0 177.9 20 0.0 0 112212Z 7.5 178.1 20 0.0 0		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
112212Z 7.5 178.1 20 0.0 0 112218Z 8.0 177.9 20 0.0 0		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
112300Z 8.0 177.4 25 0.0 0		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 6.0 0, -0, 0.
1123062 7.8 176.7 25 0.0 0		0.0 0.0 00. 0.	0.0 0.0 80. 0.	0.0 0.0 00. 0.
112312Z 7.6 176.3 25 0.0 0. 112318Z 7.3 175.8 25 0.0 0.		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
112400Z 7.1 175.2 30 0.0 0		0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
112406Z 6.9 174.8 38 6.8 174		6.2 172.6 35. 10615.	6.4 169.9 45. 17720.	6.9 167.2 55. 33440.
112412Z 6.8 174.2 35 6.8 174. 112418Z 6.9 173.3 45 6.8 173.		7.1 171.3 40. 5915. 7.6 170.5 55. 48. 0.	8.0 169.1 50. 19120.	9.3 167.1 69. 31835.
1125002 7.2 172.3 50 7.1 172		9.2 168.3 60. 76. 0.	8.8 168.8 60. 22415. 11.2 164.9 70. 6815.	10.2 166.7 70. 34630. 12.8 162.1 70. 12125.
1125062 7,4 171.3 50 7.5 171.	3 50. 6. 0.	9.6 167.5 70. 68. 5.	11.6 164.0 80. 9215.	13.2 161.3 70. 9825.
112512Z 7.5 170.4 55 7.4 170. 112518Z 7.6 169.7 55 7.4 169.		8.7 166.5 70. 32. Q.	10.0 163.2 80. 9315.	11.5 160.4 75. 11920.
112518Z 7.6 169.7 55 7.4 169 112600Z 8.0 168.7 60 7.5 168		8.2 165.9 75. 96. 0. 8.7 165.8 75. 11910.	9.5 162.4 80. 15120. 10.0 163.5 80. 22815.	10.9 159.7 75. 15925. 10.7 158.7 89. 161. 10.
112606Z 8.5 167.9 65 8.4 167.	7 65. 8. 0.	9.9 164.6 80. 10715.	10.5 161.8 80. 18115.	10.8 156.9 99. 190. 35.
112612Z 9.2 166.3 70 8.9 166. 112618Z 9.6 165.1 75 9.8 165.		10.7 162.9 80. 5615.	11.3 158.8 80. 11115.	11.7 154.3 90. 234. 40.
112618Z 9.6 165.1 75 9.8 165. 112700Z 9.9 164.2 85 10.3 163.		11.1 160.5 80. 4220. 12.2 159.8 85. 2610.	11.5 155.6 85. 21915. 12.5 156.1 85. 152. 15.	11.6 151.9 99. 322. 35. 12.7 153.4 85. 160. 25.
112706Z 10.5 162.9 95 10.5 162.	9 100. 0. 5.	11.9 158.6 130. 80. 35.	12.7 155.4 125. 174. 70.	12.9 151.8 120, 184, 60.
1127127 11.0 162.0 95 11.0 161.		12.2 157.6 130. 100. 35.	12.8 154.4 125. 208. 73.	13.2 150.8 120. 179. 65.
1127182 11.6 161.0 100 11.7 160. 1128002 12.0 160.2 95 11.9 160.		12.8 156.4 130. 145. 39. 13.1 156.2 100. 133. 30.	13.0 153.2 125. 234. 70. 13.5 152.7 100. 211. 40.	13.2 149.6 129. 173. 70. 13.5 148.9 90. 128. 40.
1128062 12.7 159.7 95 12.3 159.		13.5 155.5 105. 158. 50.	13.8 151.1 110. 242. 50.	13.8 146.8 115. 123. 70.
1128127 13.1 159.2 95 12.8 159. 1128187 13.4 158.8 188 12.9 158.		14.0 155.5 105. 144. 55.	14.5 151.4 110. 212. 55.	14.2 146.8 115. 158. 70.
1128182 13.4 158.8 100 12.9 158. 1129002 13.7 158.4 70 13.8 150.		13.7 154.8 105. 146. 50. 15.3 155.3 100. 186. 40.	14.1 150.5 110. 182. 60. 15.2 151.2 105. 229. 55.	14.1 146.0 115. 195. 75. 14.7 147.1 110. 378. 75.
112906Z 13.7 158.2 55 14.2 158.		15.3 155.2 95. 199. 35.	15.2 151.0 100. 268. 55.	14.7 147.1 110. 378. 75. 14.6 147.0 105. 474. 75.
1129122 13.4 157.9 50 13.6 157.		13.2 156.3 60. 203. 5.	13.2 151.4 80. 364. 35.	13.3 144.9 100. 448. 70.
112918Z 13.0 157.2 55 13.4 157. 113000Z 12.3 156.1 60 12.6 156.		12.8 155.5 65. 227. 15. 12.2 151.4 80. 95. 30.	12.6 150.1 80.399. 40. 13.2 145.8 86.277. 51.	13.6 143.6 100. 451. 65. 15.0 141.4 90. 396. 45.
113006Z 12.0 154.8 60 12.2 155.	1 65. 21. 5.	12.1 150.4 80. 153. 35.	13.2 145.2 85. 352. 55.	14.9 140.9 90. 454. 40.
113012Z 11.5 153.3 55 11.8 153. 113018Z 11.4 151.9 50 11.4 151.		11.5 149.8 70. 266. 25.	13.5 144.4 80. 420. 50.	16.1 148.2 90. 467. 40.
1130182 11.4 151.9 50 11.4 151. 1201002 11.6 149.9 50 11.5 150.		12.0 147.0 75. 217. 35. 13.0 144.9 45. 223. 10.	14.6 142.8 85. 413. 50. 14.8 140.3 50. 331. 5.	17.1 138.3 90. 401. 35. 16.0 135.4 60. 244, 5.
1201062 12.0 147.8 45 12.2 147.	7 50. 13. 5.	14.2 141.1 40. 164. 10.	15.0 135.7 40. 15710.	15.0 131.3 45. 5815.
120112Z 12.0 145.3 45 12.2 145. 120118Z 12.2 143.3 40 12.4 143.		13.2 139.2 40. 121. 10.	13.7 134.3 45. 1455.	15.5 130.9 45. 5220.
120200Z 12.1 141.2 35 12.0 141.		15.0 137.7 30. 1595. 13.9 133.9 30. 4715.	17.4 134.7 30. 21825. 17.4 128.0 30. 17925.	0.0 0.0 20. 0. 9.0 0.0 89. 0.
1202062 12.1 139.3 30 12.4 139.	2 35. 19. 5.	14.3 132.3 30. 4730.	17.2 127.0 25. 22635.	0.0 0.0 00. 0.
120212Z 12.4 137.3 30 12.2 137. 120218Z 13.0 135.9 35 12.7 135.		14.2 131.8 30. 5320.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
1202182 13.0 135.9 35 12.7 135. 1203002 13.8 134.7 45 13.4 134.		14.1 129.6 30. 13725. 15.5 129.1 35. 12120.	0.0 0.0 00. 0. 17.1 124.5 30. 29250.	0.0 0.0 00. 0. 18.3 120.3 25. 53430.
120306Z 14.3 133.1 50 14.4 133.	2 50. B. O.	16.3 128.7 65. 115. 5.	17.8 124.9 55. 27320.	18.8 120.9 50. 476. 0.
120312Z 15.0 132.2 50 14.9 132. 120310Z 15.3 131.6 55 15.4 131.		17.1 127.9 65. 146. 0.	18.5 124.0 50. 30915.	19.0 119.8 45. 5085.
1204002 15.5 131.2 55 15.5 131.		16.8 127.3 65. 1485. 17.2 129.8 55. 6225.	17.8 123.7 55. 3555. 21.1 130.3 40. 31115.	18.7 120.0 40. 46820. 0.0 0.0 00. 0.
120406Z 15.7 130.6 60 15.8 130.	8 60. 13. 0.	18.9 129.8 45. 15830.	23.9 131.2 35. 54715.	0.0 0.0 00. 0.
120412Z 15.9 130:1 65 16.0 130. 120418Z 15.9 129.7 70 16.2 129.		19.3 120.8 50. 15115. 19.0 127.6 55. 1755.	25.8 131.1 30. 71120.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
120500Z 16.2 129.5 80 16.2 129.		18.7 127.8 75. 183. 20.	24.8 130.0 35. 67725. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
120506Z 16.3 129.4 75 16.3 129.	4 85. 0. 10.	18.5 127.8 70. 200. 20.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
120512Z 16.8 129.1 65 16.5 129. 120518Z 16.8 129.8 60 16.8 128.		17.8 127.9 40. 20110. 17.8 127.3 40. 23320.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0.
120600Z 16.0 129.3 55 17.0 128.		18.1 126.7 40. 30530.	0.0 0.0 00. 0.	0.0 0.0 0. ~0. 0. 0.0 0.0 0. ~0. 0.
1206062 15.2 128.3 50 15.2 128.		14.2 123.8 69. 935.	14.5 118.8 55. 273. 20.	0.0 8.0 80. 0.
120612Z 14.5 127.3 50 14.7 127. 120618Z 14.0 126.5 60 14.2 126.		13.8 123.2 50. 124. 0. 13.8 121.3 45. 169. 5.	13.9 118.3 50. 250. 20. 14.3 116.0 55. 256. 25.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
120700Z 13.2 125.3 70 13.4 125.	3 70. 12. 0.	13.4 120.5 60. 191. 25.	14.5 115.8 65. 260. 40.	0.0 0.8 00. 0.
1207062 12.7 124.2 65 12.8 124.	3 70. 8. 5.	13.5 119.3 60. 222. 25.	0.0 0.0 00. 0.	0.0 0.0 00. 0.
120712Z 11.8 122.7 50 12.8 122. 120718Z 11.0 121.0 40 13.2 121.		13.3 118.3 65. 216. 35. 13.6 117.8 50. 238. 20.	0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.0 0.0 00. 0. 0.0 0.0 00. 0.
120800Z 10.4 119.5 35 10.8 119.		11.0 114.3 35. 72. 10.	0.0 0.0 00. 0.	8.0 9.0 00. 0. 8.0 9.0 00. 0.
120806Z 10.0 118.1 35 9.9 118.	1 30. 65.	0.0 0.0 00. 0.	0.8 0.8 00. 0.	0.0 0.0 00. 0.
120812Z 9.9 117.1 30 9.6 116. 120818Z 10.0 116.1 30 10.0 116.		0.0 0.0 00. 0. 0.0 0.0 00. 0.	0.8	0.0 0.0 00. 0. 0.0 0.0 00. 0.
1289902 10.2 115.2 25 10.2 115.		0.0 0.0 00. 0.	0.0 0.0 00. 0.	0.0 0.0 00. 0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35					
	WRNG	24-HR	48-HR	72-HR	WRNG	24-HR	48-HR	72-HR		
AVG FORECAST POSIT ERROR	20.	139.	263.	280.	21.	136.	258.	269.		
AVG RIGHT ANGLE ERROR	14.	79.	149.	140.	15.	74.	145.	141.		
AVG INTENSITY MAGNITUDE ERROR	5.	19.	31.	39.	6.	19.	30.	37.		
AVG INTENSITY BIAS	3.	6.	11.	22.	3.	5.	в.	19.		
NUMBER OF FORECASTS	60	56	45	34	54	51	40	32		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 4291. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 10. KNOTS

TYPHOON PANELA FIX POSITIONS FOR CYCLONE NO. 27

SATELLITE FIXES

FIX	TIME	FIX				
NO.	(Z)	FIX POSITION	ACCRY		COIPENTS	
1	219399	8.6N 176.6E 8.2N 176.7E 8.5N 176.6E	PCN 6	T1.0/1.0	INIT DBS ULCC FIX INIT OBS ULAC 8.8M 176.1E ULAC 8.9M 175.9E	PGTW
3	211694	8.5N 176.6E	PCN 6	11.8/1.8	ULAC 8.91 175.9E	KGMC
4	220300	6.9N 178.1E	PCN 6	T1.0/1.0 /S0.0/24HRS T2.0/2.0 /D1.0/24HRS		PGTW
5	220307	9.0N 178.1E	PCN 4	T2.0/2.0 /D1.0/24HRS	ULAC 8.8N 177.5E ULAC 8.6N 177.2E EXP LLCC	KGMC
7	221551	8.3N 177.5E	PCN 6		ULAC 8.6N 177.2E	PGTW KGWC
8	221600	8.3N 177.6E	FCN 6			PGTW
19	230000	7.9N 177.6E 8.2N 176.9E	PEN 4	T2.0/2.0 /S0.0/24HRS	EXP LLCC	PGTW KGWC
11	230300	8.1N 177.1E	PCN 4	71.0/1.0-/S0.0/24HRS		PGTW
12	230600	8.2N 176.7E	PCN 6	T2.0/2.0 /50.0/24HRS T1.0/1.0-/50.0/24HRS	ULAC 9.4N 174.8E	PGTU
14	231200	7.7N 176.1E	PCN 6		OLHC 9.4N 174.8E	KGUC PGTW
15	231539	7.4N 175.4E	PCN 6		ULAC 9.4N 174.8E ULAC 7.1N 173.7E ULCC 7.3N 174.3E ULAC 6.4N 174.1E	KGUC
16 17	231600	7.0N 176.2E	PCN 6	T2.5/2.5 /D0.5/16HRS		PG FW KGWC
18	232100	7.5N 175.5E	PCN 6			PGTW
19	240000	7.0N 175.3E	PCN 6	T2.0/2.0-/D1.0/21HRS	18 AC 7 1N 127 7E	PGIW
21	240300	6.9N 175.1E	PCN 6	13.8/3.8 /00.3/00NR3	OLAC 1.IN 175.7E	KGWC PGTW
22	248600	6.9N 174.7E	PCN 6		ULCC 7.3N 174.3E	PGTW KGWC PGTW
23	240909	6.8N 174.5E	PCN 6		ULAL 6.4N 174.1E	KGWC PGTU
25	241200	7.0N 174.3E	PCN 6			PGTW
26 27	241527	6.6N 172.9E	PCN 6		ULAC 6.6N 173.2E	KGWC PGTW
28	241800	6.9N 173.2E	PCN 6		ULCC FIX	PGTW
29	242048	6.8N 171.9E	PCN 5	T4.8/4.8+/D1.0/18HRS T3.5/3.5 /D1.5/24HRS	ULCC 7.3N 174.3E ULAC 6.4N 174.1E ULAC 6.6N 173.2E ULCC FIX ULCC FIX	KGWC
31	250000	7.3N 172.3E	PCN 4	T3.5/3.5 /D1.5/24HRS	ULLL FIX	PGTW PGTW
32	250300	7.3N 171.8E	PCN 4			PGTW
33	250412	7.2N 171.5E	PCN 6			KGWC PGTW
35	250746	6.8N 170.4E	PCH 6			KGWC
36	250900	6.8N 170.9E	PCN 6		ULBC ETV	PGTW PGTW
37 38	251200	7.3N 170.7E	PCN 6		ULCC FIX	KGWC
39	251600	7.3N 169.9E	PCN 6			PSTW
40	251800	7.4N 169.6E	PCN 6	TA 5/A 5 /NA 5/2/UPS		PGTW KGWC
42	252100	7.6N 169.2E	PCN 6	T4.5/4.5 /D0.5/24HRS T4.0/4.0 /D0.5/24HRS	ULCC FIX	PGTW
43	260000	8.0N 168.8E	PCN 4	T4.0/4.0 /D0.5/24HRS		PGT U
45	269499	8.2N 168.3E 8.3N 168.1E	PCN 3			PGTW PGTW
46	260400	8.2N 167.8E	PCN 1			KGWC
47 48	260600 260900	8.2N 167.8E 8.4N 167.8E 8.6N 167.6E	PCN 4			PGTU PGTU
49	260906	8.9N 167.0E	PCN 6			KGWC
50	261200	9.1N 166.4E	PCN 6 PCN 4			PGTW PGTW
52	261645	9.5N 165.7E 9.5N 165.4E 9.5N 165.2E	PCN 2			PGTW
53	261645	9.5N 165.2E	PCN 2			KGWC
	261800 262000	0 00 464 45		T5.5/5.5 /D1.0/24HRS		PGTW KGWC
56	262100	9.7N 164.7E	PCN 2	T4.5/4.5 /D0.5/24HRS		PGTW
57 58	270000 270348	10.8N 164.1E	PCN 2 PCN 2	T4.5/4.5 /00.5/24HRS	EYE OPEN SE	PGTW PGTW
59	270600	10.5H 163.0E	PCN 2			PGTW
60	210300	10.7N 162.6E 11.0N 162.1E	PCN 2 PCN 2			PGTW PGTW
62	271600	11.4N 161.4E	PCN 2			PGTW
63	271800	11.6N 161.2E	PCN 2			PGT₩
	272118 280000	11.7N 161.0E 11.7N 160.1E	PCN 3 PCN 2	T5.5/5.5 /D1.0/24HRS		PGTW PGTW
66	280336	12.3N 159.8E	PCN 2		EYE DIA 35NM	PGTW
67 60	280600	12.4N 159.6E	PCN 2 PCN 4			PGTW PGTW
69	281200	12.5N 159.5E 12.5N 159.0E	PCN 4		ULCC FIX	PGTW
70	281600	12.6N 158.8E	PCN 6			PGTW
	281800 282054	13.1N 158.7E 13.5N 158.7E	PCN 6 PCN 3			PGTW PGTW
73	290000	13.7N 158.4E	PCN 2	T4.5/5.0+/W1.0/24HRS		PGTW
	290300		PCN 4			PGTW
	298688 298988	13.7N 158.2E 13.7N 158.2E	PCN 6 PCN 6		ULCC FIX	PGTW PGTW
77	291200	13.7N 157.8E	PCH 6			PGTW
78 79	291600 291608	13.4H 157.7E 13.4H 157.7E	PCN 6 PCN 5		ULAC FIX ULAC FIX	PGTW PGTW
80	291800	13.3N 157.6E	PCN 6		ULAC FIX	PGTW
		13.0N 157.2E	PCN 6	TZ SZA GŁAN G ZGAUDO	באם וורר	PG IW
82 83	300300	12.4N 156.0E 12.4N 155.5E	PCN 4 PCN 6	T3.5/4.0+/W1.0/24HRS	EXP LLCC	PGTW PGTW

64	300453	12.3M 155.2E	PCN 5			PG TW
85	300600	12.2N 155.1E	PCN 6			PGTW
86	300909	11.9N 154.1E	DCH C			PGTW
87	301200	11.5N 153.5E	PCH 6 PCH 4		111.0C 10 111 1FF 5F	
88	301600	11.58 155.55	PEN 4		ULAC 12.1H 155.6E	PGTW
		11.5N 152.5E	PCN 4		EXP LLCC	PGTW
89	301738	11.7N 152.0E	PCH 3			PG I W
98	301800	11.7N 152.0E	PCH 4			PGTW
91	302100	11.8N 151.1E	PCH 4			PGTW
92	302148	11.7N 151.1E	PCN 5			PGTW
93	010000	11.8N 150.3E	PCN 6			PGTW
94	010300	12 ON 140 OF	PCN 6			
	010441	12.0N 148.9E				PSIW
95		12.1N 148.2E	PCN 3	T3.0/3.0+/W0.5/2BHRS		PGTW
96	010600	12.1N 147.4E	PCN 4			PGTW
97	010900	12.2N 146.1E	PCN 6			PGTW
98	011200	12.2N 145.2E	PCN 4			PGTW
99	011600	11.9N 144.1E	PCH 6		ULCC FIX	PGTW
	011800	12.0N 143.2E	PCN 6		ULCC FIX	PGTW
101	012100	12.0N 141.7E	PCN 6		ULCC FIX	PGTW
182		12.011 141.15			DECC FIA	
	012305	12.0N 141.8E	PCN 5			PGT₩
103	020000	12.0N 141.5E	PCN 4			PGTW
104	020300	12.3N 140.3E 12.0N 140.1E	PCH 4	T1.5/2.5 /W1.5/22HRS T2.0/2.0+	EXP LLCC	PGTW
105	020300	12.0N 140.1E	PCH 4	T2.0/2.0+	INIT OBS	RPMK
106	020611	12.0N 139.2E	PCN 3		EXP LLCC	PGTW
187	020900	12.1N 138.5E	PCN 6			PGTW
108	021200	12.0N 137.2E	PCH 6		ULCC FIX	PGTW
109	021600	12.011 137.22	PCN 6		OLCO I IA	
		12.8N 136.0E			ULCC ETY	PGTW
	021800	13.2N 135.3E	PCN 6		ULCC FIX	PGTW
	022100	13.5N 134.8E	PCN 6			PGT₩
112	022241	13.5N 134.6E	PCN 5			PGTW
113	030000	13.6N 134.7E	PCN 6			PGTW
114	838388	13.8N 134.1E		T3.0/3.0 /D1.5/24HRS		PGTW
115	030559	14.4N 133.4E	PCN 5	1010-010-0111-0-1111	ULAC FIX	PGTW
116	030900	14.411 133.40	PCN 6		ULAC FIX	PGTW
		14.7N 132.8E 15.0H 132.1E	PCN 6		DEMC FIX	
117	031200	15.0H 132.15				PGTW
	031600	15.2N 131.6E	PCN 6			PGTW
119	031800	15.3N 131.4E	PCN 6			PGTW
120	031843	15.4N 131.3E	PCN 5			PGTW
121	032100	15.4N 131.3E	PCN 6			PGTW
122	032217	15.3N 131.5E	PCN 3			RPMK
123	040000	15.6N 131.3E	PCN 6		ULAC FIX	PGTW
124	040300	10.00 131.32	DCH 4	T4.0/4.0-/D1.0/24HRS	ULAC FIX	PGTW
		16.0N 130.7E		14.874.8-701.87246K3		
125	040546	16.3N 130.8E 16.3N 130.8E 15.9N 130.5E	PCN 5		ULAC FIX	PGTW
126	040600	16.3N 130.8E	PCN 6		ULAC F1X	PGTW
127	040900	15.9N 130.5E	PCN 6		ULAC FIX	PGTW
128	041200	15.8N 130.2E	PCN 4			PGTW
129	041600	15.9N 129.8E	PCN 2			เมากา
130	041831	16.0N 129.6E	PCH 1			PGTW
131	042100	16.0N 129.6E	PCN 2			PGTW
132	042335	16.0N 129.9E		T5.0/5.0	INIT OUS	RODH
133	050000	16.00 123.3E	PCH 1	13.0/3.0	1111 003	PGTIJ
		16.2N 129.5E	PCN 2			
134	050300	16.2N 129.4E		T5.0/5.0-/D1.0/24HRS		PGT₩
135	050534	16.1N 129.4E	PCN 1			PGT₩
136	050600	16.4N 129.6E	PCN 2			PGTW
137	050900	16.7N 129.6E	PCN 6		ULAC FIX	PGTW
13B	051200	16.7N 129.3E	PCN 6			PGTW
	051600	16.8N 129.0E	PCN 6		ULCC FIX	PGTW
	051800	17.1N 128.9E	PCN 6		ULCC FIX	FGTW
14!	052100	16.7N 130.5E	PCN 6		BRKS CONTINUITY	PGTW
		10.111 130.35	ECH E	T4 8 # 9 411 8 C 4100		
142	052310	16.4N 129.7E		T4.0/5.0 /W1.0/24HRS	ULCC FIX	RODH
143	060000	15.7N 129.3E	PCN 6		ULAC 16.0N 128.4E	PGTW
	0 60300	15.6N 129.0E 15.5N 128.3E		T3.5/4.5-/W1.5/24HRS		PGTW
145	060552	15.5N 128.3E	PCN 6			PGTW
146	069699	15.3N 128.2E	PCN 6			PGTW
147	060900	14.8N 127.7E	PCN 6		ULAC FIX	PGTW
148	061200	14.9N 127.1E	PCN 6		=::= : =::	PGTW
	061600	14.5N 126.2E	PCN 6			PGTW
150	061807	14.3N 126.2E	PCN 5			PGTW
151	062100	13.8N 125.7E	PCN 6		**** ***	PGTW
152	862247	13.3N 125.7E		T4.0/4.0~	INIT OBS	RPMK
153	070000	13.3N 125.3E	PCN 4			PGTW
154	070300	13.3N 125.0E	PCN 6			PGTW
155	070600	13.0N 124.0E	PCH 4	T4.0/4.5-/D0.5/27HRS		PGTW
156	070652	13.1N 123.9E	PCN 5			RPMK
157	070900	13.0N 123.2E	PCH 6			PGTW
	071200	13.0N 122.6E	PCN 6			PGTW
	071537	10.3N 120.7E	PCN 3		EXP LLCC	RPMK
	080004	9.8N 119.6E	PCN 3		LA LLUG	RPMK
100	500004	J.ON 113.BE	run 3			RECK

AIRCRAFT FIXES

FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB ORS HGT MSLP	MAX-SEC-UMD VEL/BRG/RNG	MAX: FLT-LVI. DIR/VEL/BRG.			EYE SHAPE	EYE ORIE		
1 2 3 3 4 4 5 6 6 7 7 8 9 9 100 11 11 12 11 15 11 16 11 17 18 18 12 12 12 13 3 14 11 15 12 12 12 13 13 14 15 15 16 16 17 17 18 18 18 18 18 18 18 18 18 18 18 18 18	260625	7.5N 169,4E 7.7N 169,2E 8.5N 167,6E 8.8N 167,0E 9.8N 164.5E 10.5N 162.3E 11.6N 160.6E 11.7N 160.6E 11.7N 160.6E 11.7N 150.4E 13.7N 158.4E 13.7N 158.4E 13.7N 158.4E 13.7N 158.4E 13.7N 158.4E 11.5N 150.5E 12.3N 156.6E 11.5N 150.5E 12.3N 156.4E 11.5N 150.5E 12.1N 149.7E 11.5N 150.4E 11.5N 150.4E 11.5N 150.4E 11.5N 150.5E 11.5N 150.4E 11.5N 130.4E 11.5N 130.4E 11.5N 130.4E 15.5N 131.3E 15.5N 131.3E 15.5N 131.3E 15.5N 130.4E 15.9N 120.7E 15.9N 120.7E 15.9N 120.7E 15.1N 120.9E 15.2N 120.7E 15.2N 120.5E 15.4N 120.5E	700118 700118	2959 2963 2899 2894 2817 2816 967 2585 948 2577 2647 2673 2673 2673 2673 2673 2673 3016 992 3029 3016 992 3075 3093 3085 998 3075 3093 3098 3098 3098 3098 3098 3098 3098	45 288 18 68 138 15 25 188 120 70 170 7 90 828 8 58 350 48 118 158 18 70 188 18 50 208 38 75 228 12 88 368 78 35 888 198 55 270 18 45 310 17 35 360 18 50 318 15 45 270 7 55 320 8 35 260 18 56 290 15 67 390 5 68 360 5 88 360 5	330 36 288 208 46 128 340 36 230 200 73 110 650 72 340 360 53 280 170 98 99 670 77 320 170 98 99 670 77 320 180 197 99 249 197 190 180 197 99 210 110 150 150 100 042 280 75 210 020 55 29 020 55 29 020 55 29 020 50 270 080 63 330 200 25 29 080 63 330 200 54 040 060 29 360 1	30 40 5 18 7 30 30 15 20 15 10 45 130 70 127	7775751033558565533433555532335522353223 10121177751086661010101010101010101010101010101010	ELLIPTICAL CIRCULAR ELLIPTICAL ELLIPTICAL ELLIPTICAL ELLIPTICAL	12 5 22 25 15 15 15 28 35 15 40 20 10 18 20 18 20 18	+13 +14 + +13 +16 + +12 +17 + +15 +19 + +14 +15 +19 + +11 +15 + +13 +18 + +12 +20 + +13 +17 + +14 +16 + +14 +16 + +13 +12 + +18 +18 + +13 +12 + +18 +18 + +19 + +10 +12 + 6 +12 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +17 +19 + +18 +18 +18 + +19 + +19 +19 + +10 +12 + +10 +12 + +110 +12 + +111 +12 + +111 +12 + +12 + +13 +13 + +13 +13 + +14 +15 + +15 +15 + +16 +19 + +16 +19 + +16 +19 + +16 +19 + +17 +17 + +17 +18 +18 + +18 +18 +18 + +19 + +19 +19 + +110 +12 + +111 +12 + +111 +12 + +111 +12 + +111 +12 + +111 +12 + +111 +12 + +111 +12 + +111 +12 + +12 +13 + +13 +13 + +13 +13 + +13 +13 + +14 + +14 + +14 + +15 + +15 + +16 + +16 + +16 + +17 + +16 + +17 + +17 + +17 + +18 +	-13
FIX	TIME	FIX		EYE		FIXES					Donan	0. -
NO.	(Z)	POSITION	RADAR AC	CRY SHAPE		ASWAR TODEF		C	OMMENȚS		RADAR POSITION	SITE WMB NO.
13 14 15 16 17 18 19 20 21	061500 061600 061700 061800 061900 070000 070600 070600 070800 071100	8.2N 167.9E 8.3N 167.8E 8.8N 167.0E 9.0N 166.4E 9.2N 166.2E 12.3N 145.1E 12.3N 144.4E 12.4N 144.4E 12.6N 144.2E 14.4N 127.0E 14.2N 127.0E 14.2N 127.0E 14.1N 126.4E 13.8N 126.4E 13.8N 126.4E 13.4N 125.4E 12.5N 123.9E 12.4N 123.7E 11.9N 122.9E 11.8N 122.9E	LAND FILAND FILAND FILAND FILAND LAND LAND LAND LAND LAND LAND LAND	AIR AIR AIR AIR AIR AIR AIR AIR AIR		35220 42215 35210 41811 18331 42408 18221 42408 18211 52419 18211 52219 18331 52707 18432 42718 18412 42518 18412 42610 18312 42713 18312 42512	EYE	C IRCULAF C IRCULAF C IRCULAF	₹		8.7N 167.7 8.7N 167.7 8.7N 167.7 8.7N 167.7 8.7N 167.7 13.6N 144.9 13.6N 144.9 13.6N 144.9 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3 14.0N 124.3	E 91366 E 91366 E 91366 E 91366 E 91366 E 91218 E 91218 E 91218 E 91218 E 98447
	TIME	FIX		/ NEAREST	SYNOPTI	C FIXES						
NO.	(Z) 250420	POSITION	ESTIMATE	DATA (NM)		COMMENTS						
2	260610	7.3N 171.8E 8.5N 167.7E 12.2N 123.3E	050 065 045	025 015 016	WMO 913 WMO 985	66 KWAJALEIN						

TYPHOON ROGER BEST TRACK DATA

	BEST TR	ACK		WIRH:				24 HC	OUR FO	ORECAS			48 HC	UR FO				72 HC		RECAS	
						ROPS				ERRO	IRS				ERRU	₹S			E	RRORS	
MO/DA/HR	POSIT WI	MD	POSIT	MIND	DST	MIND	P09	31T	dilli	DST	MIND	POS	ĮΤ	MIND	DST	WIND	POS	ΙT	MIND	DST	UIND
120706Z	10.1 130.8	25	0.0 0.0	9.	-0.	0.	0.0	0.0	ø.	-0.	0.	8.0	0.9	0.	-0.	ø.	0.0	0.0	ø.	-8.	0.
1207122	10.8 [29.1	35	0.0 0.0	9.	-0.	ø.	0.0	0.0	0.	-·ø.	ø.	0.6	0.0	ø.	Ø .	0.	0.0	0.0	ø.	-0.	ē.
120718Z	11.5 127.2	40	0.0 0.8	9 0.	-·e.	ø.	0.0	0.0	0.	-9.	ø.	0.0	0.0	ø.	B.	Θ.	0.0	9.8	ø.	-0.	ø.
120800Z	12.4 125.5	50	11.8 125.7	50.	38.	0.	13.5	120.3	45.	134.	-20.	13.3	116.8	55.	433.	15.	0.0	0.0	ø.	-ø.	ä.
120806Z	13.2 124.2	55	12.8 124.3	2 50.	24.	~5.	13.B	119.0	50.		-15.	14.0	114.2	55.	549.	25.	0.0	0.0	В.	-0.	e.
1208122	13.8 123.3	55	14.2 123.6	55.	30.	ø.	16.3	120.0	50.		-10.	18.4	118.1	35.	243.	10.	0.0	0.0	a.	-0.	ø.
1208182		60	14.4 122.4		6.	ø.		119.3	45.	185.	-5	18.8	117.0	35.	307.	10.	я.я	0.0	ø.	-0.	e.
1209002		65	15.1 122.6		6.	ø.		119.5	50.	175.	18.	0.0	0.0	В.	-A.	Ø.	8.0	0.0	ø.	-0.	e.
1209062		65	15.6 121.5		21.	ø.		119.8	50.	158.	20.	0.0	0.0	0.	-0.	8.	0.0	0.0	ø.	-0.	o.
1209122		68	16.4 122.2		6.	В.		122.4	45.	25.	20.	0.0	0.0	В.	-0.	ø.	ю.9 И.Я				
1209182		50				٠.		122.8										0.0	ø.	-0.	ø.
					8.	٥.	19.8		45.	29.	20.	0.0	0.0	ø.	-0.	0.	0.0	0.0	в.	-0.	0.
1210002		40	17.8 122.8		21.	15.	0.0	0.0	0.	-0.	9.	១.ខ	0.0	ø.	-0.	Я.	0.0	0.0	0.	-0.	0.
1210062	18.5 122.5	30	18.5 122.5	30.	0.	0.	0.6	0.0	Ð.	-0.	в.	0.8	0.0	ø.	-0.	0.	0.0	0.0	0.	-0.	0.
1210122	19.2 122.3	25	18.7 122.4	30.	31.	5.	0.0	0.0	0.	-0.	0.	0.0	0.0	8.	-⊌.	0.	0.0	0.0	0.	-0.	0.
1210182	19.9 122.3	25	19.8 122.2	25.	8.	Ø.	0.0	0.0	0.	-0.	и.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	0.

	ALL	FORECAS	TS		TYPHOONS WHILE OVER 35 KTS					
	WRNG	24-HR	48-HR	72-HR	HRHG	24HR	48~HR	72-HR		
AVG FORECAST POSIT ERROR	17.	129.	383.	0.	18.	165.	433.	0.		
AVG RIGHT ANGLE ERROR	12.	116.	329.	0.	15.	148.	319.	0.		
AVG INTENSITY MAGNITUDE ERROR	3.	15.	15.	0.	3.	12.	15.	€.		
AVG INTENSITY BIAS	2.	3.	15.	0.	2.	-8.	15.	0.		
NUMBER OF FORECASTS	12	8	4	8	9	5	1	8		

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 906. NM
AVERAGE SPEED OF TROPICAL CYCLONE IS 11. KNOTS

TYPHOON ROGER FIX POSITIONS FOR CYCLONE NO. 28

SATELLITE FIXES

FIX	TIME	FIX				
NO.	(2)	POSITION	ACCRY	DVORAK CODE	COMMENTS	STIE
1	041800	5.3N 145.3E	PCN 6		ULCC FIX	PGT⊎
ż	050000	6.0N 145.7E	PCN 6	T1.0/1.0	INIT OBS	PGTU
3	050300	4.4N 142.2E	PCN 4			PG TW
4	050534	4.0N 141.7E	PCN 3			PGTU
5	050600	4.0N 141.7E	PCN 4			PSTU
6	050900	4.3N 141.1E	PCN 6		ULAC FIX	PGTU
7	051200	4.7H 141.0E	PCN 6		ULCC FIX	PGTH
8	051600	5.3N 138.9E	PCN 6		ULCC FIX	PGTU
9	060000	7.4N 137.5E	PCN 6	T0.5/0.5 /W0.5/24HRS		PGTM
ıõ	060300	7.7N 137.1E	PCN 6	1010-010-1010-1-1111		РСТЫ
11	071800	11.2N 127.0E	PCN 6		ULCC FIX	PGTW
12	072100	11.3N 126.6E	PCN 6			PGTU
13	080000	12.6N 126.0E	PCN 4	T3.5/3.5~	INIT OBS	PGTW
14	080004	12.1N 126.0E	PCN 3	T3.0/3.0	INIT OBS	→ RPIK
15	080300	12.6N 124.8E	PCN 6			PGTU
16	080600	13.4N 124.5E	PEN 4			PGTW
17	080639	13.2N 124.1E	PCN 3			RPNK
18	080900	13.8N 124.4E	PCN 6			PG TW
19	081200	14.1N 123.9E	PCN 6			PGTW
20	081600	14.5N 122.9E	PCN 4			PGTIJ
21	081800	14.7N 122.6E	PCN 4			PGTW
22	081924	14.5N 122.3E	PCN 3			R19R
23	082100	14.8N 122.2E	PCN 2			PGTW
24	082340	15.0N 122.2E	PCN 1	T4.5/4.5 /D1.5/24HRS		RPHK
25	090000	15.0N 122.1E	PCN 2	T4.5/4.5-/D1.0/24HRS	•	PGTU
26	090300	15.3N 121.8E	PCN 2			PGTIJ
27	090627	15.6N 121.7E	PCN 3			PG IN
2B	090900	16.0N 121.7E	PCN 4			PGTW
29	090900	15.9N 122.1E	PCN 2			RPLIK
30	091200	16.4N 121.9E	PCN 6			PGTU
31	091600	17.1N 122.4E	PCN 6			PG (W
32	091800	17.4N 122.5E	PCN 6			PG TW
33	091912	16.7N 123.0E	PCN 3		EXP LLCC	RPMK
34	091912	17.2N 122.5E	PCN 6			RODII

35 * 36 37 * 38 39 40 41	092316 100000 100300 100615	17.7N 122.8E 17.5N 124.2E 17.7N 123.4E 17.5N 124.0E 18.6N 122.5E 19.8N 122.2E 20.1N 122.4E	PCN 6 PCN 5 PCN 6 PCN 6 PCN 5 PCN 4 PCN 4			1.8/24HRS 1.5/24HRS			ULCC ULCC EXP L	FIX				PG IN PETIK PGTW PGTW PGTW PG IN PGTW		
42 43 44	110000 110300	20.5N 122.7E 20.8N 122.9E 21.3N 123.3E		T0.5/	1.5 ∕₩	2.5/24HRS	3		EXP L	LCC				PGTW PGTW PGTW		
						A	IRCR	AFT F	IXES							
FIX NO.	TIME (Z)	FIX POSITION	FLT LVL	700MB HGT	OBS MSLP	MAX-SFC- VEL/BRG/			FLT-LYL VEL/BRG				EYE SHAPE	EYE ODIEN-	EYE TEMP	
	072349 100627 100917	12.8N 125.9E 18.5N 122.5E 18.6N 122.4E	700MB 700MB 700MB	3099 3113 3123	1002 1004	50 270 30 240 25 360	10 9 20	168 200 100	65 080 34 090 15 360	120	16 5 3	3 3 2			+12 + 8 +15 + 7 +11 +13 + 6	7 2
						R	ADAR	FIXE	S							
FIX NO.	TIME (Z)	FIX POSITION	RADAR A	CCRY	EYE SHAPI				-CODE TDDFF			c	OPTENTS		RADAR POSITION	SITE WNO NO.
2345678991111211415516718922122324	888488 888938 881928 881120 881280 881380 881480 881780 881780 881780 881780 981780 99180 99180 99130 99130 89130 99130 891480 991430 891480	12.8N 125.0E 13.6N 124.5E 13.7N 123.0E 13.8N 123.7E 13.8N 123.4E 13.9N 123.4E 14.4N 123.2E 14.5N 122.5E 14.7N 122.5E 14.7N 122.5E 14.7N 122.5E 14.7N 122.5E 14.7N 122.5E 14.7N 122.5E 15.5N 121.9E 15.5N 121.9E 15.5N 121.9E 16.6N 122.1E 16.1N 122.1E 16.5N 122.3E 16.6N 122.3E 16.7N 122.3E 16.7N 122.3E 17.0N 122.3E	LAND LAND LAND LAND LAND LAND LAND LAND					10422 10433 25/43 10121 20/31 20/21 11:131 12:2131 10:63/ 11:79/ 10:412 10:412 10:412 10:412 10:41/ 10:41/ 10:51/ 10:41/	50808 42718 42911 42909 62283 43222 49900 43211 42709 42702 42902 42902 42902 42902 40303 40103 40103 40104 40104 40000	EYE	: 90 : 100 : 100	PCT PCT PCT	CIR DIA 350 CIR DIA 3500 ELPTCL DIA ELPTCL DIA	KNS IS OPIL SC 49/38/K15 49/38/K16	14.00 124.36 14.00 124.36 14.00 124.36 14.00 123.06 14.10 123.06 14.10 123.06 14.10 123.06 14.10 123.06 14.10 123.06 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66 16.30 120.66	98447 98447 98447 98446 98446 98446 98446 90443 90448 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321 98321
						SYN	OPTIO	FIX	ES							

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSITION	INTENSITY ESTIMATE	NEAREST DATA (NM)		COMPLENTS
1 2	080900 081400	13.5N 123.8E 14.0N 122.9E	055 050	020 005	WMO 98444, WMO 98440	98447
3	090300	15.4N 121.6E	850	030	W10 98333	

2. NORTH INDIAN OCEAN TROPICAL CYCLONES

TROPICAL CYCLOHE 28-82 BEST TRACK DATA

BEST TRACK WARNING				24 HOUR FORECAST 48 HOUR FORECAST					ST	72 HOUR FORECAST													
								RORS				ERRO					ERRO					ERRURS	
MO/DA/HR	POSI	T	MIND	POS	IT	HIMD	DST	WIND	£0\$	IT	UIND		MIND	FOS	IT	HIND		WIND	POS	LT	MIND		MIND
043002Z	11.4	82.7	28	9.0	0.0	ø.	-0.	ø.	0.0	0.0	0.	-0.	8.	0.0	9.0	ø.	٠ ٤١ .	ø.	0.0	0.0	Ø.	-Ø.	ø.
043008Z	12.0	82.4	25	0.0	9.9	0.	-U.	Ю.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-0.	ø.	0.0	9.9	Θ.	-0.	Ø.
0430147	12.7	82.1	25	0.0	0.0	Ø.	-0.	Ø.	0.0	0.0	0.	-0.	0.	9.8	9.0	ø.	-8.	0.	0.0	0.0	G.	-0.	0.
043020Z	13.5	82.0	25	0.0	0.0	Θ.	-Ø.	0.	0.0	0.0	0.	-8.	Θ.	0.0	0.0	ø.	(i) .	0.	0.0	0.0	11.	-3.	Э.
9 50102Z	14.3	82.2	30	0.0	0.0	8.	-0.	ø.	0.0	0.0	0.	-0.	0.	0.0	0.0	ø.	-Ø.	ø.	0.0	6.B	n.	-n.	Θ,
050106Z	14.8	82.5	30	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ø.	-0.	в.	Ø.0	0.0	ø.	· G.	U.	0.0	81.0	Г.	~ p1	₺).
050114Z	15.3	82.8	35	0.0	0.0	ø.	-⊌.	0.	0.0	0.0	е, "	-0.	0.	0.0	0.0	0.	- ค.	, U.	и.е	9.0	4.	-: U.	٠.
050120Z	15.8	83.3	35	0.0	0.0	ø.	-0.	0.	0.0	0.0	0.	-∙Ð.	ก.	0.0	0.0	ø.	-0.	€.	0.8	0.0	9.	− 1,),	и.
05 0202Z	16.2	83.8	40	16.2	82.8	25.	58.	-15.	17.8	84.1	40.	159.	-48.	19.8	86.2	50.	304.	-70.	ទេ.ខា	89.3	69.	449.	19.
050208Z	16.4	84.4	50	16.7	83.8	30.	39.	-20.	17.9	86.9	45.	55.	-45.	18.6	90.1	55.	194.	-70.	19.0	93.4	65.	232.	30.
050214 Z	16.8	85.2	60	16.8	84.8	60.	23.	0.	18.1	86.9	70.	122.	-30.	18.8	89.2	70.	330.	-25.	0.0	0.0	u.	-0	0.
050220Z	17.0	85.9	70	17.0	85.2	65.	40.	-5.	18.1	87.0	75.	186.	-35.	19.1	89.3	89.	193.	10.	0.0	ย.ย	υ.	-શ.	6.
0503022	17.2	86.8	89	17.3	86.8	65.	6.	-15.	18.2	89.5	75.	111.	-45.	19.0	92.2	85.	277.	35.	0.0	0.0	н.	-ø.	e.
050308Z	17.4	87.7	90	17.5	87.8	75.	8.	-15.	18.1	90.9	85.	142.	-40.	10.6	94.1	75.	189.	48,	0.0	ខ.ភ	ი.	0.	Θ.
0 50314Z	17.4	88.9	190	17.6	88.7	85.	17.	-15.	18.1	92.0	85.	165.	-18.	0.0	0.0	ø.	-ც.	a.	0.0	ย.ศ	14	-0	я.
0 503202	17.5	90.2		17.7	89.8	95.	26.	-15.	17.8	94.2	90.	115.	29.	0.0	0.0	ø.	-0.	0.	0.0	0.0	.1.	-0.	8.
0 50402Z	17.5	91.3		17.4	91.2	120.	8.	0.	17.7	95.6	90.	75.	43.	0.0	0.0	ø.	Ø.	ø.	ଜ.ଜ	0.0	41.	-0.	Θ.
050408Z	17.5	93.3		17.5	93.0	130.	17.	5.	17-8	98.2	40.	52.	5.	8.0	0.0	е.	-0.	Ю.	0.0	0.9	.1.	-0.	0.
050414Z	17.4	94.8		17.5	94.9	100.	8.	5.	0.0	0.0	0.	-0.	۴.	0.0	0.0	ø.	-0.	Β.	0.0	6.9	9.	-ø.	Θ.
050420Z	17.6	96.2	70	17.5	95.9	65.	18.	-5.	0.0	0.0	0.	-0.	0.	0.8	0.0	0.	r,	Θ.	0.0	3.0	ŋ.	-⊕.	0.
050502Z	17.8	96.9	50	17.4	97.2	50.	30.	0.	0.8	0.8	0.	G.		ର.ଡ	8.8	ø.	-0.	ย.	0.0	0.0	θ.	−8.	0.
05050BZ	18.2	97.4	35	17.0	97.2	35.	27.	Θ.	9.0	0.0	0.	-0.	Θ.	0.0	0.0	0.	-0.	ø.	0.9	я.п	0.	- છ.	0.

		TYPHOONS WHILE OVER 35 KTS							
f	WRNG	24-HR	48-HR	72-HR	URNG	24-HR	48-HR	72-HR	
AVG FORECAST POSIT ERROR	23.	118.	283.	340.	0.	Ø.	0.	Ю.	
AVG RIGHT ANGLE ERROR	14.	43.	87.	116.	υ.	ø.	0.	0.	
AVG INTENSITY MAGNITUDE ERROR	8.	31.	42.	20.	0,	ø.	Ø.	И.	
AVG INTENSITY BIAS	-7.	-18,	-13.	20.	0.	0.	Ø.	Ø,	
NUMBER OF FORECASTS	14	10	6	2	8	И	И	U	

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 1135, NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

9. KNOTS

TC20-82 FIX POSITIONS FOR CYCLONE NO. 20

SATELLITE FIXES

	ix o.	TIME (Z)	F]X POSITI		ACCRY	DYORAK CODE	CONTENTS	SITE
*	1	240820	4.3N	89.2E	PCN 5	T1.0/1.0	INIT OBS ULAC 2.4N 90.7E	KGUC
*	2	242115	4.7N	86.9E	PCN 6	•	ULAC 2.8N 87.0E	KCUC
	3	300900	12.0N	82.0E	PCN 5	T1.5/1.5	INIT OBS ULAC 12.8N 81.0E	KGUC
	4	301435	12.2N	81.8E	FCN 6			KGMC
	5	302144	13.6N	82.1E	PCN 6		ULAC FIX	KGWC
	6	302145	13.0N	82.0E	PCN 6			FJDG
	7	010300	14.6N	82.4E	PCN 5	T2.0/2.0	INIT OBS ULCC FIX	PRTU
	В	010848	15.1N	82.6E	PCN 5	T3.0/3.0 /D1.5/24HRS	ULAC FIX	KUPIC
	9	010848		82.9E	PCN 6			FJDG
*	10	011200		81.7E	PCN 5			PGTW
	11	011412		83.1E	PCN 6		ULAC FIX	KGUC
*	12	011800		82.ØE	PCN 5			₽GTW
	13	012132		83.0E	PCN 6		ULAC FIX	KGWC
	14	020250		84.5E	PCN 5		-	KGWC
	15	020300		83.2E	PCH 5	T3.0/3.0 /D1.0/24HRS		PGTIJ
	16	020836		84.6E	PCH 5	T4.5/4.5 /D1.5/24HRS		KGIJC

1	7 021200	16.6N	84.2E	PCN 5				есты
ı	8 021348	16.7N	85.0E	PCN 4		EYE DIA		KGWC
1	9 021348	17.3N	84.5E	PEN 6		21		JDG
2	021600	16.6N	84.8E	PCN 1				PGTW
2	1 021800	16.7N	85.1E	PCN 1				GTW.
2	2 022120	17.0N	86.0E	PCN 2		EYE DIA		KGWC
2	3 030227	17.1N	86.9E	PCN 1		EYE DIA	•	KGIJC
2	4 030300	17.2N	86.4E	PCN I	T4.5/4.5 /D1.5/24HRS			PGTW
2	5 030600	17.4N	87.0E	PCN 1				GTW
2	6 030823	17.4N	87.7E	PCN 1	T6.0/6.0 /D1.5/24HRS	EYE DIA		CGWC
2	7 031200	17.4N	88.4E	PCN 1		2.2 2	· ·	PGTW
2	B 031324	17.6N	88.7E	PCN 2		EYE DIA		(GWC
2	9 031600	17.4N	89.2E	PCH 1				หราย
3	031800	17.4N	89.6E	PCN 1				GTW
3	1 032100	17.4N	90.3E	PCN 1	•			GTIJ
3		17.4N	90.2E	PCN 1		EYE DIA		GWC
3	3 040203	17.3N	91.9E	PCN 1		EYE DIA	•	GWC
3		17.5N	91.7E	PCH 1	T5.5/5.5-/D1.0/24HRS			GTW
3		17.5N	92.5E	PCM 1				GTW
3		17.3N	93.5E	PCN 1	T5.5/6.0-/W0.5/24HRS	EYE DIA		GUC
3		17.6N	93.4E	PCN 1				GTW
3		17.6N	94.1E	PCN 1				GTW
3		17.6N	94.8E	PCN 3				GTW
4		17.5N	95.4E	PCN 3				GTW
4		17.6N	96.6E	PCH 6				GWC
4		17.5N	96.4E	PCN 5		ULCC F1		GTW
4		17.5N	96.8E	PCN 5				'GTW
4		17.7N	97.0E	PCN 5	T3.0/4.0 /W2.5/24HRS			GTIJ
* 4		17.7N	99.2E	PCN 5	T3.0/4.0 /W2.5/24HRS			GUC
* 4	5 250818	4.0N	85.2E	PCN 5	T0.5/1.0 /W0.5/24HRS			GWC

NOTICE - THE ASTERISKS (*) INDICATE FIXES UNREPRESENTATIVE AND NOT USED FOR BEST TRACK PURPOSES.

TROFICAL CYCLONE 22-82 BEST INACK DATA

		BEST 1	TRACK			unrn1		RORS		24 HL	JUR FO	RECO			48 H	MIR FE	ORECAS ERECA			72 HO		RECAS RRORS	т
MO/DA/HR	POST	T 1	CH1L	POS	tr	MIND		MILLE	POS	tT.	UHID	DS1	IJIND	205	17	ыны			500				
060120Z	16.9	89.5	25	0.0														MIND	P051		MIHD		MIND.
	10.5				0.0	0.	-0.	0.	0.0	0.6	Θ.	-0.	8.	0.0	9.9	0.	- 0.	8.	0.0	0.0	0.	-0.	а.
060202Z	17.3	89.3	30	0.0	0.0	0.	-0.	0.	9.0	0.0	Θ.	-0.	0.	0.8	8.8	0.	-8.	0.	0.0	0.8	в.	ø.	9.
060208Z	17.7	89.1	30	18.2	88.9	30.	32.	ø.	19.6	86.3	40.	40.	-15.	21.0	88.2	40.	238.	10.	0.0	8.8	ø.	-A.	ø.
0 60214Z	18.0	88.7	35	18.5	88.8	35.	31.	0.	19.8	80.2	40.	80.	-15.	0.0	8.8	0.	-0.	a.	Э.В	0.0	я.	-0.	e.
0602202	18.3	88.2	40	18.6	88.5	40.	25.	ø.	19.5	87.9	45.	148.	ø.	4.0	Ø.8	ø.	-0.	0.	0.0	0.0	8.	-a.	ø.
0603027	18.8	87.9	45	19.0	87.9	45.	12.	e.	26.8	86.8	45.	123.	5.	11.14	8.6	Ð.	~A.	ø.	0.0	0.0	9.	-0.	0.
060308Z	19.6	87.6	55	19.7	87.2	45.	23.	-10.	22.2	86.8	48.	134.	10.	0.0	0.0	Ð.	.0.	0.	0.0	0.0	0.	-8.	0.
868314Z	20.2	86.7	55	20.2	87.1	45.	23.	-ie.	0.0	0.0	Ø.	-0.	U.	8.0	0.0	0.	- Ð.	ø.	0.0	0.0	9.	-8.	ø.
060320Z	21.2	86.0	45	21.0	86.2	45.	16.	е.	0.0	0.0	0.	0.	Θ.	0.0	0.0	ค.	۶١.	0.	0.9	0.0	9.	-0.	ø.
060402 Z	22.2	85.2	48	22.3	85.5	40.	18.	0.	0.0	0.0	Ð.	-3.	0.	0.0	0.0	0.	-0.	Θ.	0.0	0.0	9.	-0.	0.
060408Z	23.3	84.7	30	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-0.	θ.	0.0	0.0	Я.	-Ø.	0.	8.6	0.0	Ø.	-0.	ø.

	ALL	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24HR	48-HR	72-HR	1JP:NG	2:1-HR	40 HiR	72-HR
AVG FORECAST POSIT ERROR	22.	106.	23B.	0.	9.	8.	9.	0.
AVG RIGHT ANGLE ERROR	16.	36.	85.	0.	0.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	3.	9.	10.	0.	Θ.	0.	Ø.	0.
AVG INTENSITY BIAS	-3.	-3.	10.	0.	Ø.	0.	Θ.	0.
NUMBER OF FORECASTS	8	5	1	6	6	0	8	8

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 482, NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

8. KNOTS

TC22-82
FIX POSITIONS FOR CYCLONE NO. 22

SATELLITE FIXES

FIX NO.	TIME (Z)	F1 POSIT		ACCRY	DVORAK CODE	COMMENTS	SITE
1	300600	13.5N	87.8E	PCN 5	T1.5/1.5 、	INIT OBS	PGTW
2	310600	14.9N	90.6E	PCN 5	T2.0/2.0 /D0.5/24HRS		PGTU
3	310752	15.2N	91.1E	PCN 5	T1.0/1.0	INIT OBS ULAC FIX	KGWC
4	311600	15.9N	89.7E	PCN 5		ULCC FIX	PGTU
5	312037	15.7N	89.3E	PCN 6		ULAC FIX	KGUC
6	010600	16.5N	92.3E	PCN 3	T1.5/2.0 /U0.5/24HRS		PGTW
7	011200	17.BN	92.6E	PCN 5			PGTW
8	011600	17.0N	88.9E	PCN 5		ULCC FIX	PGTW
9	012025	16.8N	89.4E	PCN 6		BASED ON EXTRAP	KGUC
10	012100	17.4N	89.9E	PCN 5		LLCC 18.0N 93.3E	PGTM
11	020000	17.8N	89.6E	PCN 5		ULCC FIX	PGTW
12	020225	16.BN	09.5E	PCN 5	T2.0/2.0 /D1.0/30HRS	ULAC FIX	KGUC
13	020600	17.9N	88.8E	PCN 5	T2.0/2.0 /D0.5/24HRS		PGTW
14	020910	18.0N	89.2E	PCN 5	T2.5/2.5 /D0.5/0GHRS		KGWC
15	021600	17.9N	88.4E	PCN 5			PGTW
16	021800	18.3N	88.2E	PCN 5			PGTW
17	022100	18.6N	87.7E	PCN 5			PGTW
18	022155	18.6N	88.0E	РСИ 6		ULAC FIX	KGWC
19	030000	19.0N	87.8E	PCN 5			' PGTW
20	030300	19.4N	87.7E	PCH 5			PGTN
21	030600	19.6N	87.5E	PCN 5	T2.0/2.0-/S0.0/24HRS		PGTU
22	030858	19.9N	87.5E	PCN 3	T3.5/3.5 /D1.0/24HRS	EYE DIA 15NM	KGUC
23	030900	19.7N	86.9E	PCH 5	•		PGTW
24	031200	20.1N	87.0E	PCN 5			PGTW
25	031600	20.5N	86.7E	PCN 5			PGTU
26	031800	21.0N	86.5E	PCN 5			PGTW
27	032100	21.5N	85.9E	PCN 5			PGTU
28	032143	21.2N	85.8E	PCN 6			KGWC
29	040000	21.9N	85.5E	PCN 6		ULCC FIX	PGTW
30	040300	23.2N	85.7E	PCN 6	T1.5/2.0 /W8.5/21HRS		PGTW
31	040846	23.4N	84.5E	PCN 5	T1.0/2.0-/W2.5/24HPS		KGWC

TROPICAL CYCLONE 23-82 BEST TRACK DATA

		BEST 1	rack			WARN I		2000		24 H	UR FO				48 H	OUR FI				72 HO			т
MO/DA/HR	Denot t	- .		500				RORS				ERRO					Empl				Ξ	RRORS	
			JIND	POS		MIND	DST	MIND	POS	IT	MIND	DST	WIIID	POS	JΤ	WHID	DST	MIHD	POS	IT.	MIND	DST !	MIND
101320Z	13.2	91.5	25	0.0	0.0	Я.	-0.	ø.	0.0	0.0	Ø,	-0.	0.	0.0	0.0	9.	· e.	ø.	0.0	6.6	Θ.	-0.	Ð.
101402Z	13.8	90.6	30	0.0	0.0	0.	-0.	0.	0.0	0.0	9.	-0.	0.	0.0	0.0	8.	-0.	Θ.	0.8	р. р	Я.	-0.	Θ.
101408Z	14.2	89.6	30	0.0	0.0	0.	-0.	ø.	0.0	0.0	ø.	-8.	ø.	U.0	0.0	Ð.	-0.	ū.	0.0	ค.ย	n.	-u.	Ð.
1014142	14.8	88.2	30	14.2	89.6	30.	89.	0.	15.2	87.3	40.	174.	-5.	16.7	84.9	45.	201.	10.	0.0	0.0	G.	-0.	ø.
1014202	14.9	37.1	35	15.3	07.0	30.	25.	5.	16.5	84.8	12.	89	-10	17.5	02.5	45.	100	20	6.6	9.0	v.	-0.	e.
1015022	14.9	86.2	40	15.2	86.6	30.	29.	-10.	16.6	84.5	48.		-10.	0.0	0.0	ø.	0.	Ã.	0.9	6,0	Š.	-e.	0.
101508Z	14.9	85.4	40	14.9	85.7	40.	17.	ø.		83.1	50.	59.	5.	0.0	0.0	a.	-0.	Й.	0.0	8.0	9.	ø.	9.
1015142	15.2	84.3	45	15.0	84.5	45.	17.	ø.	16.2	81.3	50.	36.	15.	0.0	0.0	в.	-0.	Ñ.	0.0	2.0	2.	-0.	
1015202	15.7	83.5	50	15.2	83.1	45.	38.	-5.	17.3	79.6	25.	69.	n.	0.0	0.0	и.	-0.	n.					ø.
1016022	16.2	82.8	50	15.9		50.													8.9	0.0	Э.	-0.	ø.
							29.	ø.	0.0	0.0	Θ.	-ē.	0.	0.0	8.0	0.	-0.	0.	9.8	0.0	0.	-0.	0.
1016092	16.4	82.1	45	16.5	81.5	50.	35.	5.	0.0	0.0	0.	-0.	0.	ម.២	0.0	0.	~છે.	0.	9.0	0.0	Θ.	-0.	Э.
1816142	16.8	81.4	35	17.2	81.7	35.	30.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	-A.	ø.	9.9	0.0	۹.	0.	Ø.
1016202	17.2	80.8	25	0.0	0.0	ø.	-8.	0.	0.0	0.0	0.	-0.	ø.	0.0	0.0	0.	-0.	0.	8.8	8.9	n.	ä.	ø.

	AL.L	FORECAS	TS		TYPHO	ONS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	72-HR	WRKG	24-HR	43-HR	72-HP
AVG FORECAST POSIT ERROR	34.	88.	151.	9.	0.	0.	0.	0.
AVG RIGHT ANGLE ERROR	.81	49.	86.	0.	Θ.	0.	9.	0.
AVG INTENSITY MAGNITUDE ERROR	3.	8.	15.	0.	8.	Ø.	0.	в.
AVG INTENSITY BIAS	-2.	-1.	15.	0.	0.	ø.	0.	0.
NUMBER OF FORECASTS	9	6	2	0	Ø	a	A	B

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 681. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

. TC23-02 FIX POSITIONS FOR CYCLONE NO. 23

SATELLITE FIXES

FIX NO.	TIME (Z)	F1 POSIT		ACCRY	DVORAK CODE	COMMENTS	SITE
	127	10011		HOURT	DYONIN CODE	00/11/21/10	
	400000	44 50			T. F F	***********	
1	120802	11.8N	94.2E	PCN 5	T1.5/1.5	INIT OBS	KGUC
2	122047	13.0N	92.7E	PCN 6	24 0 4 0	**** ***	KGUC
3	130300	11.9N	93.0E	PCN 4	T1.0/1.0	INIT OBS	PGTW
4	130600	12.2N	92.5E	PCN 6		ULCC FIX	PGTW
5	130750	14.0N	91.7E	PCN 5	T2.0/2.0 /D0.5/24HRS		KGWC
6	132033	13.6N	91.4E	PCN 6			KGWC
7	140000	14. IN	91.1E	PCH 6		ULAC FIX	PG IW
8	140300	14.1H	90.8E	PCN 4	T2.0/2.0-/D1.0/24HRS	ULAC 13.8N 89.2E	FGTW
9	140600	14.8H	90.6E	PCN 4		ULAC 13.7N 88.6E	PGTI-J
10	140900	14.BH	90.7E	PCN 6			PGTW
11	140920	13.41	88.6E	PCN 5	T2.5/2.5 /DM.5/25HRS		Kenc
* 12	141200	15.5N	87.ØE	PCN 6			PG16
13	141600	15.2N	87.2E	PCN 6			PGTIJ
14	141860	15.3N	87.8E	PCN 6			PGTLI
15	142100	15.3N	86.5E	PCN 6		ULCC FIX	PGTU
16	142205	14.7N	86.6E	PCN 6		ULAC FIX	KGUC
17	150000	15.4N	86.1E	PCN 6		ULAC FIX	PGTW
18	150300	14.7N	86.2E	PCN 6	T3.0/3.0 /D1.0/24HRS		PGTN
19	158688	14.8N	85.8E	PCN 6			PGTW
20	150900	14.8N	85.2E	PCN 6		ULAC FIX	PGTW
21	150908	14.7N	85.1E	PCN 5	T1.5/2.5 /W1.0/24HRS		KGWC
22	151200	15.1N	84.6E	PCN 6		ULCC FIX	PSTU
23	151600	15.2N	83.5E	PCN 6			PGTW
24	151800	15.2N	83.1E	PCN 6			PGTW
25	152100	15.3N	82.6E	PCN 6			PGTW
26	152152	16.0N	83.6E	PCN 5			KGWC
27	160000	15.9N	82.5E	PCN 6			PGTW
28	160600	16.3N	82.2E	PCN 6	T3.0/3.0-/S0.0/27HRS		PGTU
29	160856	17.UN	82.7E	PCN 5	T1.5/1.5-/S0.0/24HRS	ULCC FIX	KGWC

TROPICAL CYCLOHE 24-82 BEST TRACK DATA

		BEST	TRACK			WARN I		RORS		24 HC	WR FO	RECAS ERRI			48 H	OUR FO	RECAS			72 H	DUR FO	RECAS	
MO/DA/HR	POSI	T	MIND	POS	1 T	WIND	DST	MIND	POS	ΙT	WIND	DST	WIND	POS	17	MIND	DST	WIND	PUS	ΓŢ	นหาม	DST	WIND
181798Z	10.4	83.7	30	0.0	0.0	0.	-0.	Θ.	0.0	0.0	0.	-0.	8.	0.0	8.9	Я,	-0.	0.	0.0	8.0	0.	-0.	0.
1017142	11.0	83.0	35	10.9	83.6	30.	36.	-5.	13.4	81.2	45.	58.	-5.	B.8	0.B	0.	~9.	8.	0.0	0.0	ø.	-0.	0.
1917202	11.6	82.2	40	11.8	82.4	48.	17.	8.	14.2	80.4	50.	58.		0.0	0.0	Ю.	~ຄ.	₿.	9.0	0.0	₽.	-0.	0.
1018022	12.1	81.6	45	12.1	82.2	45.	35.	0.	14.2	80.4	50.	88.	28.	0.0	0.0	0.	-0.	0.	0.0	0.0	3.	-0.	0.
101808Z	12.9	81.1	45	12.8	81.7	50.	36.	5.	0.0	0.0	Я,	-Ø.	8.	ค. ย	0.8	0.	-0.	0.	0.9	0.0	9.	-0.	0.
101B14Z	13.8	89.3	50	13.8	80.2	50.	6.	0.	0.0	6.8	0.	-8.	я.	B. B	0.0	0.	-8.	Ø.	0.0	0.0	9.	-0.	0.
1018202	14.6	79.5	45	14.5	79.6	45.	8.	0.	0.0	0.0	0.	-0.	0.	0.0	0.0	0.	0.	0.	0.0	8.0	ø.	-0.	0.
1019022	15.1	79.2	30	14.9	79.4	30.	17.	Ø.	0.0	р.а	0.	-0.	0.	0.0	0.0	ด.	-0.	0.	0.0	8.0	0.	-Ð.	0.

	ALL	FORECAS	TS		TYFFE	DHS WHIL	E OVER	35 KTS
	WRNG	24-HR	48-HR	7?-HR	URNG	?4-HR	48 HR	72-IIR
AVG FORECAST POSIT ERROR	22.	68.	0.	Ø.	8.	8.	0.	ρ.
AVG RIGHT ANGLE ERROR	15.	22.	0.	Θ.	8.	3.	ຍ.	0.
AVG INTENSITY MAGNITUDE ERROR	1.	ί0.	0.	0.	0.	8.	я.	0.
AVG INTENSITY BIAS	0.	7.	0.	0.	0.	ð.	0.	U.
NUMBER OF FORECASTS	7	3	Ø	0	8	8	8	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 389. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS 9. KNOTS

TC24-82
FIX POSITIONS FOR CYCLONE NO. 24

SATELLITE FIXES

FI) NO.		TIME (2)	F1 POSIT		ACCRY	DVORAK CODE	COMMENTS	SITE
* 1	-	150908	7.6N	88.0E	PCN 5	T1.5/1.5	THIT OBS ULCE FIX	KGWC
* 2		160856		83.8E		T2.0/2.0 /D0.5/24HRS	ULCC FIX	KGWC
* 3	3	162140	10.9N	84.2E	PCN 6		ULCC 10.0N 84.4E	KGWC
	4	170843	10.5N	83.5E	PCN 5	T2.5/2.5 /D0.5/24HRS		KGUC
	5	172128	11.0N	81.3E	PCN 6		DEGC FIX	KG₩C
€	5	180831	12.9N	80.1E	PCN 5	13.0/3.0-/D0.5/24HRS		KGWC

SYNOPTIC FIXES

FIX NO.	TIME (Z)	F1X POSIT		INTENSITY ESTIMATE	NEAREST DATA (NM)		COMMENTS
1	181500	14.0N	80.0E	045	030	WM043279	

TROPICAL CYCLONE 25-82 BEST TRACK DATA

		BEST T	TRACK			WARN		RORS		24 HO	ÚR F	ORECA: ERRI			48 H	OUR FO	DRECA: ERRO			72 HO		ORECAS ERRURS	
MD/DA/HR	POST	т 1	JIND	POS	1T	WIND		MIND	POS	TT.	UIND	DST	MIND	PDS	1 T	MIND	DST	MIND	POS	T.T.	MIND,		MIND
1104142	11 1	63.9	20	0.0	9.0	0.	-Ø.	ø.	0.0	. 0.0	0.110	-0.	0.	0.0	9.0	Ø.	-8.	Ø. 111D	9.0	ີ່ ຍ. ຍ	۵۱,	-0.	0.
1104202	11.3	63.6	25	9.0	8.0	ø.	-0.		0.0	0.0	Đ.	-0.	0.			8.							
1105022	11.8		38											0.0	0.0		-0.	e.	8.0	0.0	_0.	-0.	0.
		63.5		11.0	62.7	35.	67.	5.	12.6	59.9	48.	294.	5.	13.7	56.9	50.	583.	-5.	15.7	54.2	55.		- 25.
1105082	12.1	63.8	39	11.5	62.8	30.	69.	ø.	12.3	60.8	40.	273.	0.	13.2	58.0		582.	-10.	14.8	55.1	55.		-35.
110514Z	12.4	64.2	30	12.5	63.2	30.	59.	0.	14.1	61.4	40.	251.	-5.	15.2	59.2	45.	539.	-20.	16.3	56.9	35.	887.	-45.
i 10520Z	12.7	64.5	38	12.0	63.0	30.	97.	0.	13.0	62.7	35.	223.	-15.	14.7	69.8	40.	513.	-30.	15.0	58.6	35.	884.	-25.
110682Z	13.1	64.9	35	14.2	62.8	35.	139.	0.	16.4	60.5	45.	370.	-10.	18.1	58.0	50.	675.	- 50.	19.2	56.0	33.1	1822.	·-5.
110609Z	13.5	65.3	40	14.0	62.2	35.	183.	-5.	15.7	59.6	45.	457.	-15.	17.5	57.2	50.	775.	-40.	0.0	9.0	Я.	-0.	ø.
110614Z	13.9	65.7	45	13.8	65.8	45,	8.	0.	15.8	67.6	55.	99.	-10.	18.7	69.1	60.	220.	-20.	0.0	0.9	9.	-0.	ø.
110620Z	14.5	66.2	50	14.3	66.2	50.	12.	ø.	16.7	68.0	55.	109.	-15.	19.6	69.5	65.	238.	5.	0.0	0.0	9.	-0.	
1107027	15.3	66.8	55	14.9	66.6	60.	27.	5.	17.2	68.2	75.	160.	-5.	20.4	69.8	60.	261.	20.	0.0	0.0	e.	-0.	ø.
1107082	16.3	67.5	60	15.4	67.0	60.	61.	Đ.	17.8	68.8	75.	188.	-15.	0.0	0.0	0.	-9.	0.	8.8	0.0	Й.	-8.	Ð.
1107142	17.3	68.3	65	17.1	68.1	65.	17.	ø.	21.1	71.A	69.	41.	-29.	0.0	8.8	ø.	-0.	9.	0.0	0.0	ø.	-ø.	ø.
1107202	18.3	68.9	70	18.0	68.8	65.	19.	-5.	22.1	71.6	55.	57.	-5.	0.0	0.8	ø.	-0.	ē.	0.0	0.0	ø.	-0.	ē.
1108022	19.4	69.8	80	19.1	69.1	65.	44.	-15.	23.0	71.4	45.	142.	5.	0.0	0.0	ø.	-0.	ø.	0.0	0.0	Ø.	-0.	ø.
110808Z	20.5	70.5	94	28.8	69.3	60.	74.	-30.	0.0	0.0	0.	-0.	ø.	0.0	0.0	9.	-0.	0.	9.0	0.0	в.		e.
1108142	21.6	71.5	88	21.3	71.3	80.	25.	0.	0.0	0.0	e.	-0.	8.	0.0	8.8	8.	-B.	8.				-0.	
1108202					77.4			5.			0.								0.0	9.8	8.	-0.	0.
	22.3	72.6	68	22.2	(2.1	65.	28.		9.0	9.0	_	-0.	ø.	0.0	0.0	0.	-0.		0.0	0.0	ø.	-0.	0.
1109022	22.5	73.9	40	22.4	73.7	40.	13.	0.	0.0	0.0	0.	-0.	ρ.	0.0	0.0	0.	-0.	0.	0.0	9.8	0.	-0.	0.

	ALL FORECASTS				TYPHOONS WHILE DVER 35 KIS			
	WRNG	24-HR	48-HR	72~HR	WRIIG	24-HR	48-HR	72-HR
AVG FORECAST POSIT ERROR	55.	205.	487.	931.	ø.	0.	0.	0.
AVG RIGHT ANGLE ERROR	34.	113.	264.	519.	0.	0.	0.	0.
AVG INTENSITY MAGNITUDE ERROR	4.	10.	20.	27.	0.	Ð.	в.	0.
AVG INTENSITY BIAS	-2.	-e.	-14.	-27.	0.	Θ.	0.	0.
NUMBER OF FORECASTS	17	13	9	5	0	Я	9	0

DISTANCE TRAVELED BY TROPICAL CYCLONE IS 949. NM

AVERAGE SPEED OF TROPICAL CYCLONE IS

9. KNDTS

TC25-82
FIX POSITIONS FOR CYCLONE HO. 25

SATELLITE FIXES

	1X 10.	TIME (Z)	FI POSIT		ACCRY	DVORAK CODE	COMMENTS	SITE
*	1	032307	12.5N	66.1E	PCN 5		ULAC 11.5N 66.4E	KGWC
*	2	041810	12.3N	62.4E	PCN 5	T2.5/2.5+/D1.5/24HRS	ULAC 12.3N 61.6E	KGWC
*	3	842255	10.6N	62.3E	PCN 5		ULAC 11.4H 62.6E	KGWC
	4	050958	12.1N	63.3E	PCN 5	T3.0/3.0 /D0.5/24HRS	ULAC 12.9N 62.6E	KGWC
*	5	052243	14.0N	63.2E	PCN 5		ULAC 12.3N 63.8E	KGWC
	6	060946	13.3N	65.7E	PCN 5	T3.0/3.0 /S0.0/24HRS	ULAC 12.5N 64.4E	Kenc
	7	062231	14.5N	66.3E	PCN 5			KGWC
	Θ	070934	16.4N	67.7E	PCN 5	T3.5/3.5 /D8.5/24IRS	ULAC 16.0N 70.5E	KGWC
	9	072218	18.5N	68.9E	PCN 5		ULAC 18.5N 69.3E	KGWC
	10	080921	20.6N	70.6E	PCN 1		EYE DIA 24HM	KGWC

SYNOPTIC FIXES

FIX NO.	TIME (Z)	FIX POSIT		ESTIMATE	NEAREST DATA (NM)	CONTRENT	3
1 2 3 4	041200 060600 081500 090000	11.0N 14.0N 21.8N 22.3N	64.2E 62.2E 71.7E 73.3E	020 040 860 040	010 090 060 060	SHIP OBSERVATION SHIP OBSERVATION LMO 42737 LMO 42647	

APPENDIX I CONTRACTIONS

ACCRY	Accuracy	GOES	Geostationary Operational Environmental Satellite
ACFT ADP	Aircraft Automated Data Processing	HATTRACK	Hurricane and Typhoon Tracking
AFGWC	Air Force Global Weather Central	HGT	(Steering) Program Height
AIREP	Aircraft Weather Report(s)		•
AIREF	(Commerical and Military)	HPAC	Mean of XTRP and CLIM Techniques (Half Persistence and Climatology)
ANT	Antenna	HR	Hour(s)
AOR	Area of Responsibility	HVY	Heavy
APRNT	Apparent	ICAO	International Civil Aviation Organization
APT	Automatic Picture Transmission	INIT	Initial
ARWO	Aerial Reconnaissance Weather Officer	INJAH	North Indian Ocean Component
ATT	Attenuation		of TYAN
AVG	Average	INST	Instruction
AWN	Automated Weather Network	IR	Infraced
BPAC	Blended Persistence and Climatology	KM	Kilometer(s)
BRG		KM/HR	Kilometer(s) per Hour
	Bearing	KT	Knot(s)
CDO	Central Dense Overcast	LLCC	Low-level Circulation Center
CI	Cirriform Cloud or Cirrus also Current Intensity (Dvorak)	LVL	Level
CINCPAC	Commander-in-Chief Pacific	М	Meter(s)
	AF - Air Force, FLT - Fleet (Navy)	M/SEC	Meter(s) per Second
CLD	Cloud	MAX	Maximum
CLIM	Climatology	МВ	Millibar(s)
CLSD	Closed	MET	Meteorological
CM	Centimeter	MIN	Minimum
CNTR	Center	монатт	Modified HATTRACK
CPA	Closest Point of Approach	MOVG	Moving
CSC	Cloud System Center	MSLP	Minimum Sea Level Pressure
CYCLOPS	Tropical Cyclone Steering Program (HATTRACK and MOHATT)	MSN	Mission
DEG	Degree(s)	NAV	Navigational
DIAM	Diameter	NEDN	Naval Environmental Data Network
DIR	Direction	NEDS	Naval Environmental Display Station
DMSP	Defense Meteorological Satellite	NEPRF	Naval Environmental Prediction
Drisp	Program	NEPRE	Research Facility
EL	Elongated	NESS	National Environmental Satellite Service
ELEV	Elevation	NET	Near Equatorial Trough
EXP	Exposed	NM	Nautical Mile(s)
FI	Forecast Intensity (Dvorak)	N/O	Not Observed
FLT	Flight	-	
FNOC	Fleet Numerical Oceanography Center	NOAA	National Oceanic and Atmospheric Administration
FT	Feet (Foot)	NOCC	Naval Oceanography Command Center
GMT	Greenwich Mean Time	NWOC	Naval Western Oceanography Center

NR	Number	TC	Tropical Cyclone
NRL	Naval Research Laboratory	TCARC	Tropical Cyclone Aircraft Reconnaissance Coordinator
NTCM	Nested Tropical Cyclone Model		,
OBS	Observation(s)	TCFA	Tropical Cyclone Formation Alert
OTCM	One-way (Interactive) Tropical	TCM	Tropical Cyclone Model
	Cyclone Model	TD	Tropical Depression
PACOM	Pacific Command	TDO	Typhoon Duty Officer
PCN	Position Code Number	TIROS	Televison Infrared Observation
PSBL	Possible	m o	
PTLY	Partly	TS	Tropical Storm
OUAD	Ouadrant	TY	Typhoon
RADOB	Radar Observation(s)	TYAN	Typhoon Analog Program
RECON	Reconnaissance	TYFN	Western North Pacific Component (Revised) of TYAN
RNG	Range	TUTT	Tropical Upper-Tropospheric Trough
RT	Right	ULAC	Upper-level Anticyclone
SAT	Satellite	VEL	Velocity
SFC	Surface	vis	Visual
SLP	Sea Level Pressure	VSBL	Visible
SPOL	Spiral Overlay	WESTPAC	Western (North) Pacific
SRP	Selective Reconnaissance Program	WMO	World Meteorological Organization
STNRY	Stationary	WND	Wind
SST	Sea Surface Temperature	WRNG(S)	Warnings
ST	Subtropical	WRS	Weather Reconnaissance Squadron
STR	Subtropical Ridge	XTRP	Extrapolation
STY	Super Typhoon	Z	Zulu Time
TAPT	Typhoon Acceleration Prediction Technique		(Greenwich Mean Time)

APPENDIX II

DEFINITIONS

BEST TRACK - A subjectively smoothed path, versus a precise and very erratic fixto-fix path, used to represent tropical cyclone movement.

CENTER - The vertical axis or core of a tropical cyclone. Usually determined by wind, temperature, and/or pressure distribution.

CYCLONE - A closed atmospheric circulation rotating about an area of low pressure (counterclockwise in the Northern Hemisphere).

EPHEMERIS - Position of a body (satellite) on space as a function of time; used for gridding satellite imagery. Since ephemeris gridding is based soley on the predicted position of the satellite, it is susceptible to errors from vehicle pitch, orbital eccentricity, and the oblateness of the earth.

EXPLOSIVE DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 2.5 mb/hr for 12 hrs or 5.0 mb/hr for six hrs (ATR 1971).

EXTRATROPICAL - A term used in warnings and tropical summaries to indicate that a cyclone has lost its "tropical" characteristics. The term implies both poleward displacement from the tropics and the conversion of the cyclone's primary energy sources from release of latent heat of condensation to baroclinic processes. The term carries no implications as to strength or size.

 $\underline{\text{EYE}}$ - "EYE" is used to describe the central area of a tropical cyclone when it is more than half surrounded by wall cloud.

FUJIWHARA EFFECT - An interaction in which tropical cyclones within about 700 nm (1296 km) of each other begin to rotate about one another. When intense tropical cyclones are within about 400 nm (741 km) of each other, they may also begin to move closer to each other.

MAXIMUM SUSTAINED WIND - Maximum surface wind speed averaged over a one-minute period of time. Peak gusts over water average 20 to 25 percent higher than sustained winds.

RAPID DEEPENING - A decrease in the minimum sea level pressure of a tropical cyclone of 1.25 mb/hr for 24 hrs (ATR 1971).

<u>RECURVATURE</u> - The turning of a tropical cyclone from an initial path toward the west or northwest to a path toward the northeast.

RIGHT ANGLE ERROR - The distance described by a perpendicular line from the best track to a forecast position. (See Figure 4-1).

SIGNIFICANT TROPICAL CYCLONE - A tropical cyclone becomes "significant" with the issuance of the first numbered warning by the responsible warning agency.

SUPER TYPHOON/HURRICANE - A typhoon/hurricane in which the maximum sustained surface wind (one-minute mean) is 130 kt (67 m/sec) or greater.

TROPICAL CYCLONE - A non-frontal low pressure system of synoptic scale developing over tropical or subtropical waters and having a definite organized circulation.

TROPICAL CYCLONE AIRCRAFT RECONNAISSANCE COORDINATOR - A CINCPACAF representative designated to levy tropical cyclone aircraft weather reconnaissance requirements on reconnaissance units within a designated area of the PACOM and to function as coordinator between CINCPACAF, aircraft weather reconnaissance units, and the appropriate typhoon/hurricane warning center.

TROPICAL DEPRESSION - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 33 kt (17 m/sec) or less.

TROPICAL DISTURBANCE - A discrete system of apparently organized convection--generally 100 to 300 nm (185 to 556 km) in diameter--originating in the tropics or subtropics, having a non-frontal migratory character, and having maintained its identity for 24 hours or more. It may or may not be associated with a detectable perturbation of the wind field. As such, it is the basic generic designation which, in successive stages of intensification, may be classified as a tropical depression, tropical storm or typhoon (hurricane).

TROPICAL STORM - A tropical cyclone with maximum sustained surface winds (one-minute mean) in the range of 34 to 63 kt (17 to 32 m/sec) inclusive.

TROPICAL UPPER-TROPOSPHERIC TROUGH (TUTT) "A dominant climatological system, and a daily synoptic feature, of the summer season over the tropical North Atlantic, North Pacific and South Pacific Oceans," from - Sadler, J.C., Feb. 1976: Tropical Cyclone Initiation by the Tropical Upper-Tropospheric Trough (NAVENUPREDRSCHFAC Technical Paper No. 2-76).

TYPHOON/HURRICANE - A tropical cyclone in which the maximum sustained surface wind (one-minute mean) is 64 kt (33 m/sec) or greater. West of 180 degrees longitude they are called typhoons and east of 180 degrees they are called hurricanes. Foreign governments use these or other terms for tropical cyclones and may apply different intensity criteria.

VECTOR ERROR - The distance described by a straight line from the forecast position to the position at verification time as found on the best track. (See Figure 4-1).

WALL CLOUD - A organized band of cumuliform clouds immediately surrounding the central area of a tropical cyclone. The wall cloud may entirely enclose or only partially surround the center.

APPENDIX III NAMES FOR TROPICAL CYCLONES

Column 1	Column 2	Column 3	Column 4
ANDY	ABBY	ALEX	AGNES
BESS	BEN	BETTY	BILL
CECIL	CARMEN	CARY	CLARA
DOT	DOM	DINAH	DOYLE
ELLIS	ELLEN	ED	ELSIE
FAYE	FORREST	FREDA	FABIAN
GORDON	GEORGIA	GERALD	GAY
HOPE	HERBERT	HOLLY	HAZEN
IRVING	IDĀ	IKE	IRMA
JUDY	JOE	JUNE	JEFF
KEN	KIM	KELLY	KIT
LOLA	LEX	LYNN	LEE
MAC	MARGE	MAURY	MAMIE
NANCY	NORRIS	NINA	NELSON
OWEN	ORCHID	OGDEN	ODESSA
PAMELA	PERCY	PHYLLIS	PAT
ROGER	RUTH	ROY	RUBY
SARAH	SPERRY	SUSAN	SKIP
TIP	THELMA	THAD	TESS
VERA	VERNON	VANESSA	VAL
WAYNE	WYNNE	WARREN	WINONA

NOTE:

Names are assigned in rotation, alphabetically. When last name (WINONA) has been used, the sequence will begin again with "ANDY."

Source: CINCPACINST 3140.1 (series)

APPENDIX IV

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APPENDIX V PAST ANNUAL TYPHOON/TROPICAL CYCLONE REPORTS

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CINCPACAF/DOS (1)	NOAA/NESS WASHINGTON DC (2)
CINCPACFLT (3)	
	NOAA/PMEL SEATTLE, WA (2)
CIUDAD UNIV, MEXICO (1)	NOCD, AGANA (3)
CIVIL DEFENSE, GUAM (5)	NOCD, ASHEVILLE (3)
CIVIL DEFENSE, SAIPAN (6)	NOCD, ATSUGI(1)
CNO WASHINGTON DC (1)	NOCD, BARBERS POINT (1)
CNOC (2)	NOCD, KADENA (2)
COLORADO STATE UNIV (3)	NOCD, MISAWA (2)
COLORADO STATE UNIV (LIBR) (1)	NOCD, MONTEREY (1)
COMFAIRECONRON ONE (VQ-1) (2)	NOCF, CUBI POINT (1)
COMNAVAIRSYSCOM (1)	NPGS DEPT OF MET (3)
COMNAVFACENGCOMPACDIV (1)	NPGS LIBRARY (1)
COMNAVMARIANAS (2)	
	OCEAN ROUTES INC, CA (2)
COMNAVSURFGRU (1)	OCEANO SERVICES INC, CA (1)
COMNAVSURFPAC (3)	OCEANO SERVICES INC, CA (1)
COMPATRECONFORSEVENTHFLT (1)	OKINAWA MET OBS (1)
	OLG/HQ AWS (1)
COMPHIBGRU ONE (1)	
COMSC (1)	PACAF/DOS (1)
COMSEVENTHFLT (1) \	PAGASA RP (3)
COMSUBGRU SEVEN (1)	PENNSYLVANIA SATE UNIVERSITY (1)
COMTHIRDFLT (1)	ROYAL OBSERVATORY HONG KONG (5)
COMUSNAVPHIL (1)	SCALLOP CORP (1)
CONGRESSIONAL INFORMATION SERVICE (2)	STARS AND STRIPES (1)
COORDINATED SCIENCE LABORATORY (1)	TAIWAN UNIV (3)
DEFENSE COMMUNICATIONS AGENCY, GUAM (1)	TEXAS A&M UNIV (1)
DEFENSE TECHNICAL INFORMATION CENTER (2)	TTPI, SAIPAN (8)
DEPT OF AIR FORCE (1)	TYPHOON COM SECR, MANILA (2)
DET 2, 1WW (2)	UNESCAP (4)
DET 4, 1WW (1)	UNIV OF CHICAGO (2)
DET 4, HQ AWS (2)	UNIV OF GUAM (2)
DET 5, 1WW (2)	
	UNIV OF HAWAII DEPT OF MET (3)
DET 8, 30WS (2)	UNIV OF HAWAII LIBRARY (1)
DET 10, 30WS (1)	UNIV OF ILLINOIS AT URBANA-CHAMPAIGN (1)
DET 15, 30WS (1)	UNIV OF RP (2)
	uec (1)
DET 17, 30WS (1)	USC (1)
DET 18, 30WS (1)	USC (1) UNIV OF WASHINGTON (1)
DET 18, 30WS (1) FAA, GUAM (5)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU MOOD (LHA-3) (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU **COD (LHA-3) (1) USS BLUE RIDGE (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU *COOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMCCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU **COD (LHA-3) (1) USS BLUE RIDGE (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMCCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU *COOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BELUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARSINERS WEATHER LOG (2) MASS INSTI OF TECH (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1) LWW/DON (4)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1) MCAS IWAKUNI (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1) LWW/DON (4)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1) MCAS FUTENMA (1) MCAS KANEOHE BAY (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1) 1WW/DON (4) 3AD/DOX (1) 3WW/DNC (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MARINERS WEATHER LOG (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1) MCAS IWAKUNI (2) MCAS KANEOHE BAY (1) MET DEPT BANGKOK (1)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1) 1WW/DON (4) 3AD/DOX (1) 3WW/DNC (1) 5WW/DNC (1)
DET 18, 30WS (1) FAA, GUAM (5) FLENUMOCEANCEN MONTEREY (2) FLORIDA STATE UNIV TALLAHASSEE (2) GEOLOGICAL SURVEY, GUAM (2) GOVERNOR OF GUAM (4) GUAM PUBLIC LIBRARY (5) HUGHES AIRCRAFT COMPANY (1) INDIA MET DEPT (3) INST OF PHYSICS, TAIWAN (2) INSTITUO DE GEOFISICA (1) JAPAN MET AGENCY (3) JASDF, TOKYO (2) LOS ANGELES PUBLIC LIBRARY (2) MAC/HO, IL (2) MASS INSTI OF TECH (1) MCAS FUTENMA (1) MCAS FUTENMA (1) MCAS IWARUNI (2) MCAS KANEOHE BAY (1) MET RESEARCH INST LIBRARY, TOKYO (2)	UNIV OF WASHINGTON (1) UNSECDEF, PENTAGON (1) USS BELLEAU WOOD (LHA-3) (1) USS BLUE RIDGE (1) USS CONSTELLATION (2) USS CORAL SEA (1) USS ENTERPRISE (1) USS ENTERPRISE (1) USS KITTY HAWK (1) USS LONG BEACH (2) USS NEW ORLEANS (2) USS OKINAWA (1) USS RANGER (2) USS TARAWA (1) USS TRIPOLI (2) WEA SERV MET OBS, AGANA (2) WEATHER MODIFICATION PROGRAM OFFICE (1) WORLD WEATHER BLDG LIBRARY (1) 1WW/DON (4) 3AD/DOX (1) 3WW/DNC (1) 5WW/DNC (1) 5WW/DNC (1) 17 WS/DON (1)
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REPORT DOCUMENTATION P	READ INSTRUCTIONS	
1 PERCET NUMBER		BEFORE COMPLETING FORM
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1982 ANNUAL TROPICAL CYCLONE REPO	RT	Annual (Jan-Dec 1982)
	i	6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(a)		8. CONTRACT OR GRANT NUMBER(s)
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18. SUPPLEMENTARY NOTES		
 KEY WORDS (Continue on reverse side if necessary and in Tropical cyclones 		depressions
Tropical cyclone forecasting	Tropical	
Tropical cyclone research		Super typhoons
Tropical cyclone best track data Meteorological satellite Tropical cyclone fix data Aircraft reconnaissance		-
20. ABSTRACT (Continue on reverse side if necessary and id		
Annual publication summarizing the tropical cyclone season in the western North Pacific, Bay of Bengal and Arabian Sea. A brief narrative is given on each significant tropical cyclone including its best track. All reconnaissance data used to construct the best tracks are provided. Forecast verification data and statistics for the JTWC are summarized. Research efforts at the JTWC and recent NOCC/JTWC publications are briefly discussed.		

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FM NAVOCEANCOMCEN GUAM
TO TYPHOON WARNING WESTPAC
BT
UNCLAS
WTPA32 PGTW 280500
MSGID/NOCC GUAM/SPECIAL/04/AUG/TROP CYCLONE NR15/AMP/26
REF/NOCC GUAM/270813Z1/AUG/82/SPECIAL/04/AUG/AMP/25
UNK/JTWCCONT08-15/TROPICAL STORM FAYE WARNING NR 27
LAMP/2 ACTIVE TROPICAL CYCLONES IN WESTPAC
TMPOS/280600Z6/2415N2/13045E3/FIXED/OTHER/40NM/070T/13K
LAMP/POSIT BASED ON CENTER LOCATED BY SATELLITE DATA
LAMP/WINDS MAX 035K/GUSTS 045K
AREA/2415N2/13045E3/040NM
TIME/280600Z6/////AREA OF OVER 30KT WINDS
RMKS/REPEAT POSIT 2415N2 13045E3/////FORECAST FOLLOW
LAMP/
TMPOS/281800Z9/2530N0/13310E8
LAMP/12 HR FCST POSIT
LAMP/WINDS MAX 040K/GUSTS 050K
LAMP/
TMPOS/290600Z7/2655N8/13540E3
LAMP/24 HR FCST POSIT
LAMP/WINDS MAX 050K/GUSTS 065K
AREA/2655N8/13540E3/040NM
TIME/290600Z7/////AREA OF OVER 30KT WINDS
RMKS/EXTENDED OUTLOOK FOLLOWS/////
LAMP/
TMPOS/300600Z9/3015N9/13925E1
LAMP/48 HR FCST POSIT
LAMP/WINDS MAX 050K/GUSTS 065K
LAMP/
TMPOS/310600Z0/3415N3/14230E0
LAMP/72 HR FCST POSIT
LAMP/WINDS MAX 050K/GUSTS 065K
NARR/ACFT RECON REQUESTED FOR 282200Z AND 291000Z.
NEXT WARNINGS AT 281200Z, 281900Z, 290100Z AND 290700Z.
AT 280000Z SATELLITE IMAGERY REVEALED THAT TROPICAL STORM FAYE
HAD REGENERATED NEAR 23.6N1 129.5E7. THE SYSTEM REMAINS COMPACT
IN SIZE AND MAXIMUM WIND RADII ARE SMALL.
THIS WARNING SUPERSEDES THE TROPICAL CYCLONE BULLETIN ISSUED
AT 280323Z AUG 82 (WTPA31 PGTW 280318Z)
REFER TO NAVOCEANCOMCEN GUAM 280029Z AUG 82 (WTPA33 PGTW 280100)
AND SIX-HOURLY UPDATES FOR WARNINGS ON TROPICAL STORM GORDON.
ENDAT/
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